



Array measurements in wind tunnels with open test sections

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Outline

- motivation
- experimental setup
- investigations: sound propagation through shear layers:
 - a) frequency broadening
 - b) phase fluctuations
 - c) velocity of turbulent structures
 - d) generic model
- summary



1. Motivation

The microphone – array – technique in the aero acoustics:
measurements in open - jet wind - tunnels

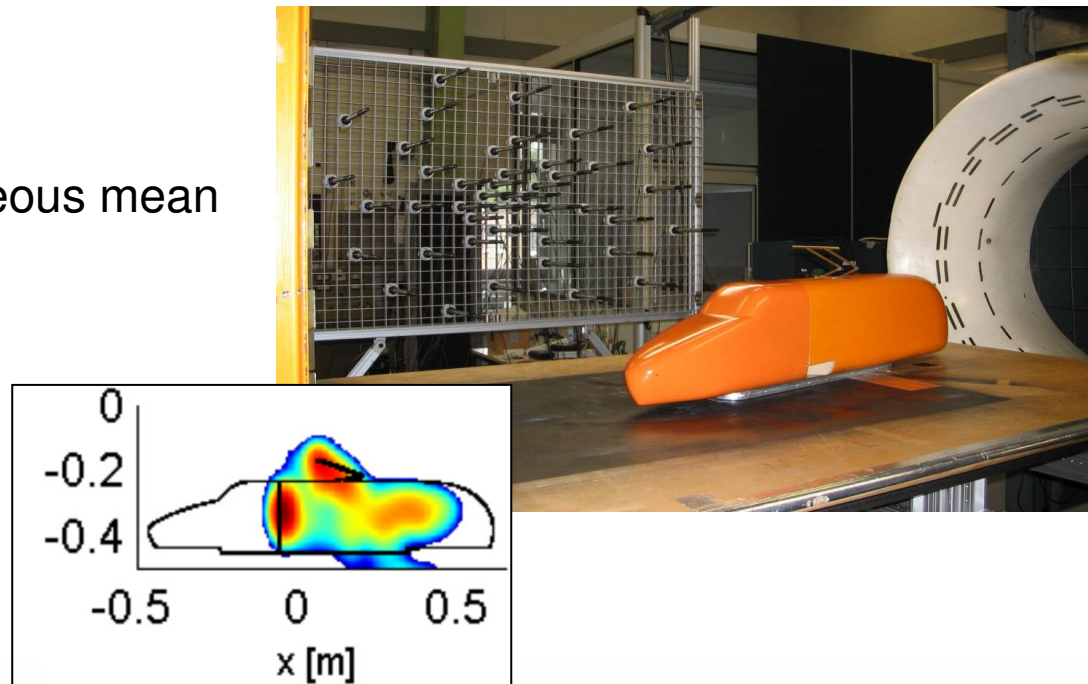
- sound source inside the flow, microphone array outside the flow: sound has to propagate through the wind - tunnel shear - layer

steady interactions:

- refraction in a inhomogeneous mean flow field

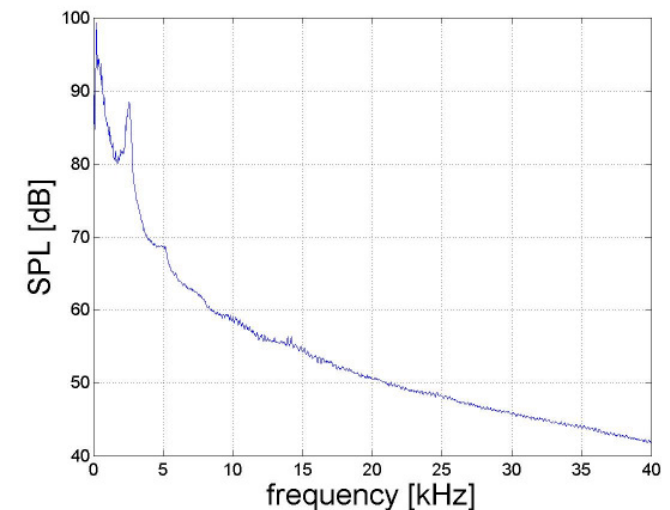
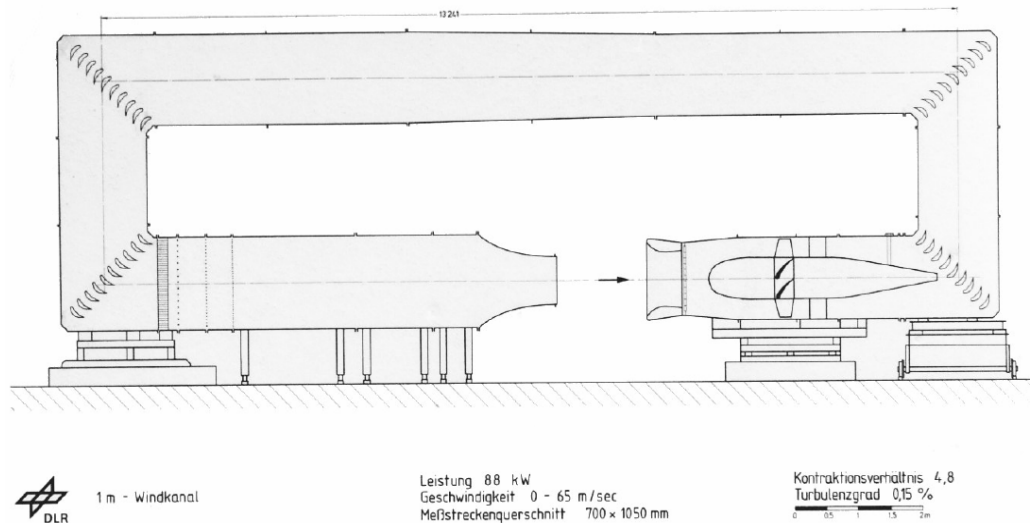
unsteady interactions:

- frequency broadening
- phase fluctuations



2. Experimental setup

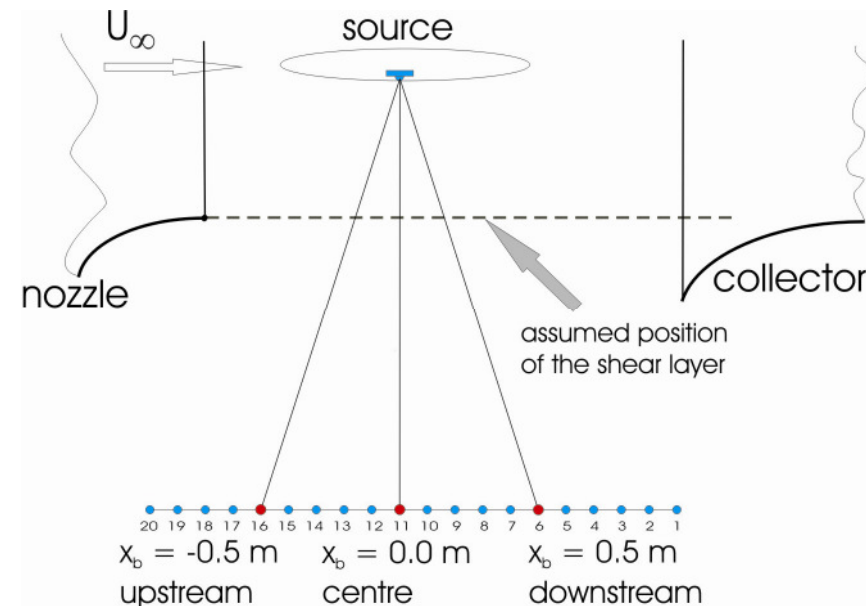
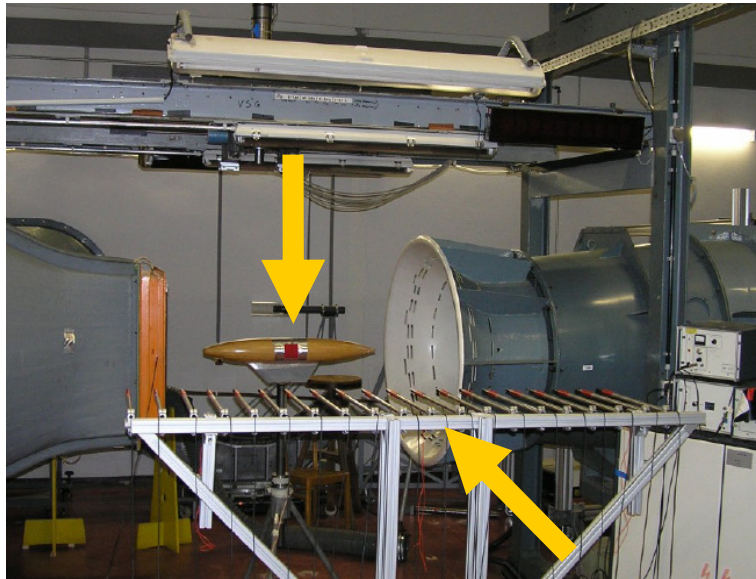
1M wind tunnel, DLR Göttingen ('1MG')



- $U_\infty = 0 - 65$ m/s, closed circuit, open test section
- noise, especially at lower frequencies, **not** acoustically optimized

2. Experimental setup

Sound source and microphone line – array in the 1MG



- foreground: line – array
- inside the test section: sound source, standard hi-fi tweeter, supplied with sine and/or white noise
- the red marked microphones are considered for the first investigations

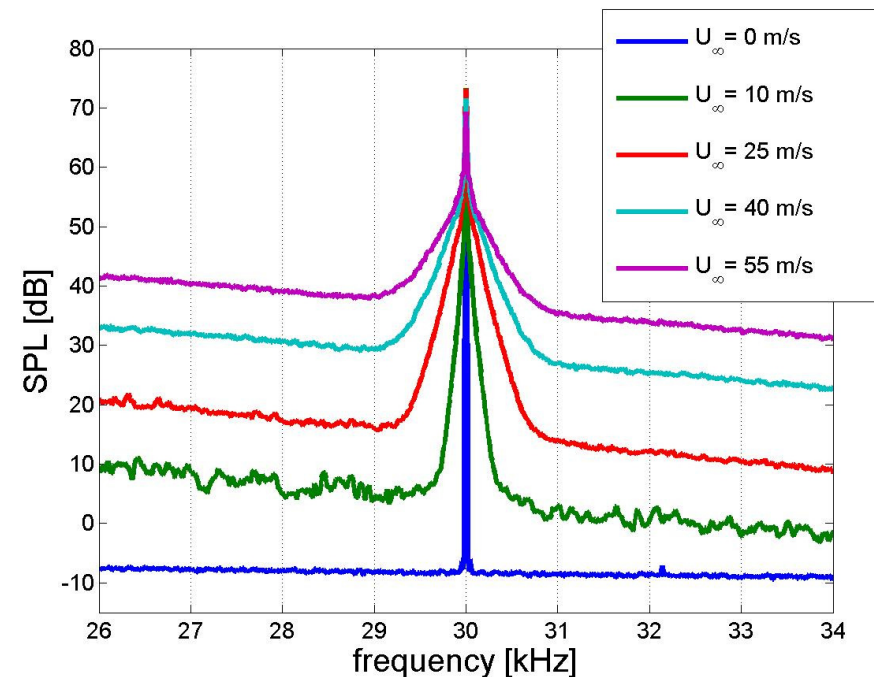
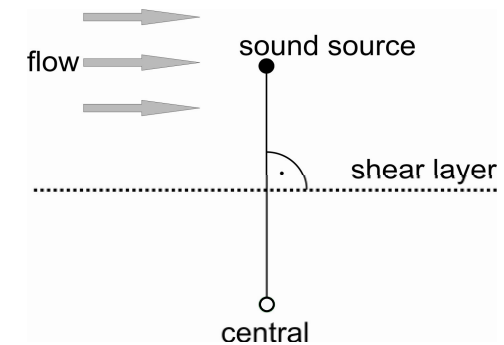
3. Frequency broadening

Influence of the wind tunnel shear layer on a tone

- sound source: $f_{\text{test}} = 30 \text{ kHz}$
- microphone, central located:
sound propagates
perpendicularly
- different flow velocities U_{∞}

result:

- symmetric peak broadening
- SPL of the peak decreases with velocity
- (as expected, higher ambient noise level)





3. Frequency broadening

Influence of the wind tunnel shear layer on a tone

explanation:

- interaction with structures → act as sources
- due to turbulence irregularly moving sources
- irregularly fluctuating Doppler shift: Doppler broadening: well known!

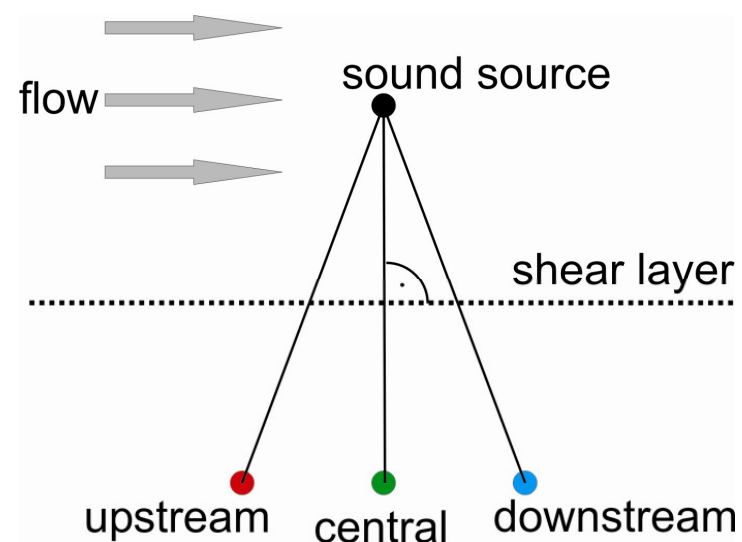
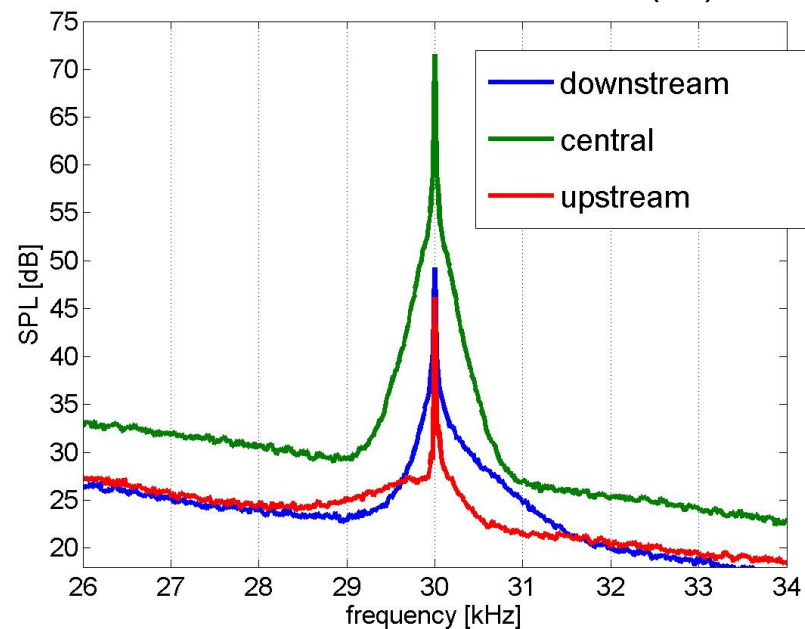
(see Ross 1981, AIAA 80-0984R)

3. Frequency broadening

Influence of the wind tunnel shear layer on a tone

three different positions of the observer: $U_{\infty} = 40$ m/s:

- asymmetric broadening for non - perpendicularly propagation
- observer upstream (-): peak skewed to lower frequencies
- observer downstream (-): skewed to higher frequencies





3. Frequency broadening

Influence of the wind tunnel shear layer on a tone

asymmetric broadening:

- irregular movement (symmetric broadening) superimposed with:
 - component toward the observer (microphone downstream)
 - component away from the observer (microphone upstream)

assumption:

- structures inside the shear layer which influence sound propagation
- these structures move downstream

→ motivation for the next investigations: learn more about these structures:
consideration of the phase



4. Phase fluctuations

of a wave which propagates through a shear layer

- phase fluctuations between source signal and observer signal:
 - due to acceleration or deceleration of the wave by the shear layer
- decreases correlations between array microphone signals:
 - SNR of beamformer output is reduced

experimental setup:

- standard setup
- tone with $f_{\text{test}} = 15$ or 30 kHz, emitted by source inside the flow
- recorded signals:
 - central microphone
 - electrical signal from the signal generator, simultaneously
- flow velocities: $U_{\infty} = 10, 25, 40$ and 55 m/s

4. Phase fluctuations

of a wave which propagates through a shear layer: calculation

computing $\phi'(t)$:

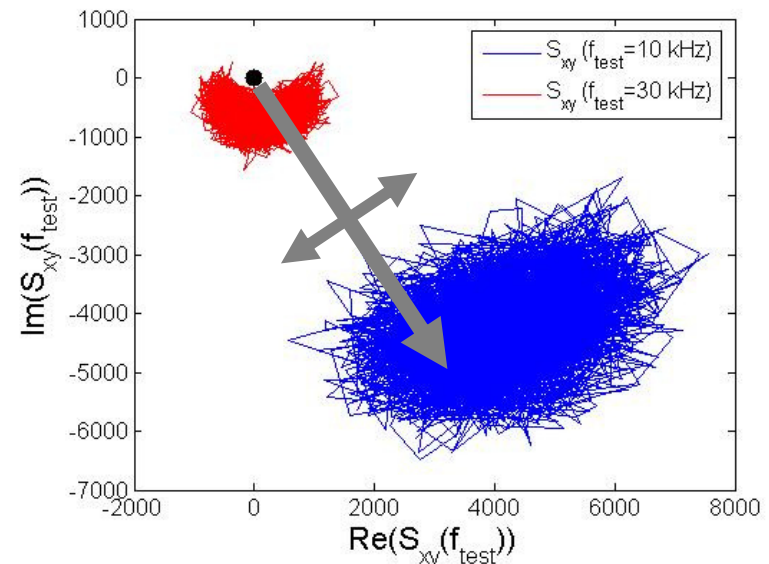
step 1:

- spectral cross density between microphone signal and electrical signal from the signal generator

$$S_{xy}(f) = F\{y(t)\} \cdot [F\{x(t)\}]^*.$$

- window-wise, narrow windows
- considering a single Fourier coefficient that corresponds to f_{test} : time series

→ phase and amplitude fluctuate



parameters:

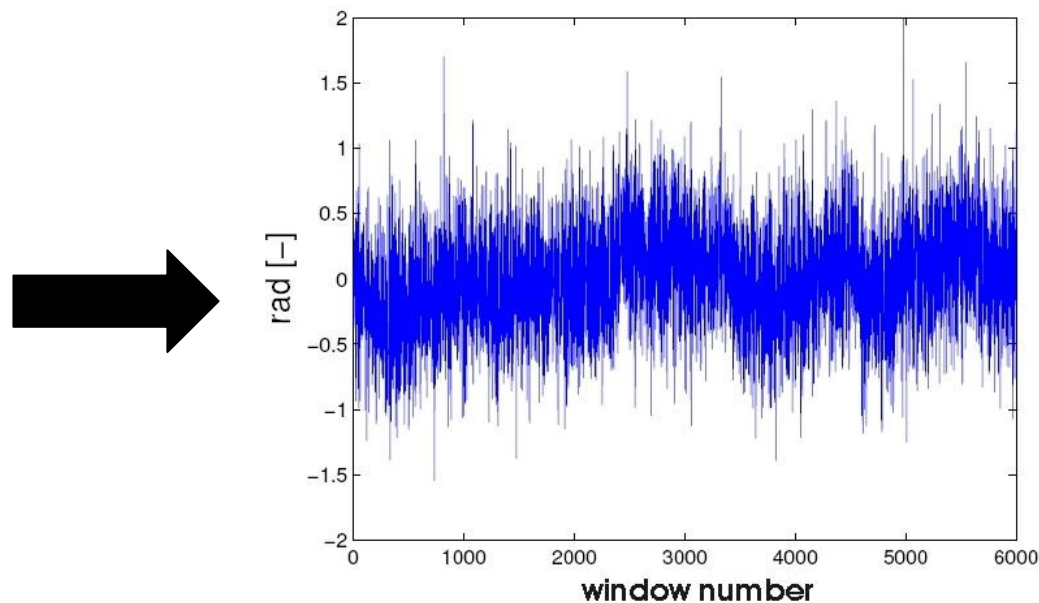
- $f_{\text{test}} = 10 \text{ kHz}$ and $f_{\text{test}} = 30 \text{ kHz}$, signal of the source
- windows: 50% overlap, Hanning – weighted, size: 1024 samples
- Mean over time interval: 10ms @ $f_s = 102.4 \text{ kHz}$,
→ artificial sampling frequency $f_{\text{sampling, Fourier}} = 200 \text{ Hz}$

4. Phase fluctuations

of a wave which propagates through a shear layer: calculation

step 2: using expression $\phi = \arctan\left(\frac{\operatorname{Re}(S_{xy}(f_{test}))}{\operatorname{Im}(S_{xy}(f_{test}))}\right)$ one obtains the phase

step 3: only the fluctuations are interesting : $\phi' = \phi - \bar{\phi}$



6000 windows \equiv 30 sec
measuring duration
@ artificial sampling rate:
 $f_{\text{sampling, Fourier}} = 200 \text{ Hz}$

4. Phase fluctuations

of a wave which propagates through a shear layer: calculation

- Frequency spectra of $\phi'(t)$, from measurements with $f_{\text{test}} = 15 \text{ kHz}$ and $f_{\text{test}} = 30 \text{ kHz}$

results:

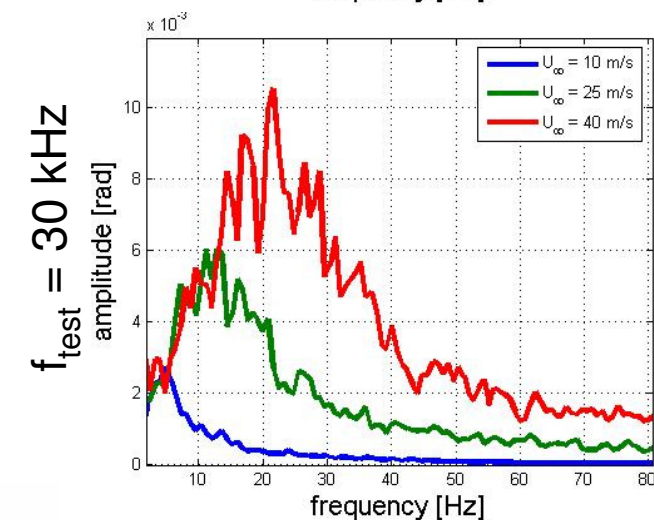
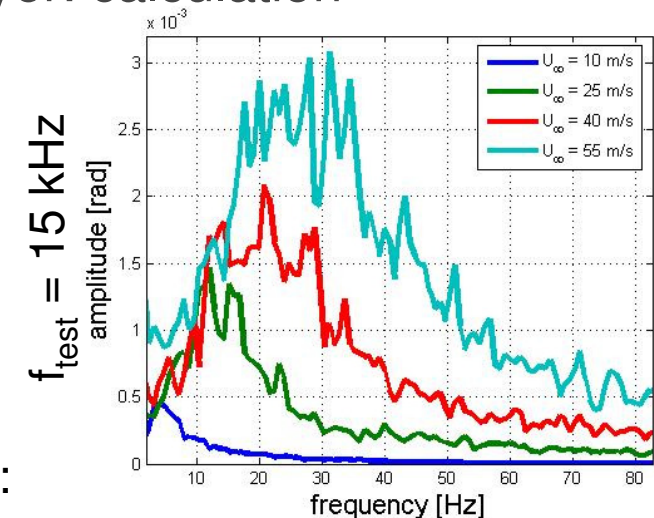
- distinct frequency spectra
- peak is flow velocity dependent \rightarrow Strouhal number:

$$Sr = \frac{f l}{U_{\infty}}$$

low frequencies \rightarrow large scale structures

(Sr with characteristic length diameter of the nozzle)

- peak position is not influenced by f_{test}





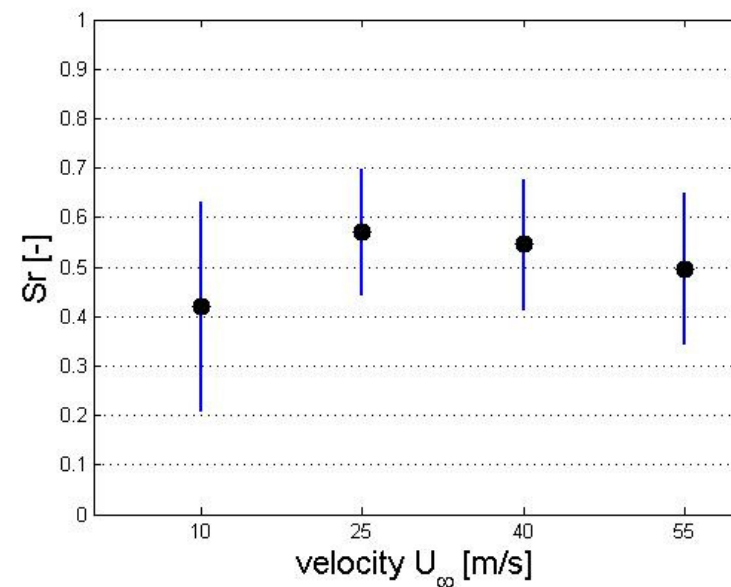
4. Phase fluctuations

of a wave which propagates through a shear layer: calculation

- Strouhal number constant around mean value $Sr \approx 0.48$
 - linear dependency between velocity and frequency

annotation concerning phase fluctuations:

- measurable = compensatable?
- 'guide star method': Ehrenfried et al. AIAA 2005-2962



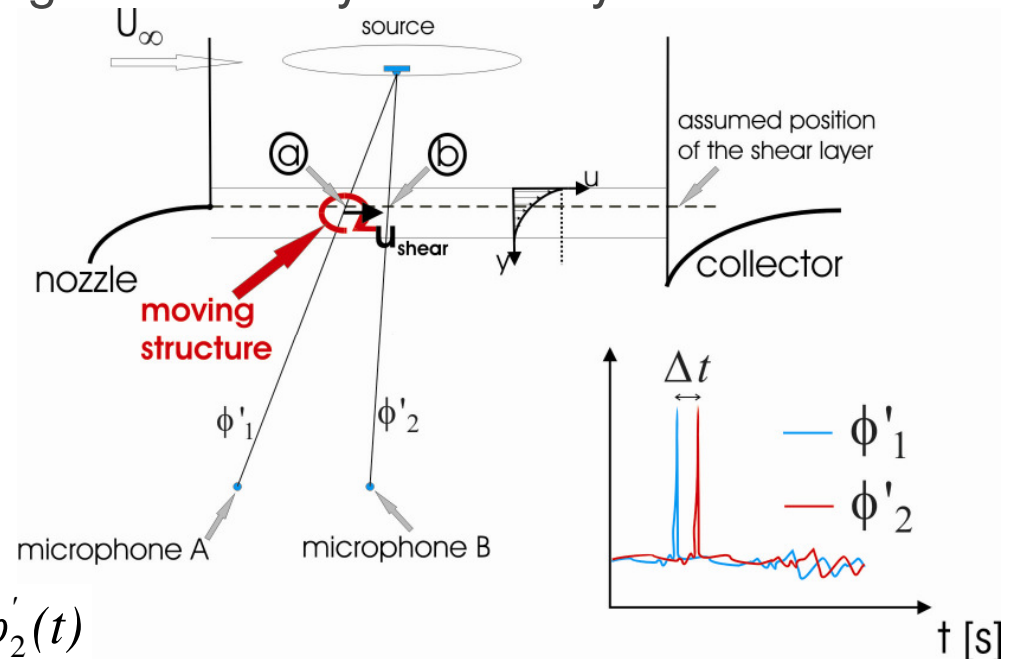
4. Phase fluctuations

of a wave which propagates through a shear layer: velocity of structures

downstream moving structures:
→ asymmetric broadening

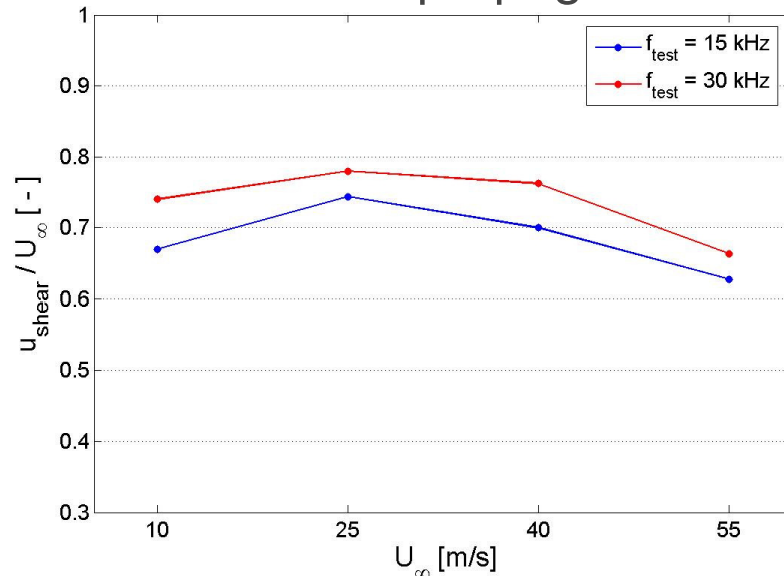
velocity measurement:

- source emits tone
- calculating time series: $\phi'_1(t)$ and $\phi'_2(t)$
- moving structure influences phases one after another
- cross correlation function computes time shift Δt
- one obtains the mean velocity of structures



4. Phase fluctuations

of a wave which propagates through a shear layer: velocity of structures



- ratio $u_{\text{shear}} / U_{\infty}$ nearly constant
- u_{shear} between 62% and 78% of U_{∞}
- u_{shear} depends on f_{test}

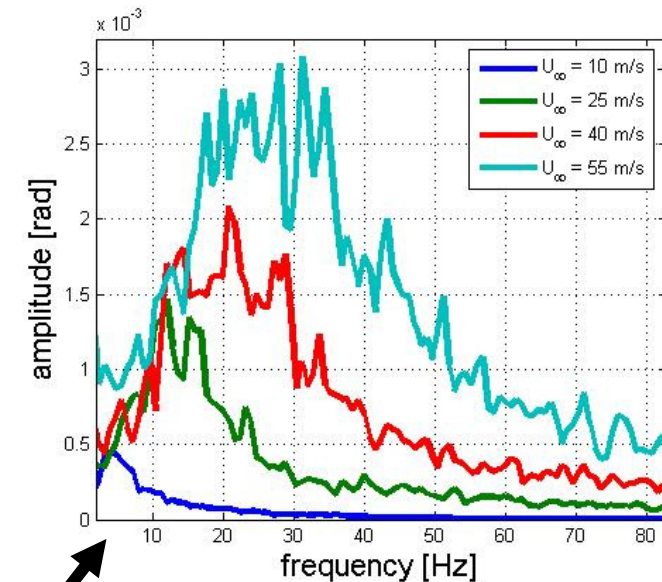
- assume: ensemble of structures with different velocities inside the shear layer
 - frequency dependence:
 - strong interaction: structure size \geq wavelength
 - weak interaction: wavelength \gg structure size
- smaller structures travel faster than larger ones

5. Model of the sound propagation using phase modulation

$$u'(x_s, f, t) = \hat{u}_r \cdot \exp \left[i \left(2\pi f t + \varepsilon \cdot \cos \left(2\pi \tilde{f} t - \frac{2\pi \tilde{f}}{u_{shear}} x \right) \right) \right]$$

basic ideas:

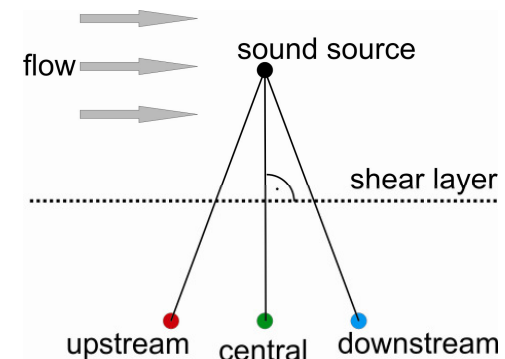
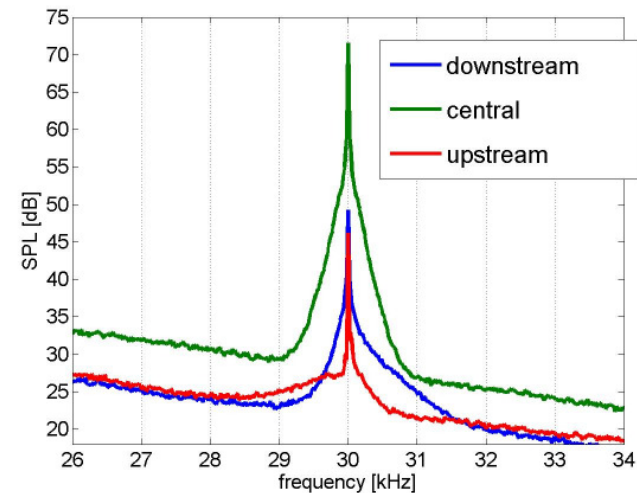
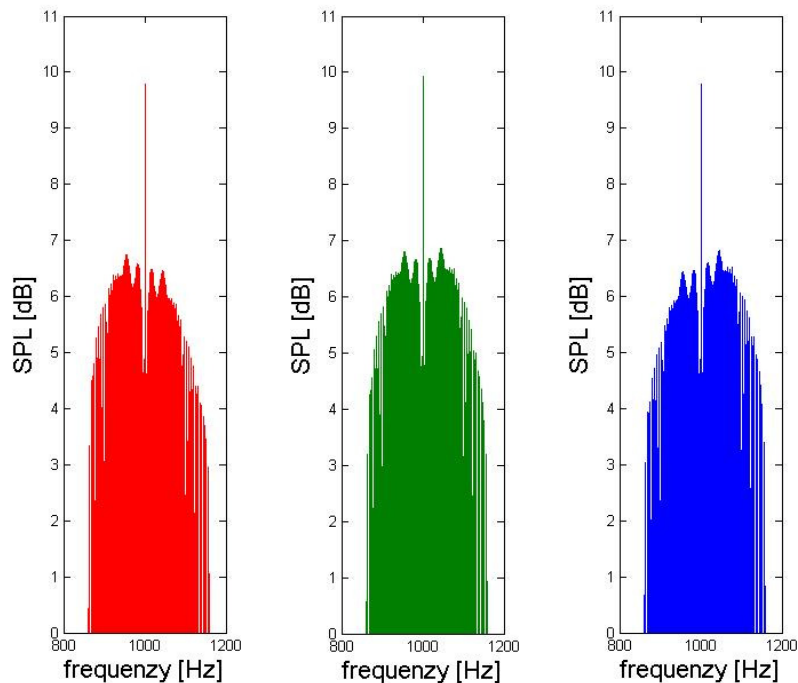
- monopole source
- infinitesimal thin shear layer
- no flow
- shear layer induces phase modulation:
frequency of modulation \tilde{f} = frequency distribution of $\phi'(t)$
- u_{shear} = downstream velocity of phase disturbance
- using Kirchhoff – Helmholtz – integral to compute sound field in front the shear layer



5. Model of the sound propagation using phase modulation

test case with $f_{\text{test}} = 1000\text{Hz}$:

- simple model able to predict tendencies of symmetric and asymmetric broadening





6. Summary

- questions concerning array measurements in open jet wind tunnels
- an experimental setup (line array and sound source) was developed which allows investigations concerning sound propagation through a shear layer
- broadening: dependence on flow velocity and especially position of the observer: important for narrow – band analysis
- assumption of structures that influence phase, moving downstream
- computing spectra of these phase fluctuations: maxima are velocity dependent: found a Strouhal number of $Sr = 0.48$
- estimation of the velocity of these structures in the shear layer: between 62% and 78% of U_∞
- finally, development of an simple model that is able to reproduce tendencies of the symmetric and asymmetric broadening



Thank you for your attention!



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BEBEC_2008 > Andreas Lauterbach > 19.02.2008