

Comparison of Refueling Methods for Hydrogen Rail Vehicles

Linus Brünner, Steffen Wieser, Anton Roß and Mathias Böhm

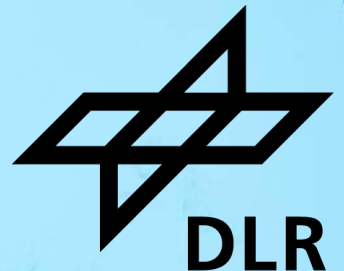
German Aerospace Center (DLR), Institute of Vehicle Concepts, Germany

RAILWAYS 2026 - The Seventh International Conference on Railway Technology: Research, Development and Maintenance

Budapest, Hungary, 23.-26. August 2026



scharlsim86/AdobeStock



Agenda

- 1 The Heidekrautbahn-Project
- 2 Motivation: Refueling of Hydrogen Rail Vehicles
- 3 Methodology: Simulation of Hydrogen Refueling Processes
- 4 Results: Comparison of different Refueling Approaches
- 5 Conclusion



The Heidekrautbahn Project

Overview



Key Facts:

- Funded by German Federal Ministry (BMV) and State of Brandenburg (MWEKE)
- Duration: 2022 – 2035
- Funding: ~ 48 million EUR



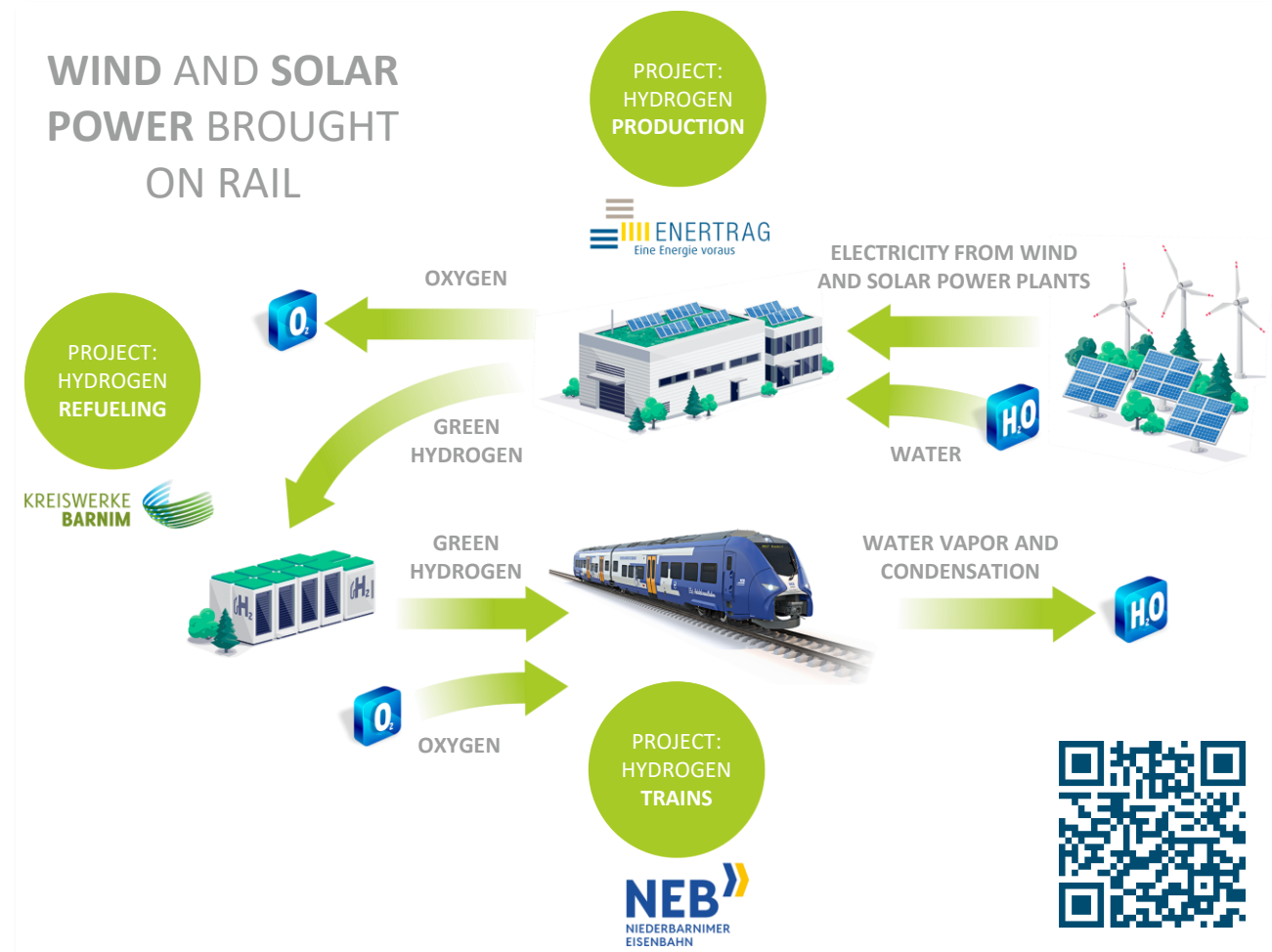
Objective:

- Emission free regional transport using green hydrogen produced from local wind and solar energy



Sub-Objectives:

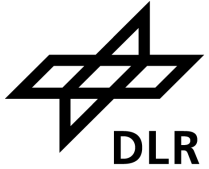
- Local hydrogen production through electrolysis
- Construction of a hydrogen refueling station for rail vehicles
- Replacement of diesel trains with seven hydrogen trains of type Siemens Mireo Plus H
→ in operation since Dec. 2024



[[Wasserstoffschiene Heidekrautbahn – Project](#) German Version]

Motivation

Refueling of Hydrogen Rail Vehicles

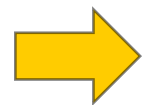


Hydrogen in Rail Vehicles:

- Stored gaseous at 35 MPa
- Capacity of 180 kg hydrogen (2 separate systems)

Why is refueling with Hydrogen difficult?

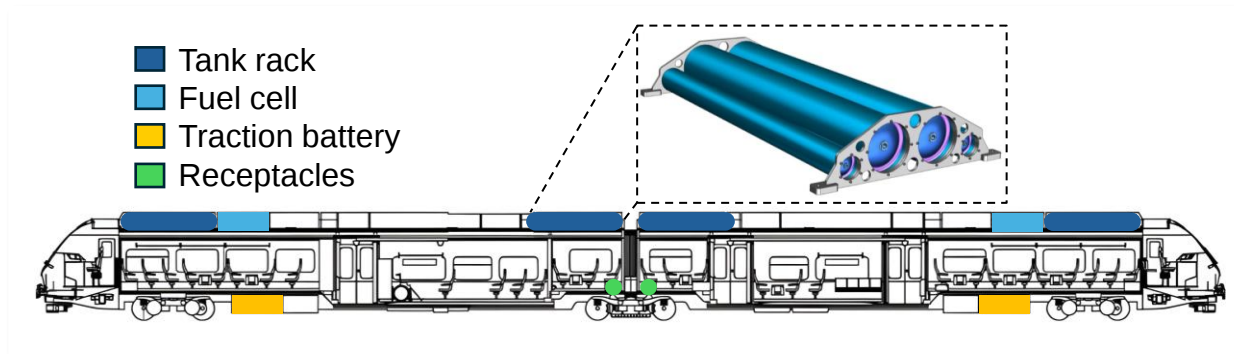
- Temperature increase during refueling:
 - Compression and Joule-Thomson effect
 - To prevent damaging tanks and to ensure safety
 - Temperature limit: 85 °C
- Standards developed to comply



None of the validated standards are usable for rail vehicles

Research Questions:

- What refueling speeds are achievable?
- Is one refueling method universally best?



Side view of the Siemens Mireo Plus H including drive train configuration and tank rack [paper sources 6,12, 14, 15]

Standard	max. H ₂ -Mass	Pre-Cooling	max. Mass Flow
SAE J2601	≤ 6 kg	[-40, -20] °C	≤ 60 g/s
SAE J2601-2	purely informative, no protocols		
SAE J2601-5 (TIR)	≤ 180 kg	[-40, amb.] °C	≤ 120 g/s
H35 CEP protocol	≤ 42.5 kg	[-40, amb.] °C	≤ 120 g/s

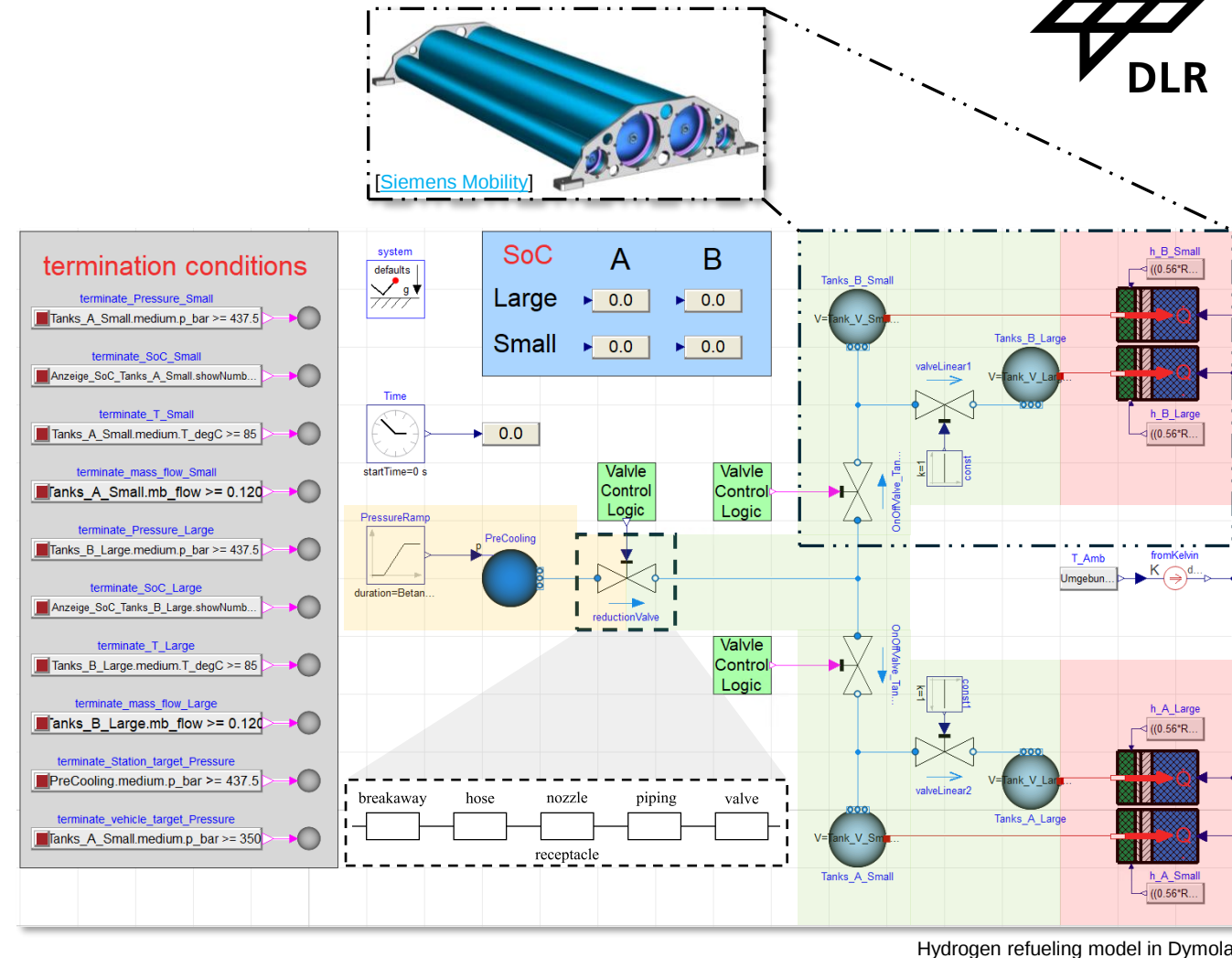
List of available refueling protocols [paper sources 7-10]

Methodology

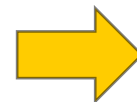
Refueling Model



- Simulation model built up in Dymola
 - Lumped parameter for fast simulation times
- Description of hydrogen refueling with following parts:
 - Termination conditions
 - Refueling station
 - Vehicle
 - Heat transfer
- Components between refueling station and vehicle summarized using one valve as flow resistance
- System characteristics of Mireo Plus H
 - Tank system with 90 kg
 - Tank system consists of 2 tank racks
- Different parameter-sets used for validation and investigation of refueling approaches



Hydrogen refueling model in Dymola



BY CHANGING REFUELING STATION PART, DIFFERENT REFUELING APPROACHES CAN BE INVESTIGATED



Approach:

- Models validated against real-world measurement data
 - Station: ambient & pre-cooling temperature, mass flow, ramp rate
 - Vehicle: tank temperature & pressure
- Measurement data used as input for simulation model (ambient & pre-cooling temperature, ramp rate)



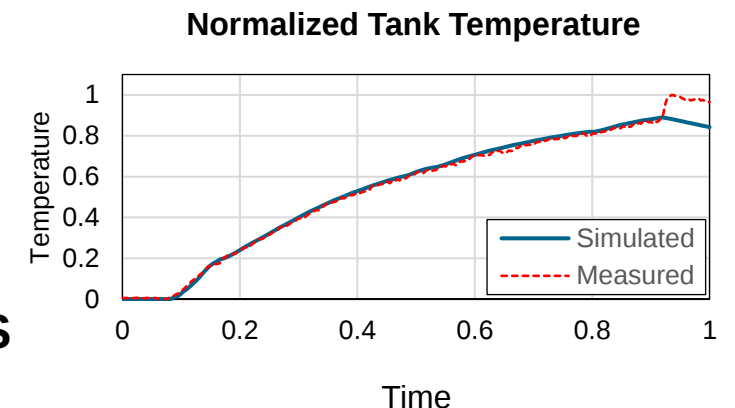
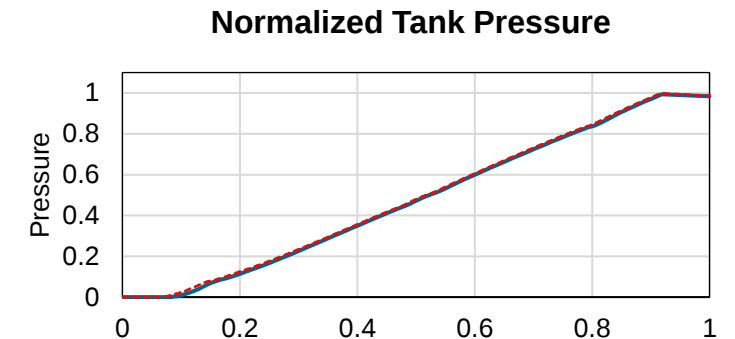
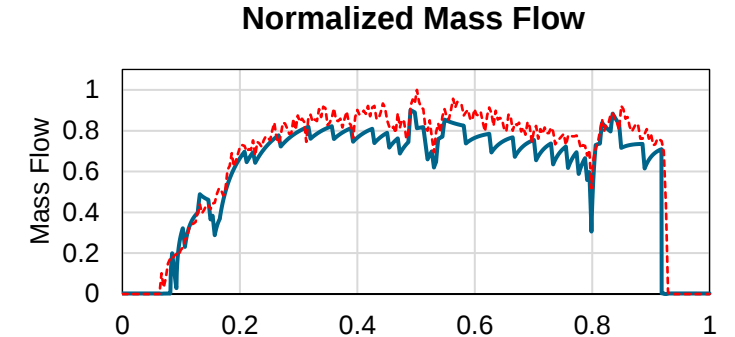
Performance:

- Models accurately capture key physical processes

Mass Flow	Pressure	Temperature
- slightly underestimated - large rel. deviations at start/end due to low flow rates - at higher flow rates rel. deviation < 20 %	- rel. deviation < 3 % - rel. deviation decreased over time	- rel. deviation < 0.5 % (until end of refueling) - increase to 1.5 % at end due to unmodeled thermal effects



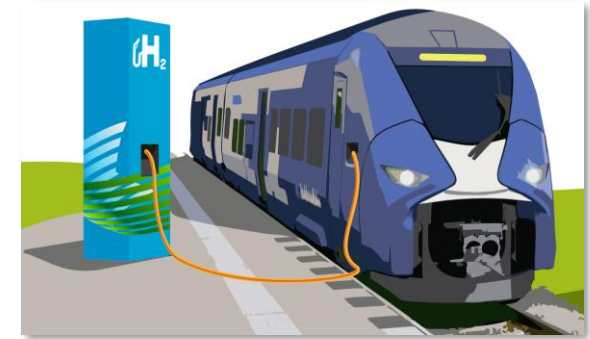
VALIDATED FOR USE IN HYDROGEN REFUELING ANALYSIS



Methodology

Refueling Approaches

- 🚚 **Hydrogen Trailer:** Simple overflow process → not controllable (p, T)
 - ✓ No infrastructure needed
 - Pressure reduces with each refueling

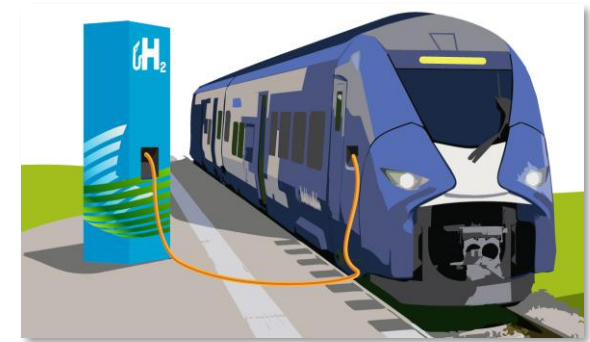


Methodology

Refueling Approaches



- 🚚 **Hydrogen Trailer:** Simple overflow process → not controllable (p, T)
- ✓ No infrastructure needed
 - Pressure reduces with each refueling



↔ **SAE J2601 – Communication**

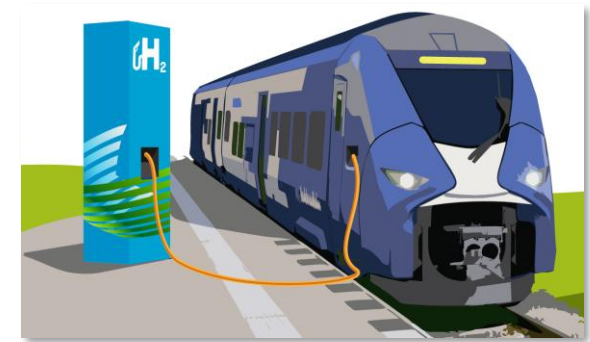
  	  
– Refueling parameters (tables) determined by data available to station (e.g. T_{amb}) – No Feedback from vehicle during refueling	– Additional data before refueling (less conservative tables) – Feedback from vehicle to monitor refueling (e.g. T_{tank})

Methodology

Refueling Approaches



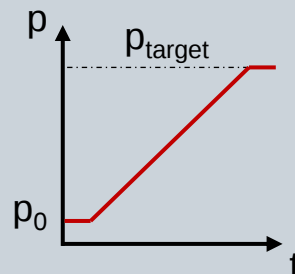
- 🚚 **Hydrogen Trailer:** Simple overflow process → not controllable (p , T)
- ✓ No infrastructure needed
 - Pressure reduces with each refueling



↔ **SAE J2601 – Communication**

  	  
– Refueling parameters (tables) determined by data available to station (e.g. T_{amb}) – No Feedback from vehicle during refueling	– Additional data before refueling (less conservative tables) – Feedback from vehicle to monitor refueling (e.g. T_{tank})

📊 **SAE J2601 – Strategy**

Table-based	
– Fixed pressure ramp rate (PRR) applied until pre defined target pressure reached – <u>With communication:</u> top-off with reduced ramp rate at the end for higher SoC	

Methodology

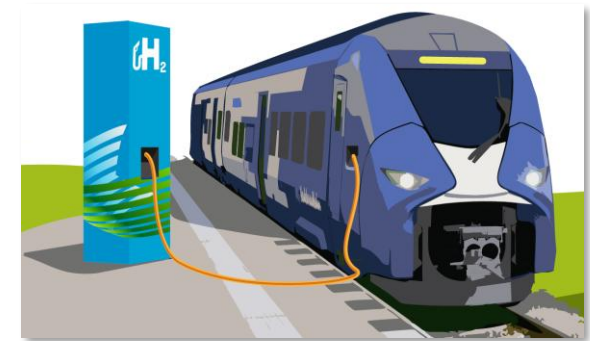
Refueling Approaches



Hydrogen Trailer: Simple overflow process → not controllable (p, T)

✓ No infrastructure needed

– Pressure reduces with each refueling



↔ **SAE J2601 – Communication**

  	  
– Refueling parameters (tables) determined by data available to station (e.g. T_{amb}) – No Feedback from vehicle during refueling	– Additional data before refueling (less conservative tables) – Feedback from vehicle to monitor refueling (e.g. T_{tank})

SAE J2601 – Strategy

Table-based

- Fixed pressure ramp rate (PRR) applied until pre defined target pressure reached
- With communication: top-off with reduced ramp rate at the end for higher SoC

MC-Formula

- Dynamic calculation of PRR every second
- Influenced by expected refueling time t_{final}
- Dependent on mass-avg. temp. of dispensed hydrogen

$$PRR = \frac{P_{final} - P_{ramp}}{t_{final} * \left(\frac{P_{final} - P_{initial}}{P_{final} - P_{min}} \right) - t}$$

Simulation Results

Trailer vs Ramp-Rate



Boundary Conditions:

15 °C

Ambient Temperature

15 %

initial State of Charge

350 bar

Vehicle Target Pressure

None

Pre-Cooling



Hydrogen Trailer:

- 350/500 bar with 31.5 m³



Table-Based:

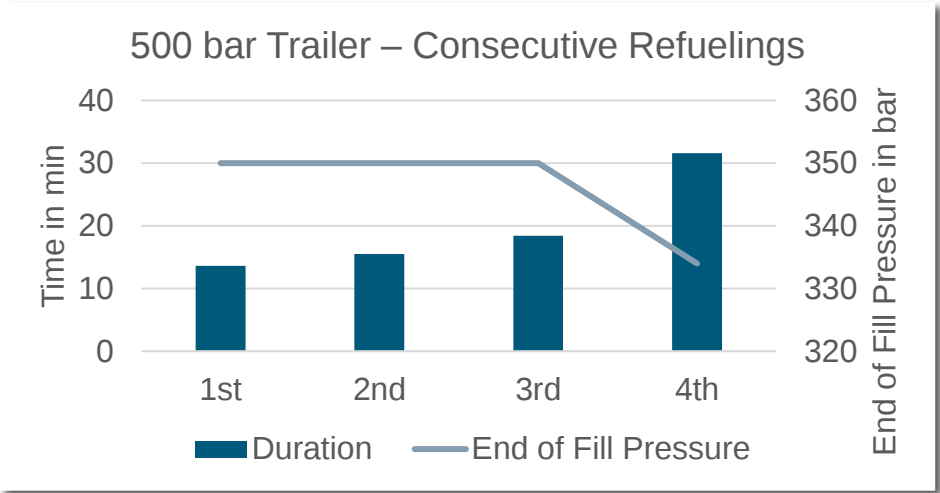
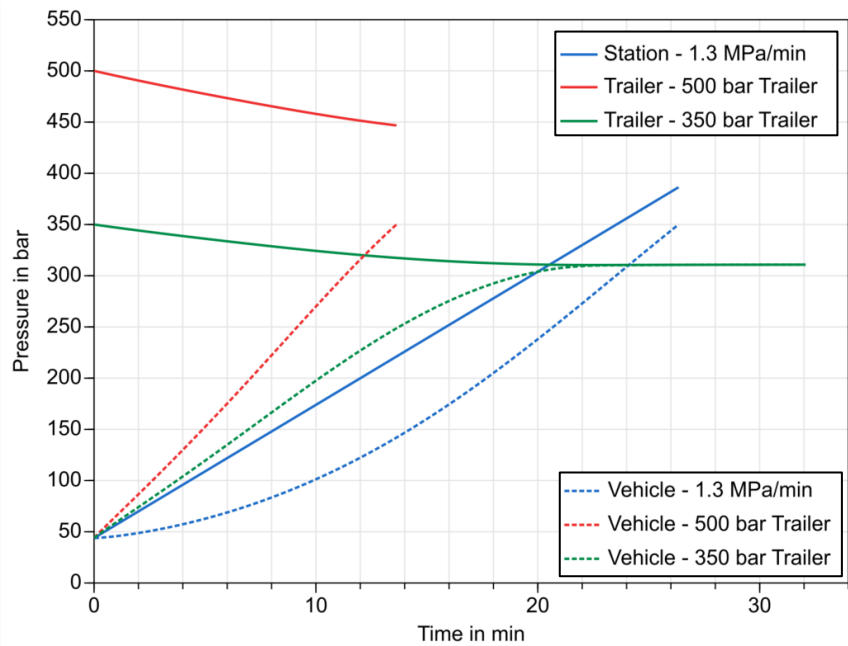
- 1.3 MPa/min

End of Fill ...	500 bar	350 bar	1.3 MPa/min
... SoC	87.3 %	82.8 %	88.5 %
... Pressure	350 bar	311 bar	350 bar
Duration	13.6 min	32.1 min	26.4 min

*per tank system each 90 kg

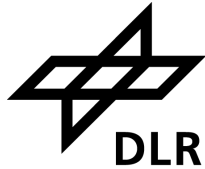


Trailer refueling can be fast – depends on initial Trailer pressure
Ramp refueling is repeatable



Simulation Results

MC-Formula vs Table-Based



Boundary Conditions:



40 °C
Ambient Temperature



15.7 %
initial State of Charge



Standard
Station Target Pressure



-20 °C
Pre-Cooling

$$PRR = \frac{P_{final} - P_{ramp}}{t_{final} * \left(\frac{P_{final} - P_{initial}}{P_{final} - P_{min}} \right) - t}$$

MC-Formula*:

- with/-out communication

Table-Based:

- 2.1 MPa/min (SAE J2601-5, H35 Cat. D HF)

End of Fill ...	MC-Formula (comm.)	MC-Formula (non-comm.)	2.1 MPa/min
... SoC	100 %	56.4 %	64.8 %
Average PRR	2.5 MPa/min	2.5 MPa/min	2.1 MPa/min
Station Target Pressure	Target SoC 100 %	367 bar	367 bar
Duration	19.4 min	12.4 min	15.1 min

*per tank system each 90 kg



MC-Formula without communication has no advantage over Table-Based strategy

MC-Formula with communication leads to complete refueling

Conclusion

? What refueling speeds are achievable?

- Achievable SoC range: 56 – 100 %
- Max. speed refueling speed: 14 min (5.3 %/min) with 87 % end of fill SoC

? Is one refueling method universally best?

- No single “best method” → depends on use case

Method	Good for:	Limitations
Trailer	- Temporary/low-infrastructure deployment - Fast when trailer SoC high	- Performance drops with trailer SoC
Table-Based	- Simple implementation in station	- Incomplete fills w/o communication
MC-Formula	- Fast and complete fills with communication	- No advantage w/o communication

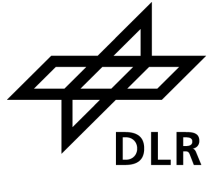
Recommendation:

- Vehicle-to-station communication for fast and safe refueling of hydrogen trains
- Revision of intended communication interface necessary

wasserstoff schiene

HEIDEKRAUTBAHN

Thank you for
your attention!



KREISWERKE
BARNIM



NEB
NIEDERBARNIMER
EISENBAHN



Federal Ministry
of Transport



btu

Brandenburg
University of Technology
Cottbus - Senftenberg



Deutsches Zentrum
für Luft- und Raumfahrt
German Aerospace Center

Accompanying DLR research funded by the Ministry for Economic Affairs, Energy, Climate Action and European Affairs of the state of Brandenburg, Germany (MWEKE) under individual measure according to the ZiFoG program, application no: 80259660, duration: 08/2022-12/2035. The vehicle data of the Siemens Mireo Plus H is collected and provided exclusively for scientific purposes as part of the research project.

Topic: **Comparison of Refueling Methods for Hydrogen Rail Vehicles**

Date: 2026-08-23/26 (YYYY-MM-DD)

Author: Linus Brünner

Institute: Institute of Vehicle Concepts

Image sources: All images “DLR (CC BY-NC-ND 3.0)”,
unless otherwise stated