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Mode Transition Behavior in Hybrid Dynamic Systems

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Vortrag

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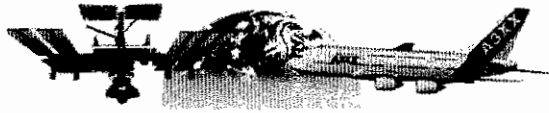
Mode Transition Behavior in Hybrid Dynamic Systems

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Mathematical Modeling of Open Dynamical Systems

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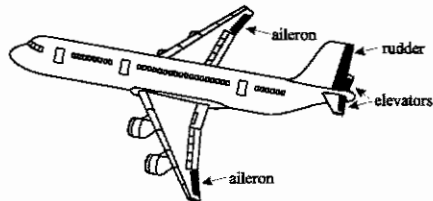


Introduction

Mode Transitions in Hybrid Models of Physical Systems

- ▶ hybrid because
 - continuous, differential equations
 - discrete, finite state machine
- ▶ overview of phenomena involved

Illustrated by Hydraulic Actuator Used for Aircraft Attitude Control Surfaces



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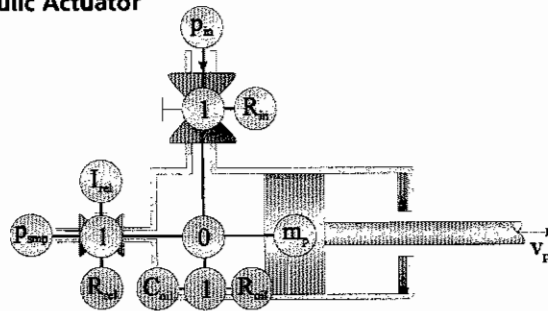


Modeling of Physical Systems

Ideal Picture Model (Schematic)

Identify Behavioral Phenomena

For Example, A Hydraulic Actuator



Equation Generation

Compile Constituent Equations

- | | |
|--------------------------|---|
| • R_{in} | $f_{in} R_{in} = P_{Rin}$ |
| • R_{oil} | $f_R R_{oil} = P_{Roil}$ |
| • C_{oil} | $C_{oil} \dot{P}_C = f_R$ |
| • m_p | $m_p \dot{v}_p = A_p P_{cyl}$ |
| • R_{rel} | $f_{rel} R_{rel} = P_{rel}$ |
| • I_{rel} | $I_{rel} \dot{f}_{rel} = P_{rel}$ |
| • 0 , cylinder chamber | $v_p = f_{in} - f_{rel}$ |
| • I , relief flow pipe | $P_{rel} = P_{smp} - f_{rel} R_{rel} + P_{cyl}$ |
| • I , intake pipe | $P_{Rin} = P_{in} - P_{cyl}$ |
| • I , oil compression | $P_{Roil} = P_{oil} - P_C$ |



Equation Processing

Before Simulation

- ▶ the number of equations is reduced
 - substitution/elimination
- ▶ equations are sorted
 - each equation computes one variable
- ▶ equations are solved
 - high index problems may require differentiation of certain equations



Hybrid Behavior

Introduce Valves

- ▶ make highly nonlinear behavior piecewise linear
 - intake valve *if* v_{in} *then* $p_{Rin} = p_{in} - p_{cyl}$ *else* $f_{in} = 0$
 - relief valve *if* v_{rel} *then* $p_{rel} = p_{smp} - f_{rel}R_{rel} + p_{cyl}$ *else* $f_{rel} = 0$

Switching Between Modes of Continuous Behavior

- ▶ intake valve, v_{in} , external switch (control law)
- ▶ relief valve, v_{rel} , autonomous switch triggered by physical quantities

$$v_{rel} = p_{cyl} > p_{th}$$

- ▶ different sets of equations



Computational Causality

When Switching Equations

- ▶ computational causality may change
 - re-ordering
 - re-solving

Example

- ▶ when the intake valve closes, equations change
 - from $p = p - p_{cyl}$
 - to $f_{in} = 0$
- ▶ therefore, in this equation
 - p_{Rin} becomes unknown
 - f_{in} becomes known



Implicit Modeling

Deal With Causal Changes Numerically

Valve Behavior

- ▶ residue on f_{in} $0 = \text{if } v_{in} \text{ then } -p_{Rin} + p_{in} - p_{cyl} \text{ else } f_{in}$
- ▶ residue on f_{rel} $0 = \text{if } v_{rel} \text{ then } -p_{rel} + p_{smp} - f_{rel}R_{rel} + p_{cyl} \text{ else } f_{rel}$

Implicit Numerical Solver (e.g., DASSL)

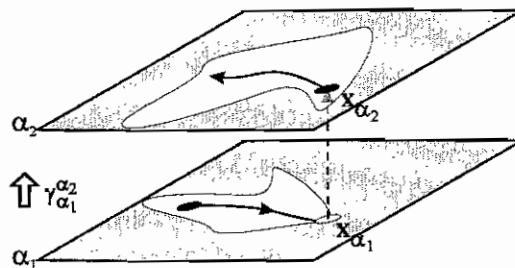
- ▶ designed to handle this formulation



Hybrid Dynamic Behavior

Geometric View

- ▶ modes of continuous, smooth, behavior
- ▶ patches of admissible state variable values



Specification Parts

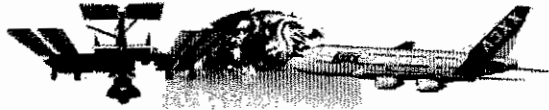
Hybrid Behavior Specification

- ▶ a function, f_i , that defines continuous, smooth, behavior for each mode

$$f_{\alpha_i}: E_{\alpha_i} \dot{x} + A_{\alpha_i} x + B_{\alpha_i} u = 0$$

- ▶ an inequality, γ , that defines admissible state variable values

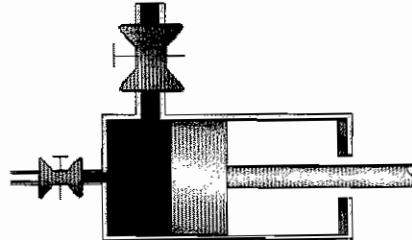
$$\gamma_{\alpha_i}^{\alpha_{i+1}}: C_{\alpha_i} x + D_{\alpha_i} u \geq 0$$



Dynamics

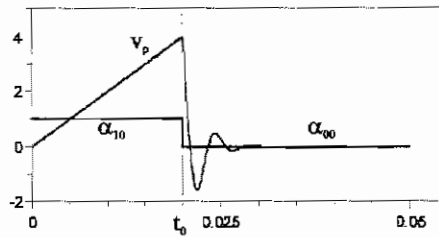
Behavior Characteristics

- ▶ C^0 , i.e., no jumps in state variables
- ▶ steep gradients



Example

- ▶ when the intake valve closes, piston velocity quickly reduces to 0



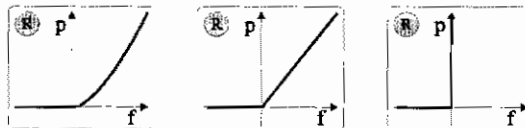
The Next Step

Remove Step Gradients

- ▶ e.g., singular perturbation

Algebraic Constraints Between State Variables

- ▶ high index systems
- ▶ subspace with admissible (continuous) dynamic behavior
- ▶ discontinuities (jumps) in state behavior

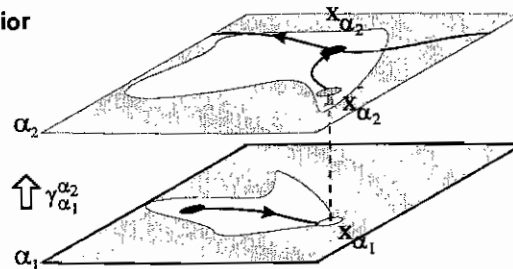




Hybrid Dynamic Behavior - Refined

Geometric View

- ▶ modes of continuous, smooth, behavior
- ▶ patches of admissible state variable values
- ▶ manifold of dynamic behavior



Specification Parts

Hybrid Behavior Specification

- ▶ a function, f , that implicitly defines for each mode
 - continuous, smooth, behavior
 - state variable value jumps

$$f_{\alpha_i}: E_{\alpha_i} \dot{x} + A_{\alpha_i} x + B_{\alpha_i} u = 0$$

- ▶ an inequality, γ , that defines admissible generalized state variable values

$$\gamma_{\alpha_i}^{\alpha_{i+1}}: C_{\alpha_i} x + D_{\alpha_i} u \geq 0$$

- ▶ for explicit reinitialization (semantics of x)

$$f_{\alpha_i}: E_{\alpha_i} \dot{x} + A_{\alpha_i} x + B_{\alpha_i}^u u + B_{\alpha_i}^x x^- = 0$$



Handling of Systems With High Index

DASSL Handles Index 2 Systems

- implicit formulation for continuous behavior

Requires Consistent Initial Conditions When Mode Changes Occur

- compute from implicit formulation to make jump space (projection) explicit
- for example, sequences of subspace iteration
 - space of dynamic behavior: $V^{n-1} = A^{-1} E V^n, V^0 = R^n$
 - jump space: $T^{n+1} = E^{-1} A T^n, T^0 = \{0\}$
- or, decomposition in (pseudo) Kronecker Normal Form



Projections

Linear Time Invariant Index 2 System

- derive pseudo Kronecker Normal Form (numerically stable)

$$\begin{bmatrix} E_{11} & 0 & 0 \\ 0 & 0 & E_{22,12} \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{x}_f \\ \dot{x}_{i,1} \\ \dot{x}_{i,2} \end{bmatrix} + \begin{bmatrix} A_{11} & A_{12,1} & A_{12,2} \\ 0 & A_{22,11} & A_{22,12} \\ 0 & 0 & A_{22,22} \end{bmatrix} \begin{bmatrix} x_f \\ x_{i,1} \\ x_{i,2} \end{bmatrix} + \begin{bmatrix} B_1 \\ B_{2,1} \\ B_{2,2} \end{bmatrix} u = 0$$

- after integration (no impulsive input behavior), consistent values are

$$x_f = \bar{x}_f - E_{11}^{-1} A_{12,1} A_{22,11}^{-1} E_{22,12} (x_{i,2} - \bar{x}_{i,2})$$

$$x_{i,1} = A_{22,11}^{-1} (-B_{2,1} u + E_{22,12} \dot{x}_{i,2}) - A_{22,12} x_{i,2}$$

$$x_{i,2} = -A_{22,22}^{-1} B_{2,2} u$$



The Hydraulic Actuator

Generalized State Jumps for Each Mode

Mode	Projection
α_{00}	$f_{rel} = 0$ $v_p = 0$
α_{01}	$v_p = (m_p v_p^- - I_{rel} f_{rel}^-) / (m_{rel} + m_p)$ $f_{rel} = (m_p v_p^- - I_{rel} f_{rel}^-) / (m_{rel} + m_p)$
α_{10}	$v_p = v_p^-$ $f_{rel} = 0$
α_{11}	$v_p = v_p^-$ $f_{rel} = f_{rel}^-$



A Scenario

Intake Valve Is Open

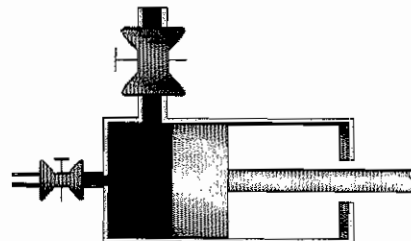
- ▶ piston starts to move

Intake Valve Closes

- ▶ piston inertia causes pressure build-up
- ▶ pressure reaches critical value

Relief Valve Opens

- ▶ cylinder pressure decreases



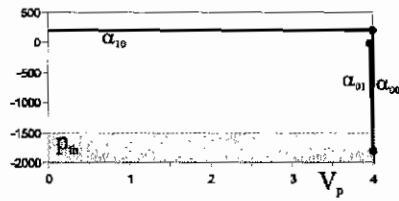
⇒ Interaction Between Mode Transition Behavior



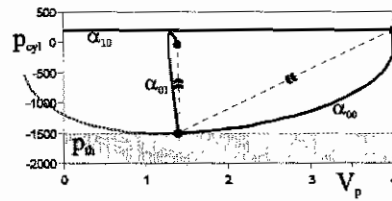
Phase Space of Cylinder Scenario

Projection Is Aborted

- ▶ immediately
- ▶ after partial completion



(a)



(b)

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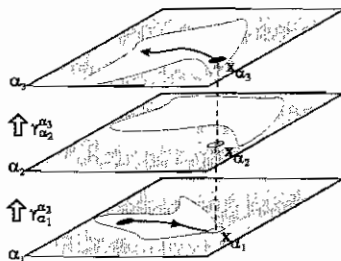
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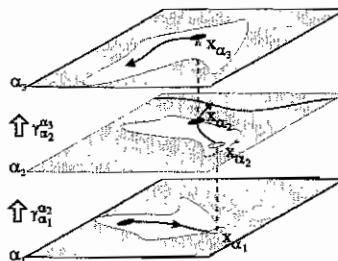
Sequences of Mode Changes

(a) State Outside of a Patch in the New Mode

(b) During Projection State Values are Reached Outside of a Patch in the New Mode



(a)

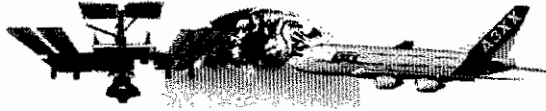


(b)

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Impulses

High Index Systems May Contain Impulsive Behavior

- ▶ in case of the hydraulic cylinder $t_s p > p_{th}$ would always hold if not $v_p = v_p^-$
- ▶ unknown where the patch is abandoned

In-Depth Analysis of Switching Conditions

- ▶ solve for required $x(t)$
- ▶ compute earliest $t = t_s$ at which $\gamma(x(t), u(t), t) \geq 0$
- ▶ substitute t_s to compute $x(t_s)$

Complex Switching Structure

Additional Difficulty When Interacting Fast Transients (e.g., collision)



Detailed Analysis of the Projection

Cylinder Example (Imaginary Eigenvalues, $\lambda = \lambda_r + i \lambda_i$)

- ▶ from detailed model

- solve for p

$$p(t) = e^{\lambda_r t} (p^- \cos(\lambda_i t) - \frac{1}{\lambda_i} (\frac{1}{C_1} v_p^- + \lambda_r p^-) \sin(\lambda_i t))$$

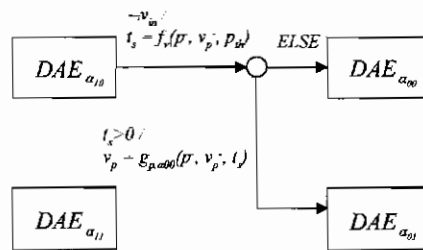
- substitute t at which $p(t) > p_{th}$

$$v_p = e^{\lambda_r t_s} (v_p^- \cos(\lambda_i t_s) - (\frac{R_2}{I_1} v_p^- - \frac{P_1}{I_1} + \lambda_r v_p^-) \frac{\sin(\lambda_i t_s)}{\lambda_i})$$



Complex Switching Structure

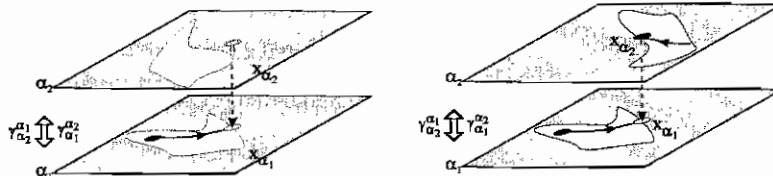
Explicit Re-Initialization

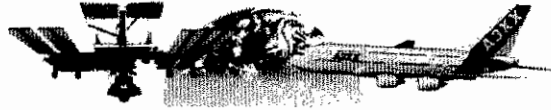


Chattering

What if the New Mode Switches Back

- ▶ immediately \Rightarrow inconsistent model, no solution
- ▶ after infinitesimal period of time \Rightarrow chattering behavior, solve with
 - equivalent control
 - equivalent dynamics

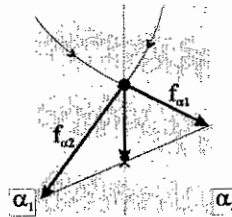




Equivalent Dynamics

Chattering

- ▶ fast component
 - remove
- ▶ slow component
 - weighted mean of instantaneous vector fields (Filippov Construction)
- ▶ sliding behavior



Ontology

Phase Space Transition Behavior Classification

- ▶ mythical (state invariant)
- ▶ pinnacle (state projection aborted)
- ▶ continuous
 - interior (continuous behavior)
 - boundary (further transition after infinitesimal time advance)
 - sliding (repeated transitions after each infinitesimal time advance)

Combinations of Behavior Classes



Conclusions

Mode Transition Behavior

- ▶ Rich
- ▶ Complex

Requires

- ▶ special algorithms/computations
- ▶ model verification analyses

How to Efficiently Generate Behavior (e.g., for Real-time Applications)?