Evaluation of Methods for Measuring Particulate Matter Emissions from Gas Turbines

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Supporting Information

1. INTRODUCTION

Concerns on potential impacts of aviation particulate matter (PM) emissions on Earth’s climate and human health1 has stimulated the development of new measurement methodologies for PM emission certifications for aircraft engines.2 PM emissions consist of volatile particles (do not exist in the condensed phase at T = 350 °C) which form in the expanding and cooling plume downstream the engine, and of nonvolatile combustion particles (exist as particulates at T = 350 °C) which form inside the engine.3 One key property governing particles’ impact on climate via contrail formation and aerosol cirrus interaction is the number of nonvolatile particles4 while studies focusing on the impact of aircraft emissions at ground on air quality show the importance of sub-20 nm sized volatile particles.5–7

The engine emissions databank of the International Civil Aviation Organization ICAO (www.caa.co.uk/) lists emission factors for gaseous species in units of gram per kg of burnt fuel. PM emissions, however, are reported as smoke number (SN), which relates the darkening of particle-loaded filters to the mass of deposited PM.8 SN does not measure mass, nor is it intended to include volatile particulate matter. New methodologies for replacing the SN method focus on engine exit plane measurements of nonvolatile particles only because combustion-related particles are closely linked to engine properties. Volatile PM is excluded in the current stage because their formation depends crucially on fuel properties and ambient conditions.

An overview of techniques available for measuring nonvolatile PM emissions from aircraft engines was prepared by the SAE...
2. EXPERIMENTAL APPROACH

2.1. Rig Description. Particle emissions were generated by a gas turbine engine simulator composed of a combustor and a unit to simulate a 3-shaft turbine section (so-called hot end simulator; HES). This particular assembly was developed and successfully applied during the EU project PARTEMIS. The representative HES PM emissions for aircraft gas turbine emissions was evaluated. Here, the HES served as a robust source for simulations gas turbine exhaust PM. Aviation grade kerosene Jet A-1 with fuel sulfur content (FSC) of 0.030 wt-% (weight-%) was used.

The exhaust gas flow was transported through temperature-controlled pipes which were kept above 160 °C on gas analysis lines and controlled at 70 °C on heated sections of PM sampling lines. The exhaust gas was pretreated in a hot dilution system for removing the majority of volatile PM. The hot dilution system was constructed of a DEKATI pressurized dilution air heater and ejector diluter (DI-1000) which was operated at 400 °C and diluted the sample by a factor of 10:1. The hot diluter was followed by a 9.525 mm (3/8 in.) line of 2655 mm length kept at room temperature. This method was adopted to avoid as much as possible any water and gaseous compounds being absorbed by the filter matrix during sampling. Prior to any measurements on filter samples a known mass was weighed 10 times to exercise the balance and determine confidence limits. Known errors associated with this technique are about ±10%.

Filter samples for 2-step combustion (2-SC) were collected on preconditioned quartz fiber filters (47 mm Ø, Pallflex—Tissue quartz, Pall Life Sciences). During sampling the flow through the filters was fixed by a critical orifice providing a constant volumetric flow rate of 10.7–11.0 L min⁻¹. 2-step combustion without HCl fumigation analyses the carbon content of PM in a two-step combustion process where OC is removed at 340 °C in pure O₂. The remaining carbon, defined as EC, is then determined as CO₂ evolving at 1000 °C (TC error 8%; EC, OC error 20%). Total carbon (TC) is measured from the same sample in a separate single-combustion step at 1000 °C in O₂ while OC is obtained from TC–EC. Besides carbon, organic matter (OM) contains also oxygen and hydrogen which can be approximated by OM ≈ 1.20 × OC for fuels with an O/C ratio of less than 1 wt-%. For the carbonaceous fraction of PM, OC is the appropriate property, whereas OM has to be considered if total mass is targeted.

Aerosol absorption photometry analyzes the modification of filter optical properties as transmittance or reflectance caused by the light-absorbing particles deposited on the filter. The principal measure of any absorption photometer is the aerosol absorption coefficient σₐp given in units of m⁻¹. The conversion of an absorption coefficient into a BC mass concentration requires the assumption of a mass-specific absorption cross-section, B₉C-Multi-angle absorption photometry (MAAP) is an improved version of absorption photometers which uses a multi angle absorption photometer approach combined with a radiation transfer code to analyze the modification of radiation fields in the forward and back hemispheres of a glass-fiber filter caused by deposited particles. The THERMO model 5012 MAAP uses B₉C = 6.6 m²g⁻¹ at λ = 630 nm which was determined from calibration studies. This value is in accordance with B₉C = 7.5 m²g⁻¹ at 550 nm proposed for fresh BC. The standard deviation of the error in BC mass concentration is 12%. In terms of reproducibility the standard deviation is 3%. Laser-induced incandescence (LII) measures the thermal emission (incandescent light) from particles heated by a pulsed laser to temperatures in the range of 2500–4500 K range. Similar to absorption photometry, LII is highly selective for BC only and cannot be used for measuring TM. LII data is converted from the volume fraction to mass concentration by applying the particle material density for EC of 1900 kg m⁻³. In terms of bias, it depends on the knowledge of the absorption function, as does the MAAP. In terms of reproducibility, the standard deviation is 3% as measured by operating two instruments in parallel.

PM emitted from a gas turbine is composed of elemental carbon, organic matter and inorganic species like sulfate (SO₄).
Besides gravimetry, the sum of chemical components offers an alternative for total mass determination. The selected approach follows version 3 of the First Order Approximation (FOA3) for estimating particulate matter emissions from certified commercial aircraft engines.21 The contributing species are determined directly like EC, estimated from measurement data like OM, or estimated from fuel properties like sulfur-containing compounds. The sulfate content of TM originates from the fuel sulfur which is converted to particulate sulfate with an average efficiency \(\varepsilon = 2.4\text{wt}-\%\).21 With FSC = 0.030wt-% (0.30 g kg\(^{-1}\)) for the fuel burned, the sulfate emission index \(E_{I_{SO}}\) in g per kg of fuel burn is

\[
E_{I_{SO}} = \text{FSC} \times \varepsilon \times \frac{\text{MW}_{SO_4}}{\text{MW}_S}
\]

with molecular weights MW\(_{\text{species}}\) of respective species. The core flow \(Q_{\text{core}}\) of air through the aircraft engine combustor in m\(^3\) per kg of fuel burn is required to calculate the exhaust mass concentration of sulfate from the respective emission index. The value of \(Q_{\text{core}}\) is calculated from the combuster air-to-fuel ratio AFR by

\[
Q_{\text{core}} = 0.776 \times \text{AFR} + 0.877
\]

This approximation matches the experimental conditions within \pm 10%, see SI.

As is known from the gravimetric analysis of particle samples from diesel engines,22 sulfate exists in its hydrated form as (H\(_2\)SO\(_4\)\(\cdot\)4H\(_2\)O) for conditions applicable to gravimetry. This fraction of sulfate-associated water has to be considered in the assessment of the sum of the chemical components. Combining all contributions, the mass concentration of hydrated sulfate in the exhaust flow is

\[
\text{H}_2\text{SO}_4 \cdot 4\text{H}_2\text{O} = \text{FSC} \times \varepsilon \times \frac{\text{MW}_{\text{H}_2\text{SO}_4}}{\text{MW}_S} \times \frac{1}{Q_{\text{core}}} \times \left[1 + \frac{4.5\text{MW}_{\text{H}_2\text{O}}}{\text{MW}_{\text{H}_2\text{SO}_4}}\right]
\]

Finally, total particulate matter is calculated from the sum of single components as

\[
\text{TM}_{\text{SUM}} = \text{OM} + \text{EC} + \text{H}_2\text{SO}_4 \cdot 4\text{H}_2\text{O}
\]

The overall error of this approximation method is estimated as 22% based on 8% uncertainty for the TC determination and on 20% uncertainty for the estimation of hydrated sulfate. The latter value is based on the fact that adding or subtracting one H\(_2\)O molecule leads to a variation in hydrated sulfate mass by \pm 10%.

Number concentrations in the exhaust gas were measured by three different models of condensation particle counters (CPC). The applied instruments differed significantly in the minimum detectable particle diameter \(d_{p, \text{min}}\). Two of the CPC instruments are manufactured by TSI Incorporated, Shoreview, MN, (TSI model 3760, \(d_{p, \text{min}} = 14\) nm; TSI model 3010, \(d_{p, \text{min}} = 10\) nm), one CPC is produced by GRIMM Aerosol Technik, Germany (GRIMM model 5.400, \(d_{p, \text{min}} = 5\) nm). Similar instruments were tested for their applicability to measuring automotive engine exhaust PM.23 Since the CPC based instruments cannot distinguish between volatile and nonvolatile particles, volatile particle removal requires thermal pretreatment of the sample as described in Section 2.1 and in the SI.

Particle size distributions were measured by means of electrical mobility spectrometers.24 Two different models were applied:

**Figure 1.** Particle size spectra for all investigated conditions measured with a DMS500 in terms of number (a) and volume (b); the fraction of particles larger than 10 nm in diameter is >90% for investigated conditions C1–C3.

DMS500 manufactured by CAMBUSTION, UK, and TSI model 3090 EEPS, manufactured by TSI Inc. Differential mobility spectrometers separate charged particles according to their electrical mobility. They are widely used in the measurement of diesel engine emissions25 and aircraft engine emissions.5 The mobility diameter was measured with compensation made for the number of charges as suggested in the data processing respective to the DMS500 and the EEPS. The maximum size of particles detectable by a DMS500 is 1 \(\mu\)m in diameter.

The electrical aerosol detector EAD26 reports a measurement of total particle length which corresponds to the sum of all particle diameters present in the probed volume. The method employs diffusion charging of aerosol particles and their subsequent detection by a sensitive electrometer. This diffusion charging produces a nearly linear relationship between particle diffusion diameter and the number of unit charges acquired by particles in the 10 nm–1 \(\mu\)m size range.27,28 Normalizing the EAD signal to the total particle number concentration measured by a CPC may provide another potential method for measuring an average particle size.27,28

**2.3. Data Reduction.** For Condition 1, two tests (Run 1, Run 2) were performed, whereas for Condition 2 and Condition 3, single tests were conducted. Respective runs lasted 03 h 40 min (C1-R1), 02 h 20 min (C1-R2), 06 h (C2), and 02 h 30 min (C3). The following numbers of filter samples were analyzed: C1-R1: three samples each for gravimetry and 2-step combustion; C1-R2: one sample each for gravimetry and 2-step combustion; C2: three samples for gravimetry, 5 samples for 2-step combustion; C3: three samples for gravimetry, 11 samples for 2-step combustion. Since the online instruments operate on different time resolutions, the data reduction was adjusted such that DMS500 and MAAP provided average data for respective filter sampling times while LII and EEPS provided data averaged over the entire condition run times. Data from CPC instruments were converted from 1 Hz to 15 s averages because this time resolution was met by all applied online instruments.

**3. RESULTS**

The exhaust aerosol is characterized by a trimodal size distribution. The number size distribution (Figure 1a) is dominated by one mode centered at 14–15 nm and a second mode centered at 47–59 nm. For the volume size distribution (Figure 1b) the
sub-20 nm mode is negligible, whereas a third mode centered at 320–420 nm contributes significantly. The size of emitted particles depends on operation conditions with particles being largest for high smoke conditions and being smallest for low smoke—low OM conditions. The chemical composition of the emitted PM is characterized by variable OC and EC fractions depending as well on the operation condition. The EC fraction of TC varies from 54% at condition C2 with high OM emissions to 91% at condition C3 with high smoke emissions, see also Table S2 of the SI and ref 10.

Mass measures are defined as follows: $T_{\text{M, GRAV}} = \text{total mass from gravimetry}$, $T_{\text{M, SUM}} = \text{total mass calculated from the sum of chemical components by eq 4,}$ $T_{\text{M, MOB}} = \text{total mass calculated from mobility spectra (DMS500, EEPS) assuming spherical particle shape and an effective particle density of 1000 kg m}^{-3}$ for particles being composed of variable fractions of organic matter and elemental carbon. All mass-based methods are evaluated against the reference gravimetry $T_{\text{M, GRAV}}$. Additionally, MAAP and LII are evaluated against 2-step combustion (EC) because they separate the light-absorbing carbonaceous fraction (BC) from TC. Data of two identical CPC are correlated for assessing the uncertainty in the measured data depending on instrument performance like variations in instrument flow and lower detection diameters. LII measures concentration directly and is independent of flow rate variations. The minimum detectable concentration for LII is approximately $1 \mu g m^{-3}$ but no known lower limit on particle size.

### 3.1. Mass-Based Techniques

Figure 2 compiles the mass concentrations obtained from the applied methods in relation to $T_{\text{M, GRAV}}$ as reference method; numerical data are listed in Table S2 of the SI. Systematic trends are obvious: Mass closure between gravimetric mass and mass calculated from the sum of chemical components is achieved with $T_{\text{M, SUM}} = (1.07 \pm 0.10) \times T_{\text{M, GRAV}}$ (Figure 2a). Neglecting adsorbed H$_2$O results in $T_{\text{M, SUM-dry}} = (0.92 \pm 0.06) \times T_{\text{M, GRAV}}$. TC is closely correlated to $T_{\text{M, GRAV}}$, but with a significant offset attributed to noncarbonaceous inorganic compounds (Figure 2b). Total mass calculated from size distributions underestimates total mass by $>35\%$ on average (Figure 2c). EC from 2-step combustion (Figure 2b) and optical methods sensitive to light-absorbing BC (Figure 2d) are weakly correlated to $T_{\text{M, GRAV}}$ while close correlation is found between EC and BC.

The correlation between online methods MAAP, LII, and DMS500 and EC as a proxy for filter-based methods is shown in Figure 3. Close agreement is found between BC from absorption photometry (MAAP) and EC for conditions C1 and C2 with $B_{\text{C,MAAP}} = (1.08 \pm 0.16) \times EC$. For condition C3 with the highest mass concentration values, all online methods deviate significantly but consistently from filter-based off-line methods.
Table 1. Average Number Concentrations Measured by the Different CPC Systems and the DMS500 in the Raw Exhaust Gas; Data Presented As Number Concentration Values Given as 10^7 cm^-3 STP and as Results of a Linear Regression Analysis of Two Identical CPC Operated in Parallel

<table>
<thead>
<tr>
<th>Condition</th>
<th>TSI 3760A ( d_{p, \text{min}} = 14 \text{ nm} )</th>
<th>TSI 3010 ( d_{p, \text{min}} = 10 \text{ nm} )</th>
<th>GRIMM 5.400 ( d_{p, \text{min}} = 5 \text{ nm} )</th>
<th>DMS500 ( d_{p, \text{min}} = 5 \text{ nm} )</th>
</tr>
</thead>
<tbody>
<tr>
<td>C1, R1</td>
<td>0.96</td>
<td>0.99</td>
<td>1.22</td>
<td>N/A</td>
</tr>
<tr>
<td>C1, R2</td>
<td>1.32</td>
<td>1.39</td>
<td>1.60</td>
<td>2.17</td>
</tr>
<tr>
<td>C2, seq 1</td>
<td>2.79</td>
<td>2.91</td>
<td>3.61</td>
<td>3.40</td>
</tr>
<tr>
<td>C2, seq 2</td>
<td>1.8</td>
<td>2.07</td>
<td>2.58</td>
<td>N/A</td>
</tr>
<tr>
<td>C3</td>
<td>1.86</td>
<td>1.89</td>
<td>2.14</td>
<td>1.92</td>
</tr>
<tr>
<td>Linear regression slope ( m )</td>
<td>0.920 ± 0.001</td>
<td>1.060 ± 0.001</td>
<td>1.011 ± 0.002</td>
<td>0.929 ± 0.007</td>
</tr>
<tr>
<td>Correlation coefficient ( r^2 )</td>
<td>0.996</td>
<td>0.990</td>
<td>0.891</td>
<td>0.988</td>
</tr>
<tr>
<td>Ratio instrument no. 1/instrument no. 2</td>
<td>0.925 ± 0.077</td>
<td>1.044 ± 0.087</td>
<td>1.013 ± 0.036</td>
<td>0.82 - 1.43</td>
</tr>
</tbody>
</table>

Figure 4. Correlation of two identical instruments (a) of CPC type GRIMM 5.400 and (b) of DMS500; (c) correlation of EAD type TSI 3070A and CPC GRIMM 5.400 for conditions C1–C3 separately.
Table 2. Size Distribution Measurements Performed As Repetitive Measurements Using Two DMS500 Instruments (See Given Serial No.), or Determined from the Ratio of EAD vs. CPC Which Is Providing a Measure of Average Size

<table>
<thead>
<tr>
<th>DMS500</th>
<th>1st mode</th>
<th>2nd mode</th>
<th>serial no.</th>
<th>EAD/CPC GRIMM 5.400</th>
</tr>
</thead>
<tbody>
<tr>
<td>CMD (nm) GSD</td>
<td>CMD (nm) GSD</td>
<td>ratio (nm)</td>
<td>r²</td>
<td></td>
</tr>
<tr>
<td>condition C1</td>
<td>15.7 1.53</td>
<td>51.6 1.39</td>
<td>M44</td>
<td>7.4 ± 0.3</td>
</tr>
<tr>
<td></td>
<td>15.8 1.54</td>
<td>50.0 1.41</td>
<td>M45</td>
<td>5.6 ± 0.2</td>
</tr>
<tr>
<td>condition C2</td>
<td>15.1 1.53</td>
<td>46.6 1.30</td>
<td>M44</td>
<td>11.5 ± 0.06</td>
</tr>
<tr>
<td>condition C3</td>
<td>14.1 1.54</td>
<td>46.9 1.32</td>
<td>M44</td>
<td></td>
</tr>
<tr>
<td></td>
<td>17.4 1.5</td>
<td>58.5 1.45</td>
<td>M44</td>
<td></td>
</tr>
</tbody>
</table>

Figure 4 shows the scatter plots for CPC model GRIMM 5.400 (Figure 4a) and for the DMS500 (Figure 4b). All instruments based on the CPC technique show excellent reproducibility with a standard deviation of less than 5% in accordance with literature, with the exception of the TSI model 3060A which deviates by 7.5%. No effect of operation conditions or the organic content of PM is observed. The DMS500 instruments are also well correlated with an overall slope of the linear regression line of 0.93. In contrast to CPC based instruments, the average ratio between the two instruments shows a substantially larger scatter and varies from 0.84 to 1.43 for different operation conditions.

3.3. Size-Based Methods. The data analysis of the differential mobility spectrometer is summarized in Table 2. Compiled are the count median diameter (CMD) and the geometric standard deviation (GSD) for two modes dominating number size distributions. These properties are defined on the basis of a bimodal log-normal size distribution. The reproducibility of particle size measurements is also shown in Table 2. Performing measurements in the same sampling line with two types of the DMS500 instruments yields relative standard deviations of measured CMD values of <4%.

The data from EAD and CPC are also highly correlated; see Figure 4c. The ratio of EAD to CPC which has the unit of an efficiency. Indirect methods for the measurement of particle number concentrations as differential mobility spectrometry (DMS500, EEPS) are also capable of providing particle number concentration values, but direct methods like CPC are preferred because of much smaller scatter in data.

We recommend the measurement of nonvolatile particle number concentration by CPC-based methods with prior agreement on the instrument ∆p, min and the application of a volatile particle remover based on the hot dilution principle. Reproducibility with a standard deviation of less than 5% can be achieved. The method for measuring particle mass requires prior agreement of the measurand. For this particular source type, light absorbing BC and chemically inert and nonvolatile (for T = 350 °C) EC are almost equivalent. Potential techniques are optical-based methods for light-absorbing BC, and carbon burn-off methods for EC. Gravimetry as the only traceable method seems not appropriate because modern aircraft engines with low particle mass emissions require very long sampling times.

4. DISCUSSION

The consistent data set collected in SAMPLE from off-line and online mass-based methods permits an assessment of investigated methods with respect to their application for PM measurement in gas turbine exhaust. The focus on nonvolatile PM is in line with current understanding of particulate matter impacts on climate as well as on human health.

We achieved mass closure with the sum of key chemical components balancing total mass within 10% deviation from gravimetry data. Carbonaceous matter makes up the largest fraction of PM mass with light-absorbing BC corresponding closely to nonvolatile EC. From that, robust light absorption measurement methods are potential candidates for online techniques sensitive to nonvolatile PM. Among those MAAP shows close agreement with EC while LII data indicate a systematic underestimation of BC compared to MAAP or EC from 2-step combustion. Total mass inferred from size distributions require major assumptions concerning particle shape and effective density for data inversion. Being aware of decreasing emission levels for future aircraft engines, methods of sufficient sensitivity at acceptable sampling times have to be considered. This requirement is met by the online methods tested here while gravimetry with sampling times of up to 45 min is ruled out.

Major discrepancies between online and off-line methods at high power condition are most likely related to sampling artifacts. These sampling issues are associated with the presence of supermicrometer-sized soot agglomerates which are suspected to originate from combustor surfaces including the spray nozzle, or from sample line abrasion. The use of a PM 1.0 cyclone or impactor prior to the filter sampling locations for eliminating these large agglomerates, will be studied in the next phase of SAMPLE in order to reduce sampling artifacts caused by large soot agglomerates.

CPC instruments proved highly robust tools for measuring aerosol number concentrations, characterized by a method precision of less than 7.5%. Dilution of sample gas prior to the measurement is required. Absolute number concentrations given by different condensation particle counter models require careful consideration of the minimum detection diameter, defined for 50% detection efficiency. Direct methods for the measurement of particle number concentrations as differential mobility spectrometry (DMS500, EEPS) are also capable of providing particle number concentration values, but direct methods like CPC are preferred because of much smaller scatter in data.

We recommend the measurement of nonvolatile particle number concentration by CPC-based methods with prior agreement on the instrument ∆p, min and the application of a volatile particle remover based on the hot dilution principle. Reproducibility with a standard deviation of less than 5% can be achieved. The method for measuring particle mass requires prior agreement of the measurand. For this particular source type, light absorbing BC and chemically inert and nonvolatile (for T = 350 °C) EC are almost equivalent. Potential techniques are optical-based methods for light-absorbing BC, and carbon burn-off methods for EC. Gravimetry as the only traceable method seems not appropriate because modern aircraft engines with low particle mass emissions require very long sampling times.

ASSOCIATED CONTENT

Supporting Information. Additional information on instrumentation, hot end simulator, gas sample distribution system, dilution systems, evaluation of FOA3 for HES, mass measurement data, and supermicron particulates. This material is available free of charge via the Internet at http://pubs.acs.org.
Environmental Science & Technology

ARTICLE

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REFERENCES