

# Thermal and mechanical properties of the near-surface layers of comet 67P/Churyumov-Gerasimenko

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Thermal and mechanical material properties determine comet evolution and even solar system formation because comets are considered remnant volatile-rich planetesimals. Using data from the Multipurpose Sensors for Surface and Sub-Surface Science (MUPUS) instrument package gathered at the Philae landing site Abydos on comet 67P/Churyumov-Gerasimenko, we found the diurnal temperature to vary between 90 and 130 K. The surface emissivity was 0.97, and the local thermal inertia was  $85 \pm 35 \text{ J m}^{-2} \text{ K}^{-1} \text{ s}^{-1/2}$ . The MUPUS thermal probe did not fully penetrate the near-surface layers, suggesting a local resistance of the ground to penetration of >4 megapascals, equivalent to >2 megapascal uniaxial compressive strength. A sintered near-surface microporous dust-ice layer with a porosity of 30 to 65% is consistent with the data.

The Multipurpose Sensors for Surface and Sub-Surface Science (MUPUS) package (1, 2) operated on the approach to and on the surface of 67P/Churyumov-Gerasimenko (67P) between 12 and 14 November 2014. MUPUS (Fig. 1) is composed of three separate instruments: (i) a thermal probe, MUPUS-PEN, which is equipped with 16 resistance temperature detector-type titanium temperature sensors to be inserted into the cometary surface by a hammer mechanism; (ii) an infrared radiometer, MUPUS-TM; and (iii) a thermal sensor and an accelerometer in each of the two harpoon anchors of the lander. MUPUS-PEN was stowed on Philae during flight, and landing and was nominally deployed. MUPUS-TM is mounted to the lander in a fixed position, with the line of sight having an angle of  $45^\circ$  relative to the lander vertical axis and an opening angle of  $\pm 30^\circ$  around the line of sight. The total field of view (FOV) of  $\sim 1 \text{ m}^2$  and the full-width-half-maximum FOV of  $0.3 \text{ m}^2$  include the MUPUS-PEN deployment location.

MUPUS was designed to measure thermal and mechanical properties of the surface and the near-surface layers and to monitor the subsurface temperature. Because the harpoon anchors failed to fire (for reasons still being investigated by the lander engineers) and because MUPUS-PEN could not be fully inserted, subsurface thermal and mechanical properties could not be measured, unfortunately. Instead, a lower bound on the

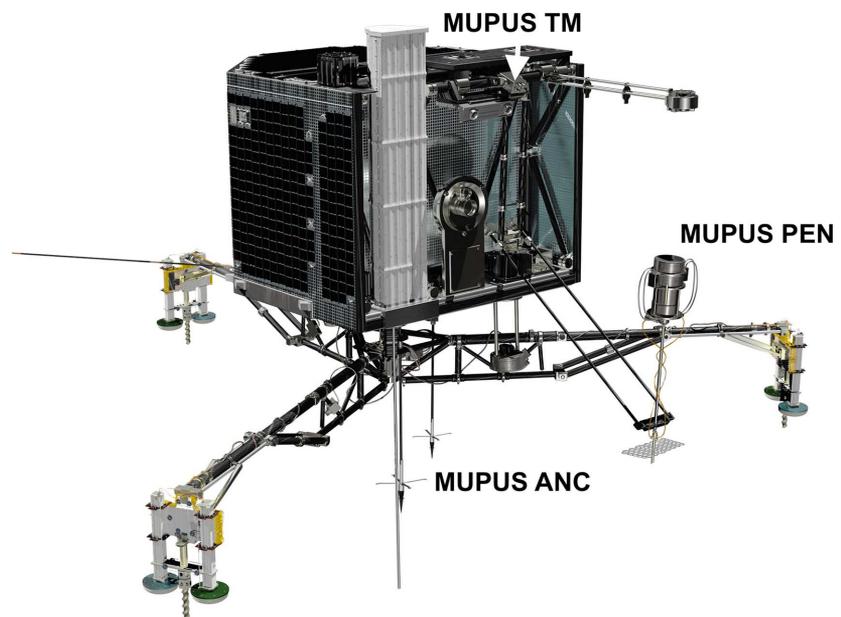
strength of the subsurface material was derived from the observed failure to penetrate of MUPUS-PEN. MUPUS-TM data were inverted in order to calculate the local daily temperature variation, the thermal emissivity, and the thermal inertia.

MUPUS-TM was switched on 1 hour before the release of Philae from Rosetta and recorded during the descent of the lander and its involuntary flight across the surface until final touchdown. These data include coverage of the surface along

the flight path, which need to be evaluated separately. The MUPUS-TM data have been used to help reconstruct the flight path of the lander (3). After the lander had settled at its final landing site, Abydos, MUPUS-TM recorded for another 41 hours.

The diurnal temperature variation (Fig. 2) was synthesized from 3 days of radiometer data and from MUPUS-PEN temperature recordings (figs. S2 to S4). The emissivity  $\epsilon$  was determined by means of least-square analysis of the TM data and was found to be  $\sim 0.97$ . The temperature varies between 90 and 130 K. This is an equivalent gray-body temperature. It should be representative of the average temperature in the FOV of MUPUS-TM. Also shown is our estimate of the  $2\sigma$  uncertainty range. A characteristic peak in temperature of  $\sim 36$  min duration is shown in Fig. 2. The complete temperature history recordings at Abydos (figs. S2 and S4), derived from the flux measured with MUPUS-TM and from MUPUS-PEN temperature recordings, show three peaks separated by 12.4 hours, which is the rotation period of the nucleus (4). We interpret these peaks as infrared radiation from the directly insolated surface, whereas the more gentle variation of the temperature outside a peak is interpreted as being due to indirect lighting.

Thermal models have been calculated to fit the data (Fig. 2). The calculation is described in more detail in the supplementary materials. We show three curves for thermal inertia  $I = \sqrt{k\rho c}$ , where  $k$  is the thermal conductivity,  $\rho$  is the density, and  $c$  is the specific heat, varying between 50 and  $120 \text{ J m}^{-2} \text{ K}^{-1} \text{ s}^{-1/2}$ , with  $85 \text{ J m}^{-2} \text{ K}^{-1} \text{ s}^{-1/2}$  providing the best fit. A thermal inertia of 10 to



**Fig. 1. Elements of the MUPUS package on the Rosetta lander Philae.** Shown is Philae with the instrument bench (also termed the balcony). The thermal mapper MUPUS-TM is shown along with the deployed thermal probe MUPUS-PEN and the two anchors, each of which houses an accelerometer, MUPUS ANC-M, and a temperature sensor, ANC-T. MUPUS-PEN is shown connected to its deployment device extending from the balcony. This double strut device was retracted 300 min after MUPUS switched on so as to allow a later rotation of the lander body. [Image courtesy ESA/ATG media lab]

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$50 \text{ J m}^{-2} \text{ K}^{-1} \text{ s}^{-1/2}$  has been inferred from the measurements reported by the Microwave Instrument for the Rosetta Orbiter (MIRO) as a representative value of the overall surface of 67P (5). Our value is clearly larger, although considering the variability of the parameters determining the thermal inertia, not dramatically so. Abydos may simply have a thinner spread of low-conductivity and -density dust than on average, underlain by a sintered but still porous dust-ice layer. Other differences may be in the dust-to-ice ratio, dust composition, and local versus global average temperature and subsurface temperature gradients. MIRO as a millimeter and submillimeter instrument samples a thicker layer than does MUPUS-TM. From unresolved Spitzer observations of 67P, an upper limit of  $15 \text{ J m}^{-2} \text{ K}^{-1} \text{ s}^{-1/2}$  was proposed (6). Other estimates of the thermal inertia of cometary nuclei are  $<45$  and  $200 \text{ J m}^{-2} \text{ K}^{-1} \text{ s}^{-1/2}$  (7, 8) for comet 9P/Tempel 1—both studies using the same Deep Impact data—and  $<250 \text{ J m}^{-2} \text{ K}^{-1} \text{ s}^{-1/2}$  (7) for comet Hartley 2. Our value is smaller than that of kilometer-sized near-Earth asteroids (9) and suggests a near-surface porous layer. Differences in thermal inertia may further indicate differences in degrees of compaction and sintering and concentrations of organics in near-surface layers (10).

Unfortunately, the local values of  $k$ ,  $\rho$ , and  $c$  have not been individually measured (11). Using the overall density of the comet of  $470 \pm 45 \text{ kg m}^{-3}$  (4) and a specific heat of 300 to  $600 \text{ J kg}^{-1} \text{ K}^{-1}$  as appropriate for a mixture of silicate dust (12) and water ice (13), with a dust-to-ice ratio of 2 to 6 (14) at temperatures of 90 to 130 K, a thermal conductivity of 0.02 to  $0.06 \text{ W m}^{-1} \text{ K}^{-1}$  is implied for  $I = 85 \text{ J m}^{-2} \text{ K}^{-1} \text{ s}^{-1/2}$  ( $8 \times 10^{-3}$  to  $0.11 \text{ W m}^{-1} \text{ K}^{-1}$  if the full uncertainty of the thermal inertia is considered). These values compare with values of  $2 \times 10^{-3}$  to  $0.02 \text{ W m}^{-1} \text{ K}^{-1}$  reported for silicate dust in vacuum (15), albeit at ambient temperatures, and with values of 0.02 to  $0.03 \text{ W m}^{-1} \text{ K}^{-1}$  for nonsintered porous ice at 100 K (16). Our values are consistent with porosities between 40 and 55% (30 to 65% for the full range of uncertainty), using the data from (15). The thermal conductivity of highly porous media depends more on the porosity and on the contact area between the grains than on the bulk thermal conductivity of the matrix material (15, 16).

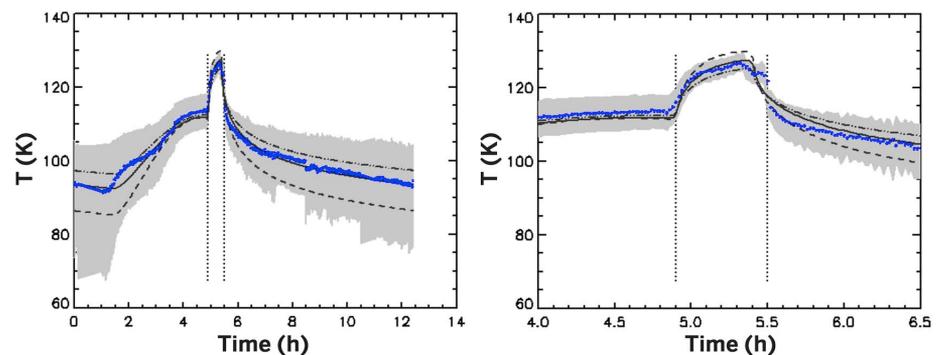
The MUPUS-PEN probe was nominally commanded to start the hammering sequence 40 min after it had been deployed. The depth-of-penetration sensor, DS, measured the progress of the hammering. The hammering was also recorded by the three accelerometers of the Surface Electrical, Seismic and Acoustic Monitoring Experiment (SESAME) installed in the feet of the lander (17). The DS recorded an initial progress of  $\sim 27$  mm, and then its readings oscillated for 3.5 hours by a total of 10 to 15 mm, indicating no net progress on penetration (Fig. 3). The rapid initial penetration could have been through a thin layer of dust, but this is speculative in the absence of precise knowledge of the initial height of the PEN tip above the ground and other independent evidence for a dust layer at Abydos. Hammering started with the lowest energy setting (Table 1 and

supplementary materials). Because progress measured by the DS was smaller than a threshold value of 1.7 mm, the energy level was increased by one level after the other and had been increased after a total of 56 strokes to its maximum, where it remained for 3.1 hours. The evidence for failure to penetrate comes foremost from the recording of the DS but is supported by the temperatures measured along the PEN (fig. S4). These temperatures follow the temperature changes recorded by the thermal mapper, in particular, when the environment is warmed by indirect light.

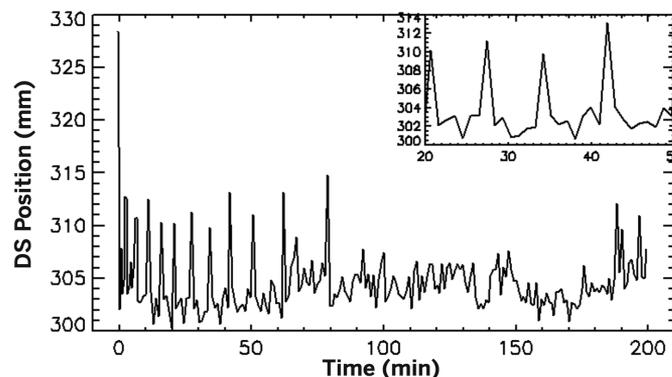
The lack of progress into the subsurface can be interpreted as being caused by a near-surface layer of a strength the PEN was not capable of penetrating. Alternative interpretations invoke malfunctioning of MUPUS-PEN but are not independently confirmed. These are discussed in the supplementary materials. It is very probable that the mechanism worked nominally at least for three of the four levels. For level 4, housekeep-

ing data suggest that hammering occurred only once per four-stroke sequence, thus at a rate of only a quarter of what was designed. This indicates a lack of full synchronization between charging of the capacitor and release of the hammer, and it is possible that the hammer mechanism could not use the full energy of level 4. A very conservative estimate would then assume that the PEN hammer worked only at level 3. From a comparison with calibration data collected in Table 1, we conclude that the material must have provided a resistance to penetration by the PEN of more than 4 MPa, which is equivalent to a uniaxial compressive strength of the material of about 2 MPa.

An independent estimate of the strength can be made by using the efficiency  $\chi$  of the hammer mechanism of 10% and taking the downward movements of the hammer tip  $\delta$  of  $\sim 3$  mm recorded by the DS as deformation of the surface (the stronger upward movements interpreted as recoil). With energy  $E$  stored in the capacitor



**Fig. 2. Variation of temperature during a comet day at Abydos.** The temperature record (blue) was synthesized from 3 days of radiometer data. (Left) The diurnal variation. (Right) The temperature during a 40-min direct illumination of part of the FOV of the thermal mapper. The gray area indicates the  $2\sigma$  uncertainty estimate. The model calculations are for a thermal inertia of  $85 \text{ J m}^{-2} \text{ K}^{-1} \text{ s}^{-1/2}$  (solid line), a ratio between stray light and direct illumination of  $\beta_0 = 0.32$ , and 69% of the FOV illuminated. The dashed line is for  $50 \text{ J m}^{-2} \text{ K}^{-1} \text{ s}^{-1/2}$ ,  $\beta_0 = 0.27$ , and 46% of the FOV illuminated, and the dash-dotted line is for  $120 \text{ J m}^{-2} \text{ K}^{-1} \text{ s}^{-1/2}$ ,  $\beta_0 = 0.35$ , and 80% of the FOV illuminated. Details of the calculation are provided in the supplementary materials.



**Fig. 3. Displacement of the MUPUS-PEN depth sensor (DS).** The sensor records the progress of penetration with MUPUS-PEN. There is a clear downward motion of 27 mm at the beginning, followed by oscillatory displacements by 10 to 15 mm, followed by smaller displacements. The reason for the reduction in amplitude after time ( $t$ ) = 80 min is not understood. One possibility is that the barbs at the tip of the PEN locked to the ground. Overall, it appears as though the PEN was hammering more or less on the spot (but not necessarily at exactly the same spot), with indentations of a few millimeters and recoils of up to 10 mm.

**Table 1. PEN hammer calibration data.** The table collects PEN hammer calibration results in three foam glasses of differing strength. Foam glasses T4 and F are commercially available. Foam glass SRC was produced at Space Research Centre (SRC) Warsaw for the prelaunch calibration measurements. The samples were kept for reference at SRC Warsaw. Listed are the uniaxial compressive strengths as given by the manufacturers for foam glasses T4 and F, and the results of control measurements done at Technische Universität (TU) Graz in 2015 for foam glasses F and SRC along with a value calculated for T4 (22) using data of a shear deformation measurement. Also given is the static penetration resistance measured at SRC Warsaw (supplementary materials).

	Foam glass T4	Foam glass F	Foam glass SRC
Compressive strength (MPa) (nominal by manufacturer)	0.85	1.70	—
Uniaxial compressive strength (MPa)	0.23*	0.52 <sup>†</sup>	2.11 <sup>†</sup>
Static penetration resistance per unit area of pile (MPa) (SRC, 2015)‡	0.52 ± 0.09	1.24 ± 0.32	4.19 ± 1.05
PEN hammer calibration results			
Progress per four hammer strokes (mm)			
Level 1, 0.49 J	2.1		
Level 2, 1.59 J	4.8	2.6	
Level 3, 2.17 J	8.3	4.4	0.3
Level 4, 4.23 J			2.0

\*From Kömle *et al.* (22). †TU Graz, 2015.

‡Average values from four measurements are described in more detail in the supplementary materials, each with the same sample; error estimates are 2σ.

The static penetration resistance per unit area is the strength of a material into which a pile is driven. The compressive strength is measured by placing a sample cylinder between two plates of the same radius. For a homogenous, isotropic medium and a thin pile, the static penetration resistance per unit area should be twice the uniaxial compressive strength for geometrical reasons of stress propagation. The table further gives the rate of penetration progress in millimeters per four hammer strokes at the four energy levels of the hammer mechanism. The energy stored in the capacitor of the mechanism is listed per level. The efficiency of the PEN mechanism, defined as the ratio of deformational energy to the energy stored, was found to be ~10%.

(Table 1) and an opening angle of the PEN tip  $\alpha$  of 28.5°, the force per unit area of tip surface to overcome the strength is  $\sigma = \chi E \cos^2 \alpha / \delta^2 \sin \alpha$ . Considering only energy level 3, we find a value of 7 MPa. Given the uncertainty of the exercise—in particular, in the deformation  $\delta$ —we take this value as a confirmation of the above lower bound of the resistance to penetration of 4 MPa.

Deep Impact crater observation for comet Tempel-1 resulted in a tensile strength estimate of <12 kPa (18). Observation of cometary meteoroids suggest tensile strengths of ~10 kPa for particles that originated from pristine comets and up to 80 kPa for those from evolved comets (such as taurids from 2P/Encke) (19). Tensile strengths are typically at least one order of magnitude smaller than compressive strengths (20).

Laboratory data on the strength of ice and ice dust mixtures are rare at relevant temperatures as measured at Abydos. Granular ice of 1 mm grain size has a compressive strength of 60 to 70 MPa at 100 to 150 K (21), which is an order of magnitude larger than our lower bound. The static penetration resistance of sintered porous ice with an initial porosity of 73% is 10 MPa at 220 K, whereas the static penetration resistance of sintered CO<sub>2</sub> ice with an initial porosity of 48% is 6.5 MPa at 193 K (22). Moreover, sintering of highly porous ice during the Comet Simulation (KOSI) experiments (23–25) resulted in a penetration resistance of 5 MPa (24). These values compare quite well with our estimates and with our independent estimate of the porosity from the MUPUS-TM data. According to a comet thermal evolution model, sintering can result in a strong near-surface layer of a comet nucleus (26) but requires the grains to be tens of micrometers in radius, or smaller. Thus, high strength suggests that the material is at least locally fine-grained.

Both the thermal inertia and the strength on the surface of 67P are larger than commonly thought. In particular, our lower bound on the strength of the subsurface material is larger than previous estimates from the stability of large-scale features both on 67P (27) and on other comets. The reason may lie with layering or with large-scale cracks in the nucleus that may render parts of it unstable. From our data, we envisage the nucleus as a low-thermal conductivity, highly porous body with a near-surface layer consisting of sintered ice-dust with substantial local strength. The layer could be covered by a thin layer of dust of low strength. The estimated porosity is consistent with earlier models of comet nucleus formation (28, 29).

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#### SUPPLEMENTARY MATERIALS

[www.sciencemag.org/content/349/6247/aab0464/suppl/DC1](http://www.sciencemag.org/content/349/6247/aab0464/suppl/DC1)  
Materials and Methods  
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