

Pulse Contour Methods to Estimate Cardiovascular Indices in Micro- And Hypergravity

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Background: The importance of noninvasive health monitoring in space increased as a result of the long-duration missions on the International Space Station (ISS). In order to monitor changes in cardiovascular indices such as cardiac output (CO) and total peripheral resistance (TPR), many methods have been developed using signal processing and mathematical modeling techniques. However, their performance in various gravitational conditions has not been known. **Methods:** The present study compared 10 methods to estimate CO and TPR by processing peripheral arterial blood pressure signals recorded from 8 subjects in multiple gravity levels (1 G, 0 G, and 1.8 G) during parabolic flights. For reference data sets, CO and TPR were simultaneously obtained by an inert gas rebreathing technique. Root normalized mean square errors and Bland-Altman plots were used to evaluate the estimation methods. **Results:** The corrected impedance method achieved the lowest estimation errors (20.0% CO error and 23.5% TPR error) over the three gravity levels. In microgravity, mean arterial pressure was also demonstrated to be an indicator of CO (24.5% error). **Discussion:** The corrected impedance method achieved low estimation errors for a wide range of the gravity levels. Gravity-dependent performance was observed in the mean arterial pressure method that achieved low errors in the short-term 0 G.

Keywords: inert gas rebreathing, parabolic flight, cardiac output, total peripheral resistance.

THE IMPACT OF SHORT and long-lasting weightlessness on the cardiovascular system, especially presyncope and fainting of astronauts after spaceflight missions (postflight orthostatic hypotension or orthostatic intolerance), has been in the focus of cardiovascular research for decades. It has been found that postflight orthostatic intolerance is caused by changes in cardiac output (CO) and vasoconstriction deficiencies before and after spaceflight (17,19). As human spaceflight entered the era of long-duration missions on the International Space Station (ISS), the importance of noninvasive health monitoring has increased in order to track changes of the cardiovascular indices and find any sign of deconditioning during and after spaceflight.

The noninvasive cardiovascular monitoring in spaceflight includes infrared finger photoplethysmography (IFP) during former Space Shuttle and Russian MIR space station missions as well as ISS missions (3,4,10). The recorded peripheral arterial blood pressure (ABP) signal can be processed to track changes in CO and total peripheral resistance (TPR). So-called pulse contour methods (PCMs) have been studied by many researchers (9,14,25) to track changes in CO and TPR, and have

been introduced into clinical medicine and physiological research (3,4,21). However, just a few methods are currently used in clinical medicine on a regular basis (22). For example, the corrected aortic input impedance method introduced by Wesseling et al. is used for stroke volume (SV) estimation by pulse wave analysis (3). However, ground-based artificial gravity studies have shown that the model flow method, which was developed from the corrected impedance method, achieves different reliabilities for measurements in different body positions (6). Furthermore, the impact of microgravity on the performance of PCMs is not known. The purpose of this study was, therefore, to compare PCMs using noninvasive beat-to-beat finger blood pressure in various gravity conditions.

METHODS

Equipment

Cardiovascular data sets of noninvasive ABP, heart rate (HR) by electrocardiography, and CO were simultaneously collected during the parabolic flight campaigns of the German Aerospace Center (DLR) in 2010–2012 in Bordeaux, France, and the French Space Agency Centre National d'Etudes Spatiales during the 2011 Paris Le Bourget Air Show. All flights were performed by the NOVESPACE Company using an Airbus A300. The Finometer MIDI[®] system (Finapres Medical Systems, Amsterdam, The Netherlands) for blood pressure measurement, the Innocor[®] rebreathing system (Innovision A/S, Odense, Denmark) for obtaining cardiac output (CO_{REB}), and the Biopac[®] system (Biopac Systems, Goleta, CA) for data acquisition were used. The raw data of ABP and HR were stored via ACQ[®] software

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(Biopac Systems). The details of the in-flight experimental setup has been described previously (15).

Subjects

In short, ABP and HR data were continuously recorded throughout the flights at a 200 Hz sampling rate from eight healthy subjects in the standing position (four women, 30 ± 3 yr, 167 ± 7 cm, 61 ± 18 kg; and four men, 35 ± 9 yr, 173 ± 9 cm, 66 ± 10 kg). All the test subjects had experienced parabolic flights previously. They received scopolamine-hydrobromide injected subcutaneously as a countermeasure for motion sickness before the flights [175 µg (men); 125 µg (women)]. The study protocols had been approved in advance by the pertinent French authorities (Agence française de sécurité sanitaire des produits de santé). Each subject provided written informed consent before participation.

Procedure

The following PCMs were applied to the aforementioned parabolic flight ABP data.

Mean arterial pressure: This method is one of the most simple estimators. CO is proportional to mean arterial pressure (MAP):

$$CO \propto MAP = \frac{1}{T} \int P(t) dt$$

where T is the beat duration and P(t) is ABP.

Pulse pressure (PP) (7):

$$CO \propto \sum_i \frac{PP_i}{T_i} = \sum_i \frac{SBP_i - DBP_i}{T_i}$$

where i represents the beat number, and SBP_i and DBP_i represent systolic and diastolic blood pressure values of the beat, respectively. Taking DBP into consideration, this method regards the difference of SBP and DBP as an indicator of CO. The PP method is simple and one of the most intuitive and arguably most commonly used in clinical settings (5).

Herd's pulse pressure (PP2) (9):

$$CO \propto \sum_i \frac{MAP_i - DBP_i}{T_i}$$

In the aforementioned PP method, SBP was replaced by MAP, which is known to be robust against pressure waveform distortion caused by the tapered and bifurcated arterial tree structure.

Modified Herd's method (2):

$$CO \propto \sum_i \frac{\int_{Systole} P_i(t) dt - DBP_i}{T_i}$$

This method uses only the systolic ABP signal in the Herd's method.

Liljestrand-Zander's method (14):

$$CO \propto \sum_i \frac{SBP_i - DBP_i}{SBP_i + DBP_i} \Big/ T_i$$

This method adds a scaling factor of 1/(SBP + DBP) to the PP method.

Area under the systolic pressure curve:

$$CO \propto \sum_i \frac{\int_{systole} P_i(t) dt}{T_i}$$

Rather than taking the average of an entire single beat, this method uses only the systolic pressure signal to obtain proportional CO. This method overcomes the disadvantage of the MAP method's tendency to underestimate CO when diastolic period is abnormally extended, regardless of the systolic period.

Area under the systolic pressure curve above DBP:

$$CO \propto \sum_i \frac{\int_{systole} (P_i(t) - DBP_i) dt}{T_i}$$

Only the ABP signal above DBP is considered.

Corrected impedance (25):

$$CO \propto \sum_i \frac{(163 + HR_i - 0.48 \cdot MAP_i) \int_{t_i^{ED}}^{t_i^{ES}} (P_i(t) - DBP_i) dt}{T_i}$$

where t^{ED}_i and t^{ES}_i represent time stamps at the end diastole and end systole of the ith beat, respectively.

Kouchoukos correction (13):

$$CO \propto \sum_i \frac{\left(1 + \frac{T_i^S}{T_i^D}\right) \int_{t_i^{ED}}^{t_i^{ES}} (P_i(t) - DBP_i) dt}{T_i}$$

where T^S and T^D represent systolic and diastolic durations, respectively.

AC power: Adopted by the commercial LiDCO Plus PulseCO method of pulse power analysis (20; LiDCO Ltd., London, UK), this makes use of the power of the ABP signal. The beat power factor is proportional to the nominal CO ejected into the aorta.

$$CO \propto \sqrt{\frac{1}{T} \int_T (P(t) - MAP)^2 dt}$$

Some of the CO estimation methods require identification of an end systolic time stamp. In this section, methods to identify the end systole from the ABP signal are introduced.

Exponential model: Weissler et al. (24) obtained the relationship between systolic duration and preceding RR interval, describing it as a saturating exponential curve. For the present study, the following equation was adopted to identify the systolic duration of the current beat (2):

$$Sys_i = 436 \left(1 - \exp(-0.0057 RR_{i-1}^{measured})\right)$$

Partial pulse pressure model (1): An end diastole always comes after a systolic peak. At the end systole, the pressure value is equal to or lower than SBP. When the pressure drops from SBP to α% PP at the end systole, the end

TABLE I. CARDIOVASCULAR DATA OBTAINED DURING CO REBREATHING MEASUREMENTS IN $N = 8$.

Subjects	CO _{REB} (L · min ⁻¹)				ABP (mmHg)				HR (bpm)				TPR [mmHg/(L/min)]			
	Max	Min	Mean	SD	Max	Min	Mean	SD	Max	Min	Mean	SD	Max	Min	Mean	SD
AA	9.94	4.29	7.47	2.44	143	63	87.8	13.3	104	34	67.6	20.4	21	9	12.6	3.3
AO	5.90	2.40	4.37	1.40	136	29	71.7	16.8	105	57	85.6	11.1	39	10	18.3	7.7
AM	8.55	3.06	5.27	2.35	205	45	94.2	25.0	180	25	100.0	32.7	35	12	20.9	7.2
BX	14.90	4.20	7.95	3.94	154	41	78.3	17.7	180	47	109.6	22.2	18	6	11.4	3.9
CC	11.41	5.06	7.10	1.76	176	60	92.1	17.5	180	64	120.5	27.7	21	7	13.8	4.6
AD	14.29	4.59	7.30	4.29	182	45	81.7	19.0	160	53	108.7	26.7	18	6	12.5	3.6
AX	11.34	4.66	7.42	2.04	212	53	104.2	25.5	180	25	122.7	19.0	23	9	15.1	4.6
BR	12.29	3.64	7.18	2.62	183	46	94.7	20.8	128	62	91.2	12.7	25	7	14.9	5.7

systolic pressure can be described as $P_{ES} = P_D + \alpha (P_S - P_D)$, where P_{ES} is the time stamp of the estimated end systole. The value of α was changed from 10 to 100% PP and applied to the CO estimation methods that require end systole identifier.

Statistical Analysis

We applied the aforementioned 10 PCMs to the parabolic flight ABP data after the experiments using MATLAB® (MathWorks, Natick, MA). The ABP signal during each CO rebreathing measurement (10 s) was processed. First, peaks in the ABP signal and their preceding local minima were determined as SBP and DBP. The signal between DBPs defines a single beat. The algorithms were applied to calculate SV on a beat-by-beat basis. Then the total SV over time was calculated as a proportional CO estimate.

Note that all the PCMs provide proportional CO; i.e., the outputs are estimates within a scaling factor. Assuming arterial compliance does not change during testing, in each subject, the proportional CO estimates were scaled as

$$C_a = \frac{\text{mean}(\text{meas})}{\text{mean}(\text{estimated})}$$

The scaling factor was set to be consistent within each subject (1).

Using the estimated CO and measured MAP, TPR was also estimated by Ohm’s Law: $TPR = MAP/CO$. The estimated CO and TPR values were evaluated by

comparing with the corresponding reference CO (CO_{REB}) obtained by Innocor®. The reference TPR (TPR_{REB}) was also calculated by Ohm’s Law: $TPR_{REB} = MAP/CO_{REB}$. As an error criterion, the root normalized mean square error (RNMSE) was adopted:

$$RNMSE = 100 \sqrt{\frac{\sum_{n=1}^N \left(\frac{Meas - Est}{Meas} \right)^2}{N - N_f}}$$

where Meas, Est, N, and N_f represent a measured value, estimated value, number of sample, and number of freedom (N_f = 1, arterial compliance), respectively. The method that achieved the lowest RNMSE was compared with the other methods using the F-test. The statistical significance was defined as $P < 0.05$.

RESULTS

Table I shows an overview of the CO_{REB}, ABP, HR, and TPR characteristics of the eight subjects analyzed. Large interindividual differences are obvious, especially in the ranges of CO_{REB}, which are larger than those typically seen in hospitalized patients. We analyzed 139 CO data sets, of which 52 sets were collected within 0 G, 28 sets in 1.8 G, and 59 sets in 1 G. The overall results are summarized in Table II, showing that most of the methods generated their largest errors in short-term 0 G and the smallest in short-term 1.8 G.

Fig. 1A summarizes the CO errors by different methods under all tested gravity loads. For methods using

TABLE II. RNMSEs OF CO AND TPR ESTIMATION (%).

Methods	CO RNMSEs				TPR RNMSEs			
	All Gs	1 G	0 G	1.8 G	All Gs	1 G	0 G	1.8 G
Wesseling’s corrected impedance (25)	20.0	19.2	27.3	16.3	23.5	17.8	30.9	17.3
Kouchoukos (13)	21.9	19.4	29.2	18.2	31.0	18.7	41.8	28.1
Area under the curve, above DBP	22.3	20.3	26.0	18.7	27.4	19.0	35.1	26.4
Modified Herd’s method (2)	22.4	21.0	26.8	18.8	26.4	19.6	34.7	20.0
Area under the curve	24.7	21.5	30.3	26.1	24.3	20.8	27.7	24.4
Herd’s pulse pressure (9)	25.0	24.4	29.1	24.9	31.4	22.6	41.4	25.4
AC power (20)	25.7	22.9	27.8	16.7	28.3	21.4	38.3	16.9
Pulse pressure	28.7	25.6	29.4	35.1	33.0	23.1	45.9	19.1
Liljestrand-Zander’s method (14)	29.2	25.3	25.5	18.1	30.8	24.5	40.4	20.3
MAP	33.3	26.5	24.5	28.6	34.9	24.8	44.4	32.6

end systolic time stamps, the end systolic identifier that provided the lowest RNMSEs is shown. Among the methods, corrected impedance with 60% PP as end systole achieved the lowest CO RNMSE (20.0%). The 1-G loading scenario (Fig. 1B) yielded similar results. Fig. 1C shows the RNMSEs during 0 G. The MAP method achieved the lowest RNMSE of 24.5%. Fig. 1D shows the RNMSEs during 1.8 G. The corrected impedance method achieved the lowest RNMSE of 16.3%.

The CO estimation history of the corrected impedance method compared to $\dot{C}O_{REB}$ is shown in Fig. 2A, demonstrating the traceability of changes of CO by the corrected impedance method over the wide range of measured CO and gravity levels. Kouchoukos (60% PP as end systole identifier), area under the curve above

DBP (60% PP as end systole identifier), and modified Herd's (using an exponential model) achieved 21.9%, 22.3%, and 22.4% RNMSEs, respectively. Other methods, especially the methods that do not use end systolic time stamps, were found to be statistically larger in RNMSEs (Fig. 1), including the Liljestrand-Zander method (29.2%, CO estimation history shown in Fig. 2B).

As for TPR estimation, the corrected impedance method achieved 23.5% RNMSE (Fig. 3A), while the Liljestrand-Zander method achieved 30.8% RNMSE (Fig. 3B). Bland-Altman plots of the Liljestrand-Zander and the corrected impedance methods are shown in Fig. 4. The corrected impedance method showed smaller correlation coefficient and 95% limits of agreement [$R^2 = 0.003$ and ± 2.73 mmHg/(L/min), respectively,

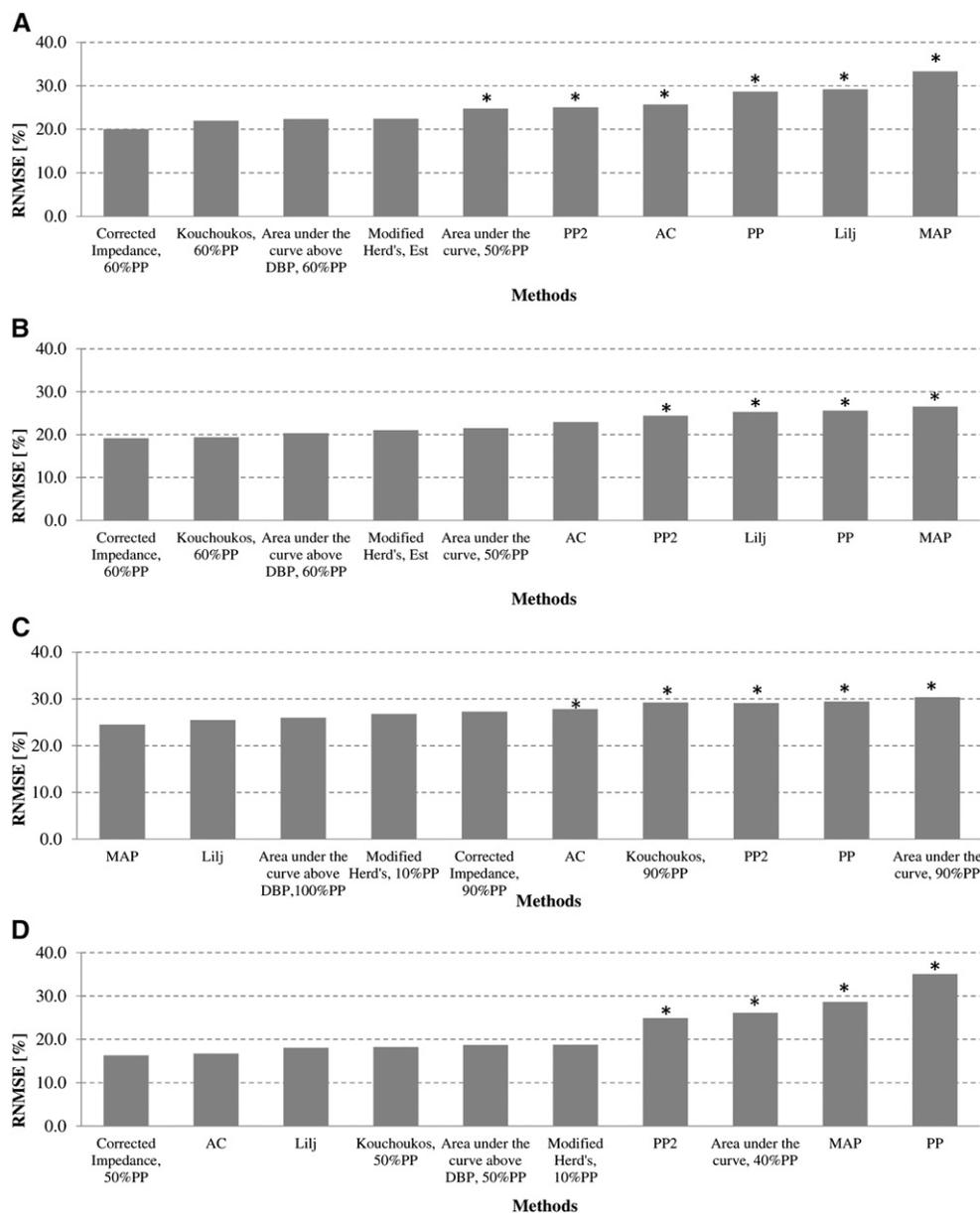


Fig. 1. A) RNMSEs of the CO estimation methods for all the gravity levels. B) RNMSEs of the CO estimation methods in 1 G. C) RNMSEs of the CO estimation methods in 0 G. D) RNMSEs of the CO estimation methods in 1.8 G. Asterisks represent significant statistical differences ($P < 0.05$) regarding the best method under the particular gravity load.

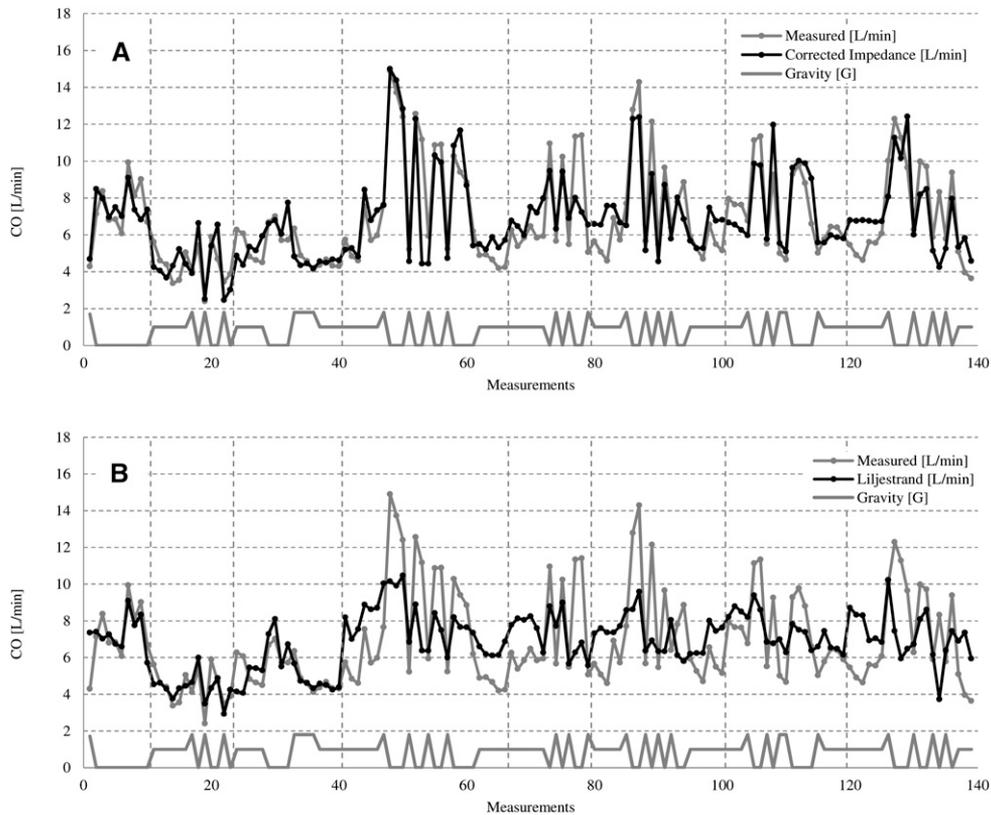


Fig. 2. A) CO estimation history by the corrected impedance method using 60% PP as end systole. B) CO estimation history by the Liljestrand-Zander method.

shown in Fig. 4B] than those of the Liljestrand-Zander method [$R^2 = 0.020$ and ± 4.12 mmHg/(L/min), respectively, shown in Fig. 4A], indicating independency from the physiological range of true CO values. Similar trends can be seen in those of TPR estimation (Figs. 4C and D).

DISCUSSION

Finger blood pressure waves obtained during parabolic flights within wide physiological ranges were processed using CO estimation methods and including different methods of end systole identification. There were 10 such estimation methods assessed against cardiac output determined by foreign gas rebreathing. The corrected impedance, Kouchoukos, area under the curve (above DBP), and the modified Herd’s methods achieved the lowest RNMSEs among all 10 analyzed methods.

The high RNMSEs of the PP method could be attributed to their sensitivity to ABP waveform distortion; SBP tends to increase as the pulse wave travels through the tapered and bifurcated arterial tree. In the meantime, DBP and MAP are known to be robust against distortion. For example, the corrected impedance method and Kouchoukos correction method are based on the area under the curve method, but adopted distortion-robust scaling factors to achieve high estimation accuracy. The corrected impedance method adopted HR and MAP as scaling factors, while the Kouchoukos correction method used the ratio of systolic and diastolic durations.

The error of the MAP method stems from the assumptions of constant TPR. Interestingly, however, the MAP method achieved low error in 0 G (Fig. 1B) with respect to the other methods, which could be attributed to the baroreceptor response induced by the headwards fluid shift; likely the sympathetic system was inhibited excessively, resulting in the saturated and constant vascular response.

Herd’s pulse pressure method (PP2) overcame the shortcoming of the PP method by using MAP and DBP, which are both robust against waveform distortion. However, the method is sensitive to variability in the diastolic periods. For example, if SV values are constant for several beats while diastolic periods start to decrease, MAP would decrease and SV values would be underestimated. In that light, the modified Herd’s method was developed to overcome the weakness of Herd’s pulse pressure method. This method takes into account only the systolic period. Since any abnormally shortened or prolonged diastolic periods (that do not contribute to SV or CO) are excluded, better estimation accuracy was expected. It was also found that the modified Herd’s method is relatively insensitive to end systole identification methods (the exponential model or partial PP methods) (2).

Although the Liljestrand-Zander method had been reported by Sun et al. to work best in the data sets of patients on intensive care units (ICU) (21), the method did not achieve low RNMSEs in the present study, especially

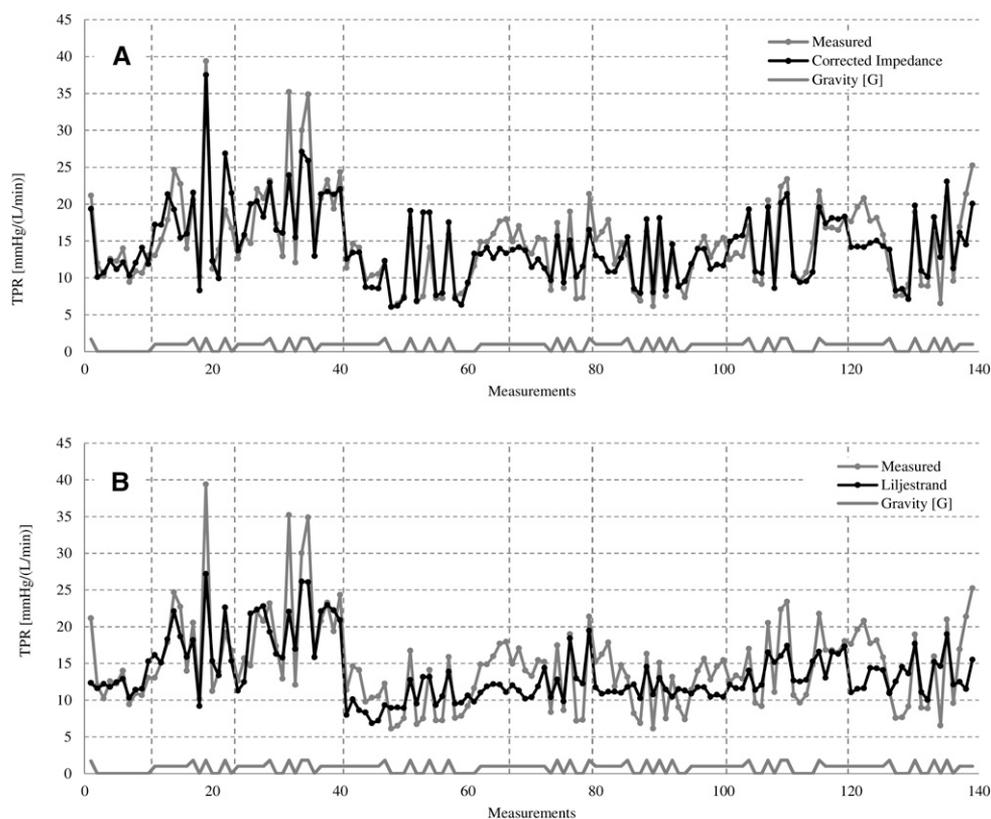


Fig. 3. A) TPR estimation history by the corrected impedance method. B) TPR estimation history by the Liljestrand-Zander method.

in 1 G and 1.8 G. The reason could be attributed to stable ICU patient data sets and the averaging effect of the method; the Liljestrand-Zander method normalizes PP by a sum of SBP and DBP. Therefore, it tends to provide relatively flat and stable CO estimates. In the ICU setting, cardiovascular indices, such as CO and ABP, of patients are carefully maintained. Thus, the averaging effect of Liljestrand-Zander favorably resulted in low RNMSEs. On the other hand, a wide range of CO and ABP, as can be seen in the present study, would challenge the method. The German physiologist Gauer pointed out that this relationship leads to good results if changes in CO are mainly the result of changes in HR (8). The Liljestrand-Zander formula was often criticized for not taking changes of elasticity and other parameters into account (8). During a parabolic flight maneuver, not only large HR changes, but also exaggerated changes in blood pressure and TPR can be observed (16).

In 0 G, higher PP values (90% or 100% PP) tended to be selected as the indicator of end systole than in other gravity scenarios. These PP values correspond to the beginning of the ABP descent immediately after SBP. This could be explained by early aortic valve closures and shortened systolic phases in the cardiac cycle in 0 G with respect to 1 G and 1.8 G. However, a shortened systolic phase in 0 G would not be well in line with the observations of Johns et al. (11), who found an increased left ventricular ejection time (LVET) in 0 G with respect to 1.8 G using ultrasound measurements. Contradictory to the findings of Johns et al. are the findings of Mukai et al.

(18). They used impedance cardiography to evaluate LVET during gravity transitions in the standing position on parabolic flight. They were not able to find a significant change in LVET during the 0-G phase with respect to the initial 1.8-G phase. From our point of view it is not clear yet if higher PP values as an end systole indicator in microgravity are just a methodical adjustment or correlate with a true change in LVET.

In 1.8 G, the corrected impedance method achieved the lowest RNMSEs of 16.3% in CO and 17.3% in TPR. During the microgravity phases, however, it resulted in high RNMSEs. The higher errors could be attributed to the rapid decrease in TPR; acute changes in TPR are known to occur in weightlessness during spaceflight missions and on parabolic flights (16), and low TPR in 0 G might have resulted in the low accuracy of the corrected impedance method (6). The other PCMs also resulted in higher RNMSEs in 0 G, which could be explained by the decreased performance of PCMs in general during low TPR values (12). PCMs assume constant blood volume in the arterial system, while fluid shift between the venous and arterial systems occurs upon a rapid decrease in TPR. Estimation errors would decrease once the transient fluid exchange between the systems is stabilized in a long-duration space mission. In considering the effect of TPR changes, locations of ABP measurement could also influence the results. A lack of agreement of arm and finger ABP was reported during spaceflight (23). The larger brachial arteries could be less subject to TPR changes than the smaller

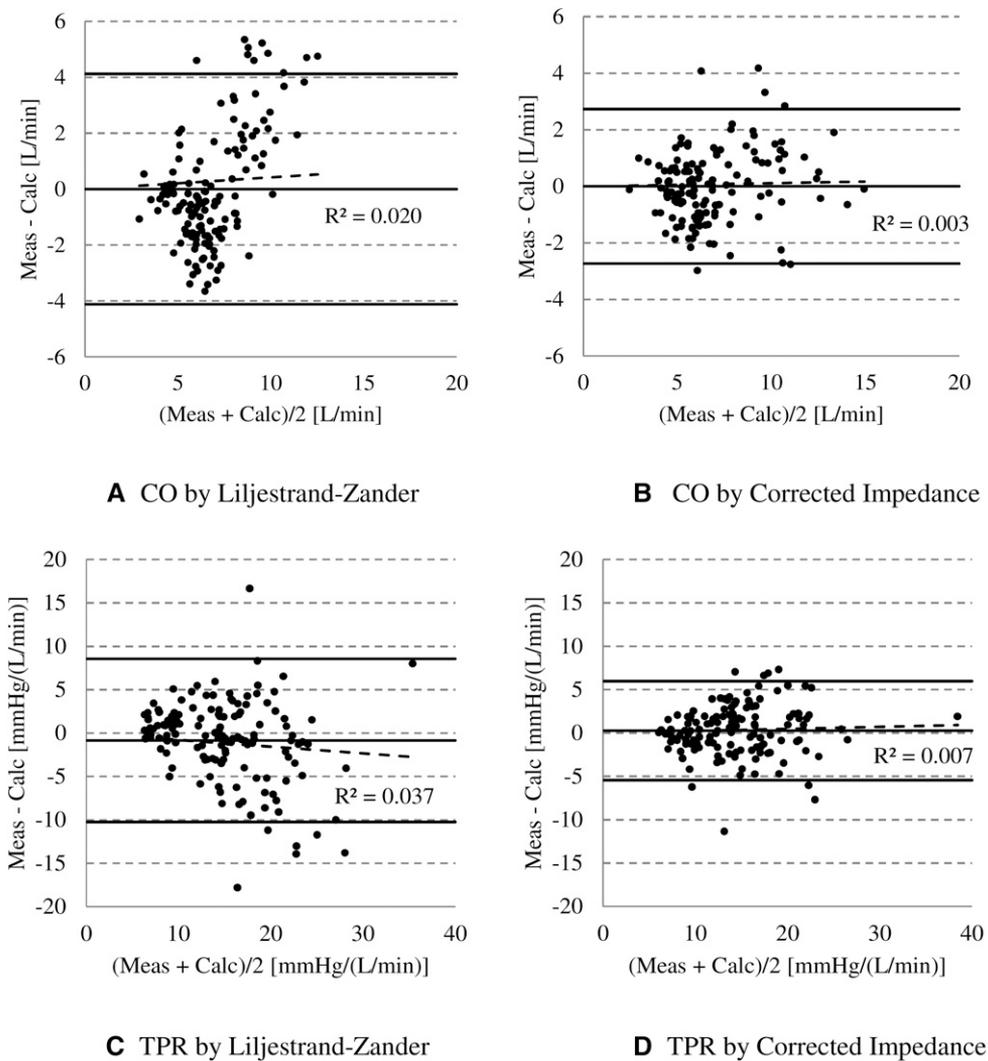


Fig. 4. Bland-Altman plots of the Liljestrand-Zander and corrected impedance methods. A) CO by Liljestrand-Zander, $R^2 = 0.020$. B) CO by corrected impedance, $R^2 = 0.003$. C) TPR by Liljestrand-Zander, $R^2 = 0.037$. D) TPR by corrected impedance, $R^2 = 0.007$.

radial arteries. Comparison of PCMs using brachial and radial arteries during parabolic flight or spaceflight would reveal the robustness of each method in response to acute changes in TPR.

To summarize, we report for the first time comparison of 10 different estimation methods of CO by processing peripheral arterial blood pressure signals under the changing gravity conditions of parabolic flights. Our main findings are: 1) changing performance of each pulse pressure estimation method was observed under changing G loads; 2) the corrected impedance method worked best on average in all tested G loads; 3) surprisingly, MAP showed the best performance of all tested methods in short-term 0 G; and 4) most of the methods showed the lowest errors in 1.8 G and the highest errors in 0 G. These preliminary results suggest that using multiple PCMs, rather than a single PCM, would be advantageous in analyzing cardiovascular systems under varying G-loads. More precisely, using the corrected impedance method for blood pressure data taken in 1 G and short-term 1.8 G, and the MAP method for the data

in short-term 0 G might decrease the overall error of CO estimation.

We acknowledge the following limitations of the study: the sample size ($N = 8$) was small due to the restriction imposed by the number of parabolic flight test subjects. The phases of different G loads lasted just few seconds and further studies are necessary to compare the estimation methods during long-duration spaceflight missions. The accuracy of the CO and TPR reference method as well as the noninvasive IFP were limited (15), which might result in the large errors of all the estimation methods ($> 20\%$) under the changing gravity conditions. Therefore, conclusions from analysis of IFP data should be drawn carefully. The most accurate cardiovascular monitoring techniques would be invasive blood flow and pressure measurement, such as an ultrasound flow probe and a catheter pressure sensor. Nevertheless, inert gas rebreathing and IFP are well-established, safe, and regularly used methods of reference CO determination and blood pressure measurement on spaceflight missions and parabolic flights. Further tuning of

the algorithm parameters in using IFP would increase the estimation accuracy. Future work should also include application of the PCM methods to ABP data sets recorded during a long-duration spaceflight on ISS. Due to the stabilized arterial blood volume in 0 G, lower estimation errors are expected.

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