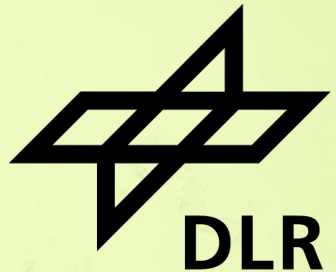


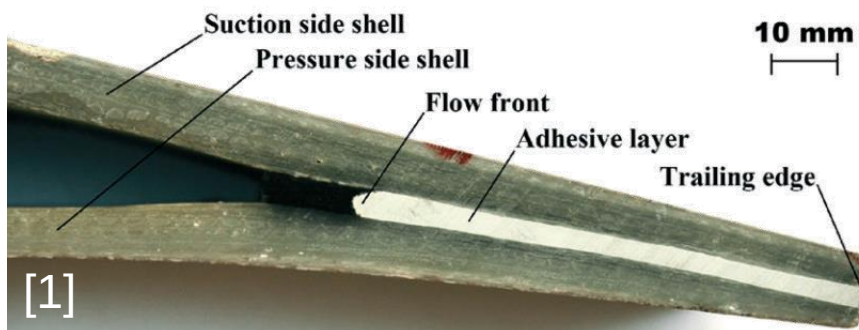
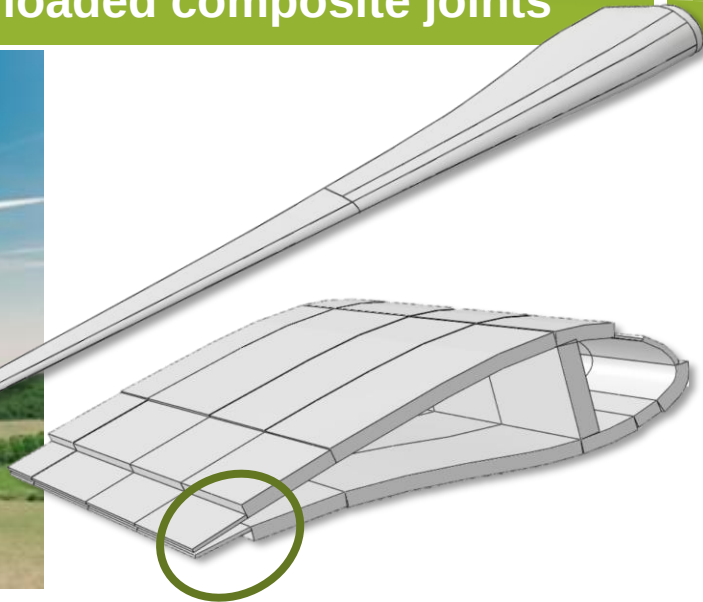
A FATIGUE DAMAGE MODEL FOR EPOXY RESIN AND ITS APPLICATION TO FIBER REINFORCED PLASTICS

Caroline Lüders, Institute of Lightweight Systems, German Aerospace Center (DLR)

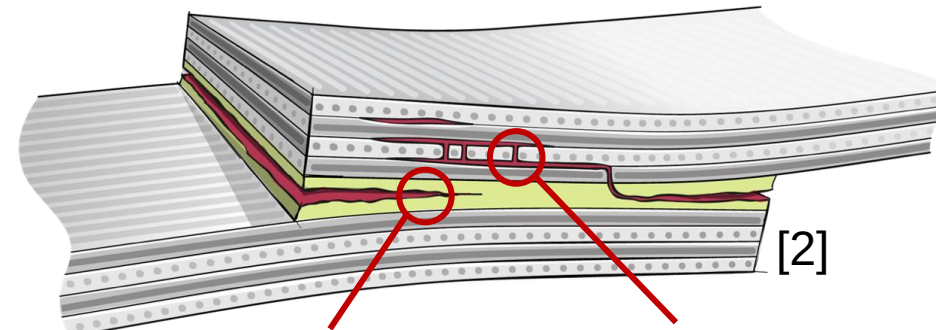


Role of epoxy resin in failure of adhesive composite joints

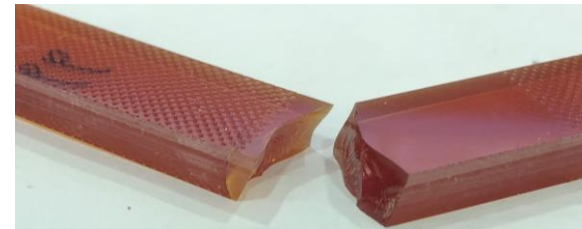
Cyclic loaded composite joints



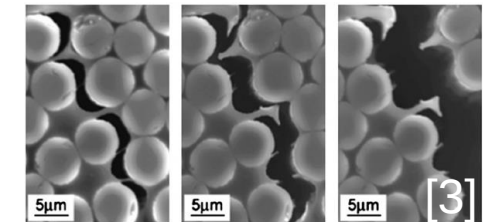
Damage phenomena in adhesive composite joints



Failure of epoxy adhesive



Failure of epoxy in composite



Fatigue behavior of epoxy resin contributes to fatigue failure of adhesive composite joints

[1] Eder et. al., 2014, DOI: 10.1002/we.1744

[2] Völkerink, 2022, DOI: 10.57676/hya4-2a09

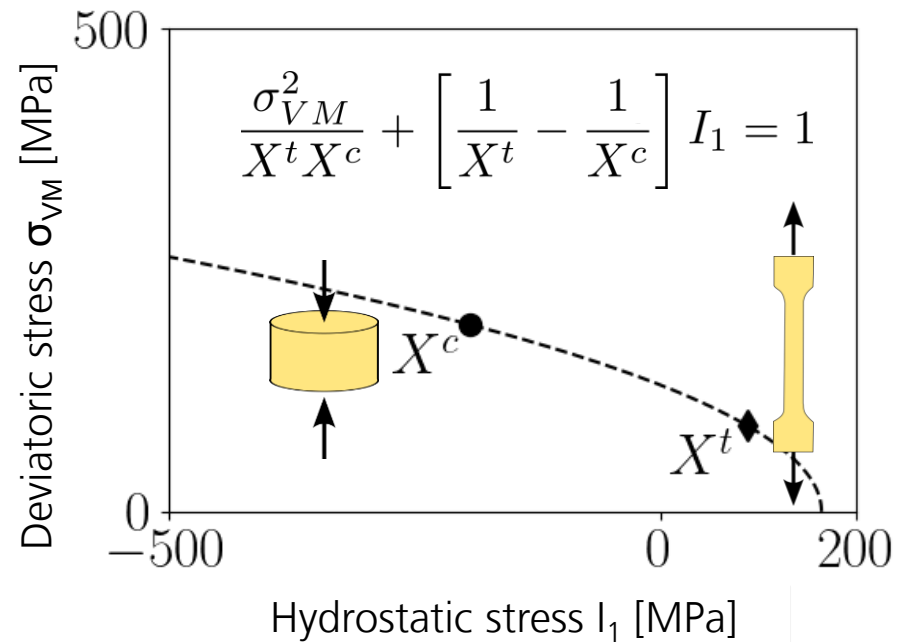
[3] Hobbiebrunken et. al., 2006. DOI: 10.1016/j.compositesa.2005.12.021

Material behavior of epoxy

Experimental characterization

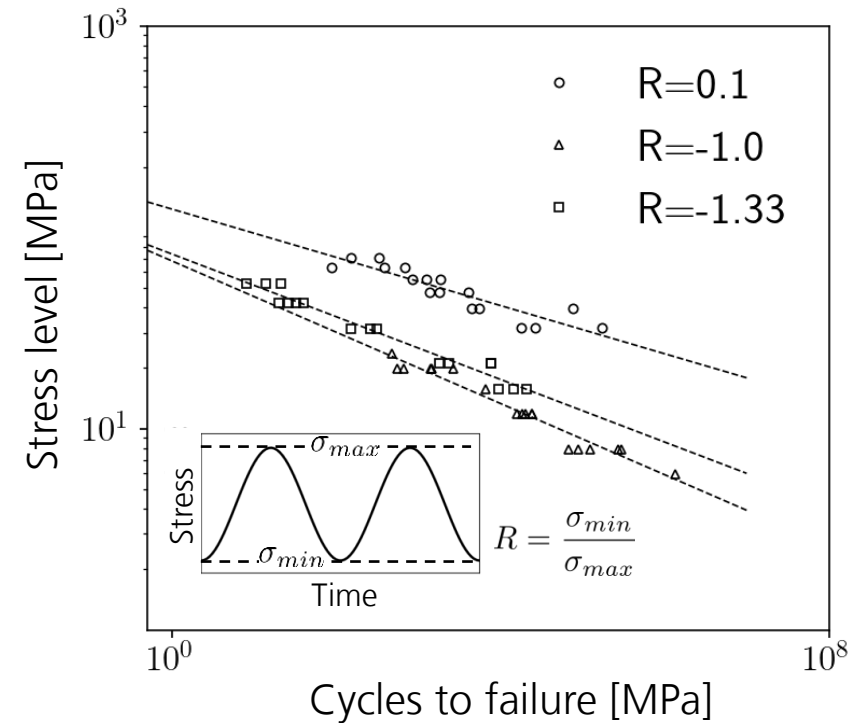
Quasi-static testing

Pressure dependent failure



Cyclic testing

Mean stress sensitivity

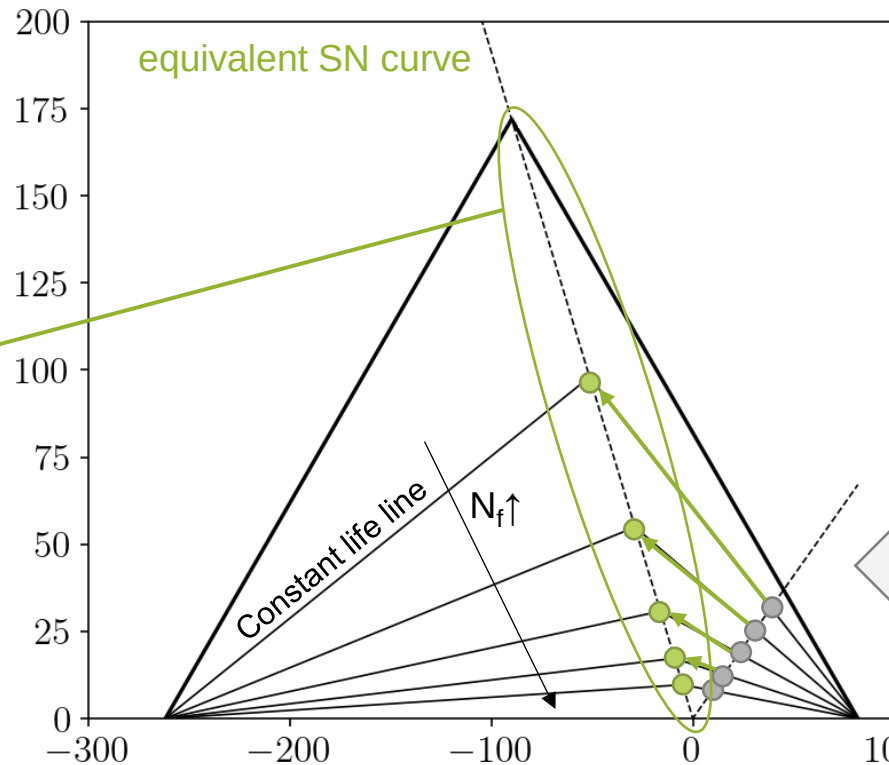
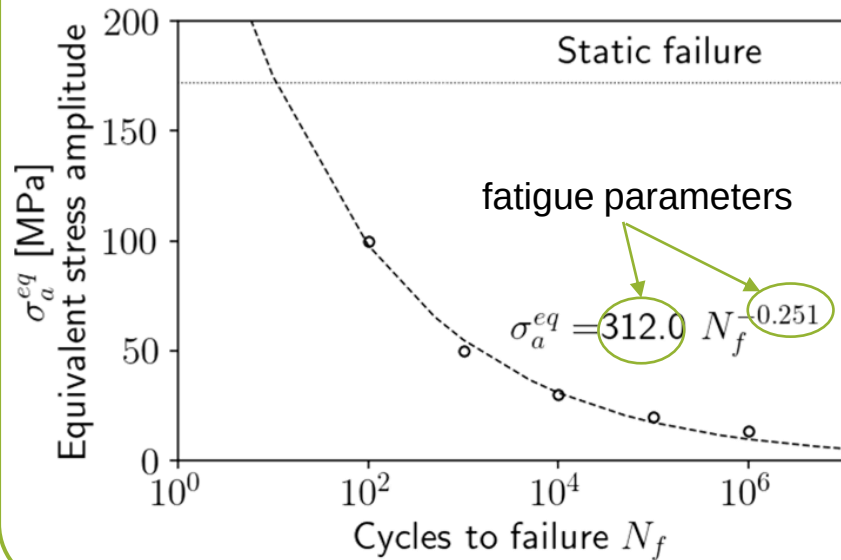


[4] Stassi-D'Alia, 1967. DOI: 10.1007/BF02128173

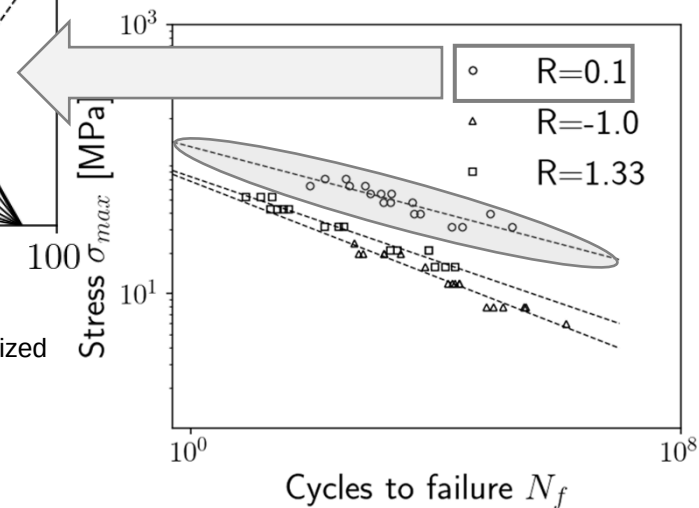
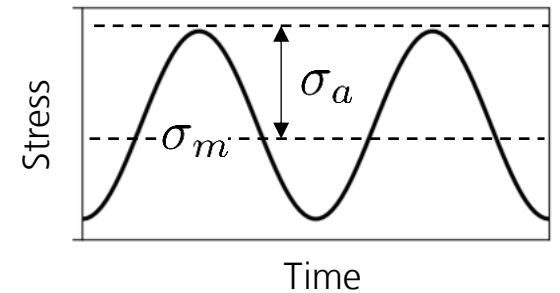
Material behavior of epoxy

Modelling mean stress effect

Equivalent SN curve



[5] Kawai et. Al., 2007, 10.1016/j.compositesa.2007.01.016; linearized



Material behavior of epoxy

Multiaxial stress states

Testing & calibration based on uniaxial stress state

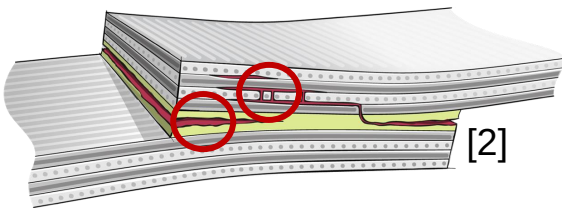


$$\underline{\underline{\sigma}} = \begin{bmatrix} \sigma_{11} & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\sigma_a^{eq} = 312 \cdot N_f^{-0.251}$$

Multiaxial stress state in adhesive and composite

$$\underline{\underline{\sigma}} = \begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix}$$



[2]

Transfer multiaxial stress state → equivalent uniaxial stress

$$\sigma^{eq} = \sigma_1^{eq}$$

← $I_1 \geq 0$ tensile stress

$$\sigma^{eq} = -|\sigma_2^{eq}| \cdot \kappa$$

← $I_1 < 0$ compression stress

$$\frac{\sigma_{VM}^2}{\kappa(\sigma^{eq})^2} + \left[\frac{1}{\sigma^{eq}} - \frac{1}{\kappa\sigma^{eq}} \right] I_1 = 1$$

$$\frac{\sigma_{VM}^2}{\kappa(X^t)^2} + \left[\frac{1}{X^t} - \frac{1}{\kappa X^t} \right] I_1 = f$$

$$\frac{\sigma_{VM}^2}{X^t X^c} + \left[\frac{1}{X^t} - \frac{1}{X^c} \right] I_1 = f$$

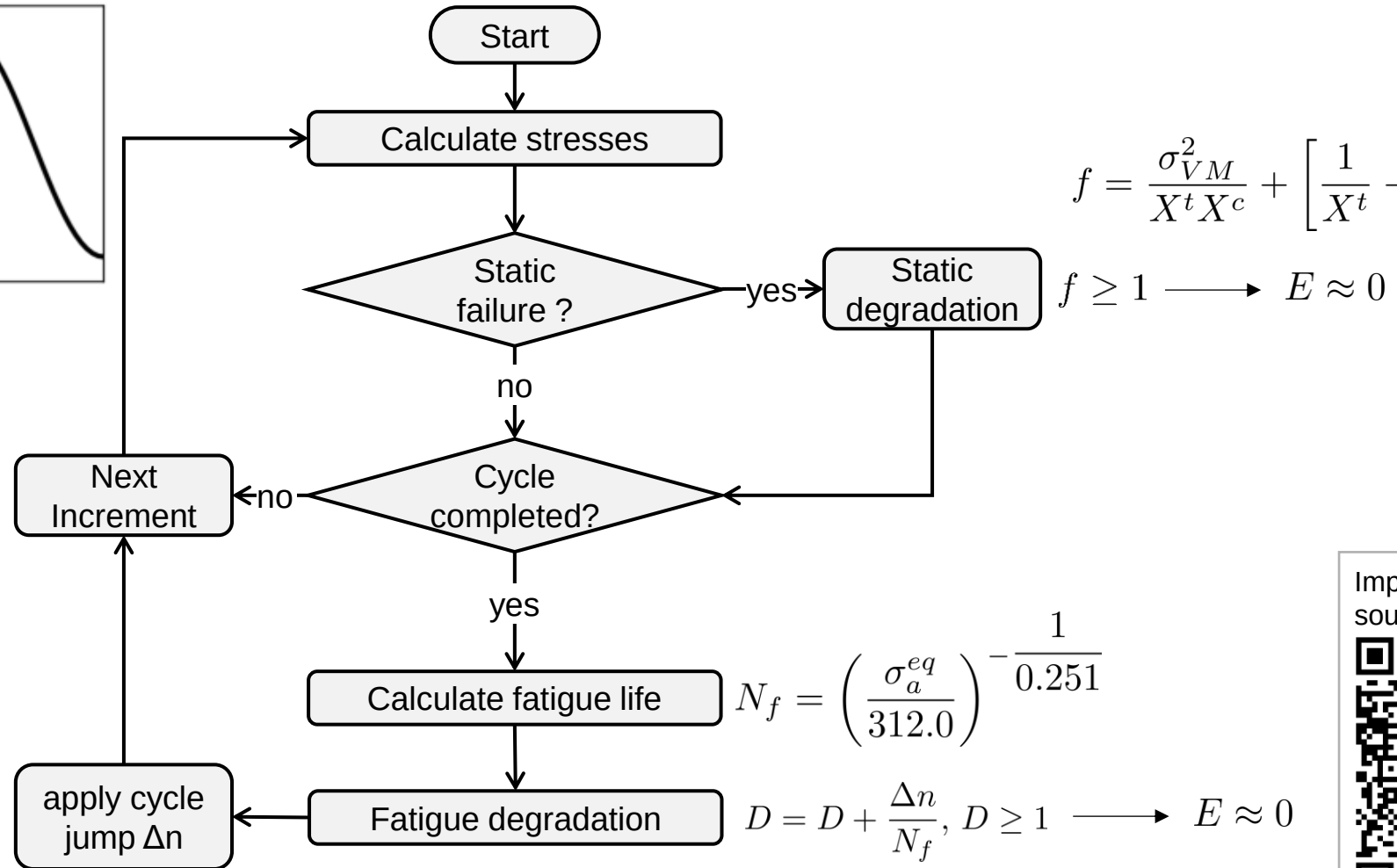
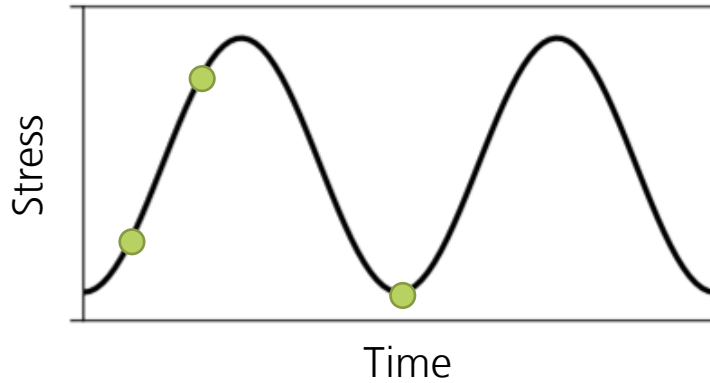
$X^t \Rightarrow \sigma^{eq}$

$X^c = \kappa X^t$

[2] Völkerink, 2022, DOI: 10.57676/hya4-2a09

[6] Tao et. al., 2009, DOI: 10.1016/j.ijfatigue.2008.03.025

Modelling framework

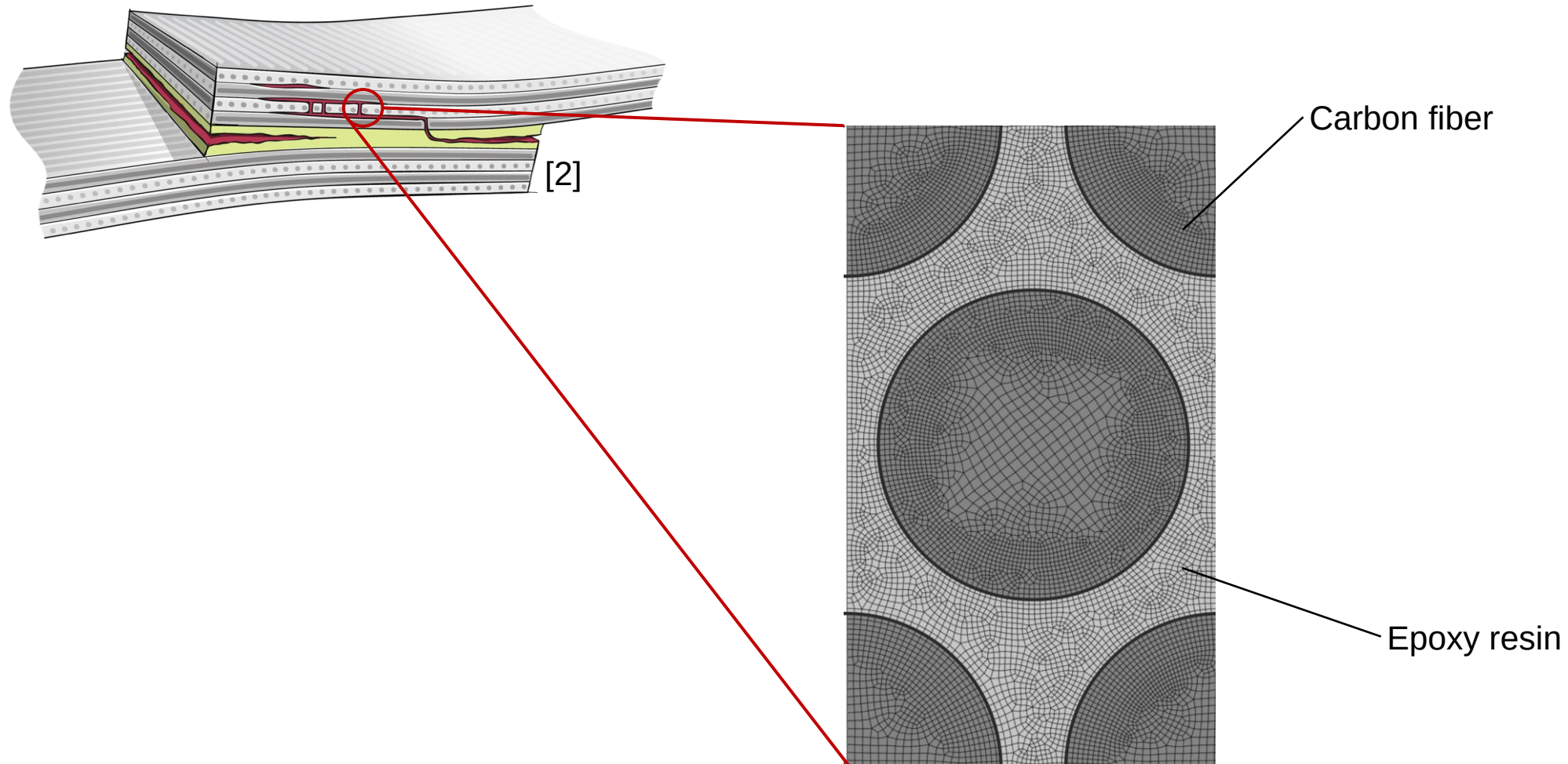


Implemented in open source code MCODEAC



Predicting FRP* fatigue behavior

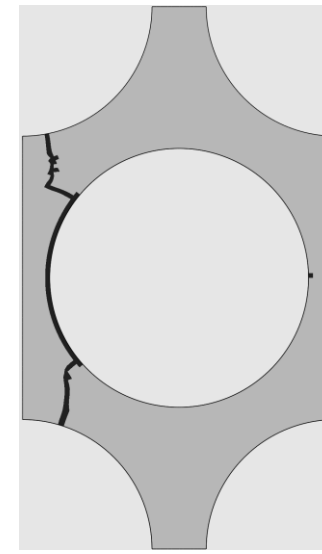
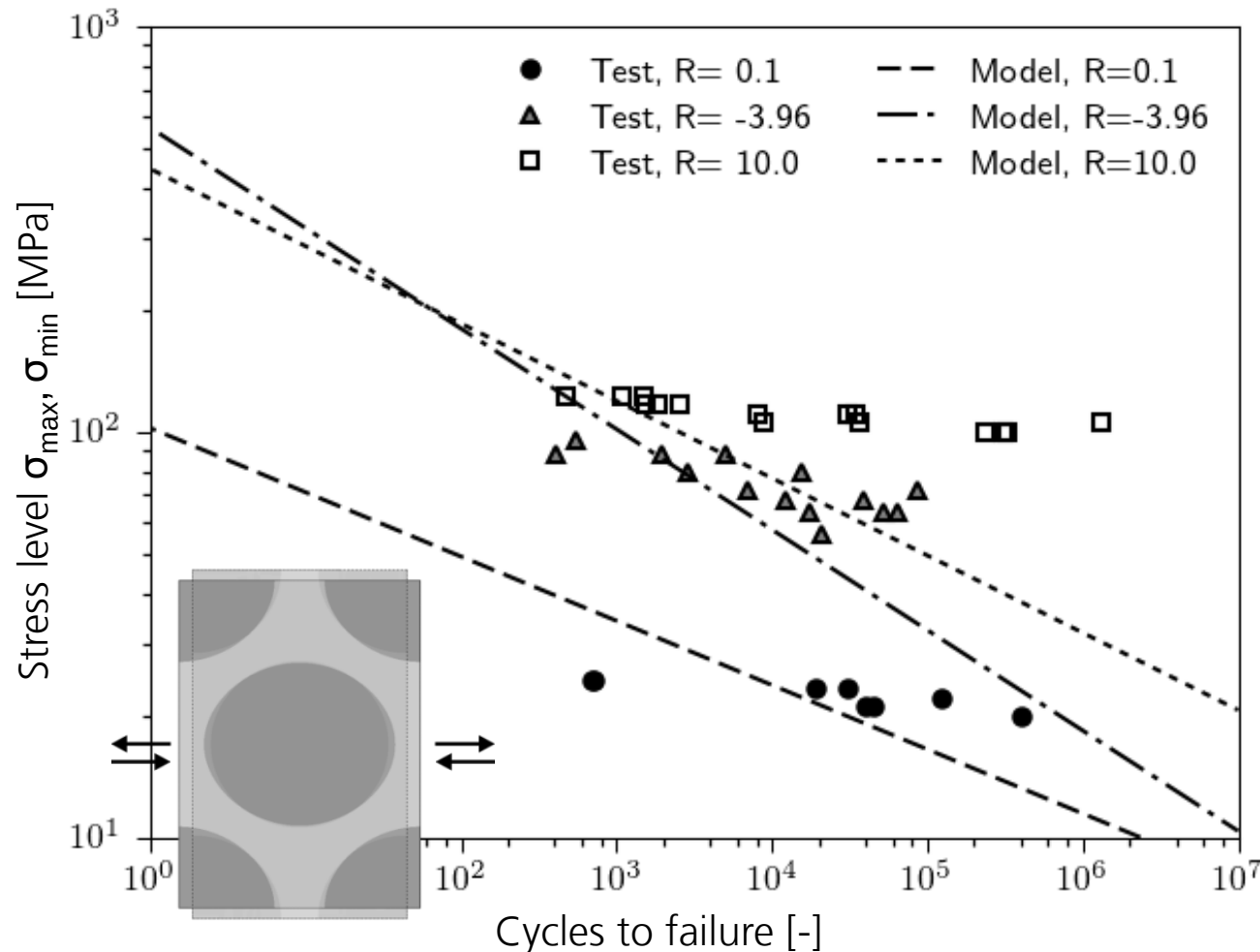
Representative Volume Element (RVE)



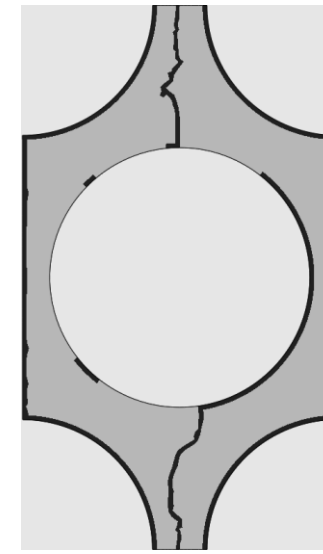
[2] Völkerink, 2022
DOI: 10.57676/hya4-2a09

Predicting FRP* fatigue behavior

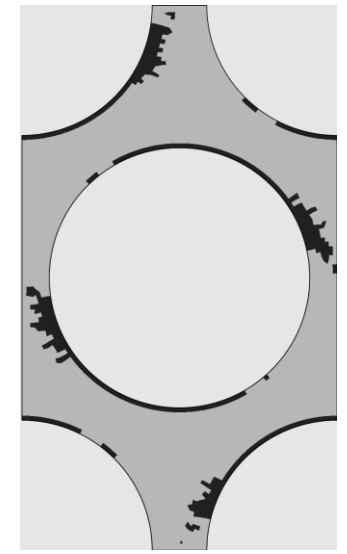
Transverse loading



R=0.1



R=-3.96



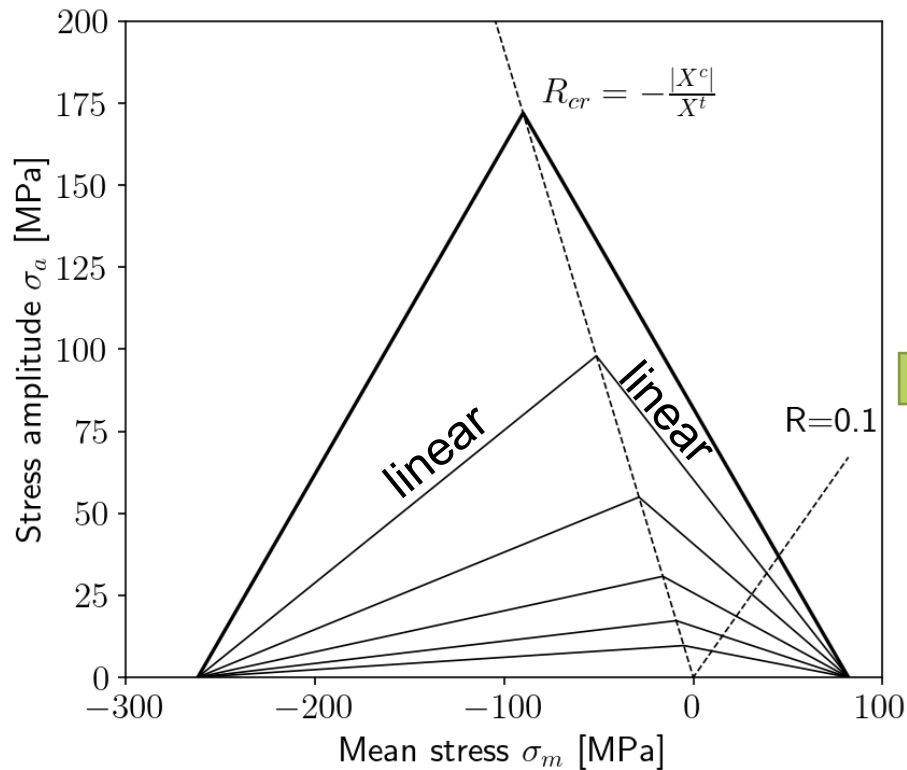
R=10

Mean stress sensitivity qualitatively captured.

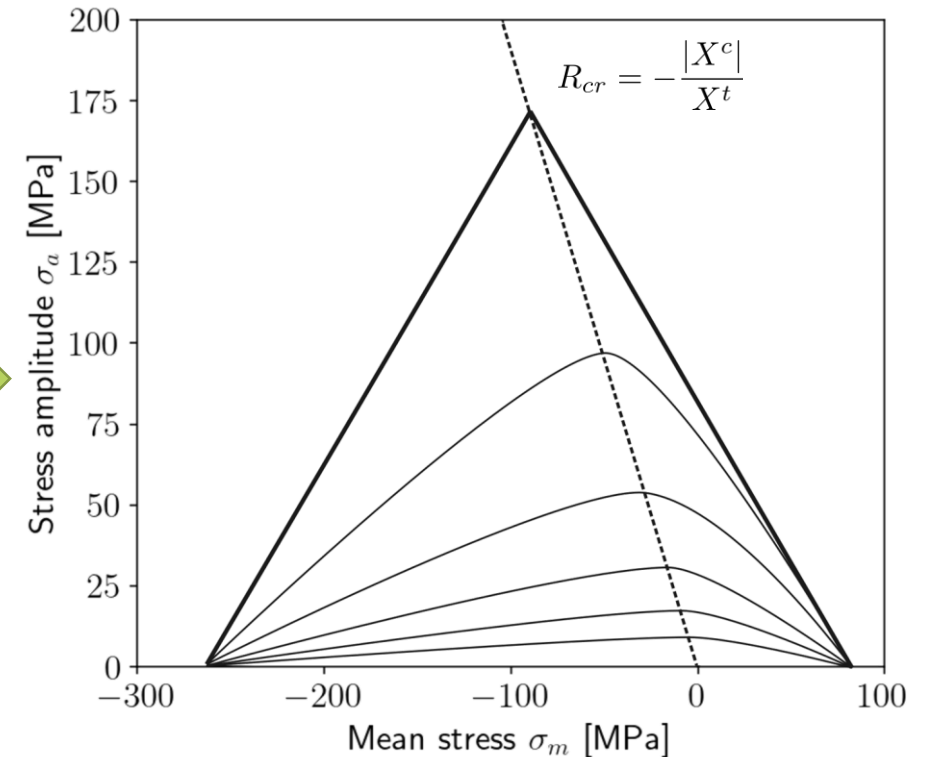
Fatigue strength underestimated in regime of higher cycles.

Challenges of stress-based fatigue modelling

Mean stress sensitivity



Nonlinear CLD



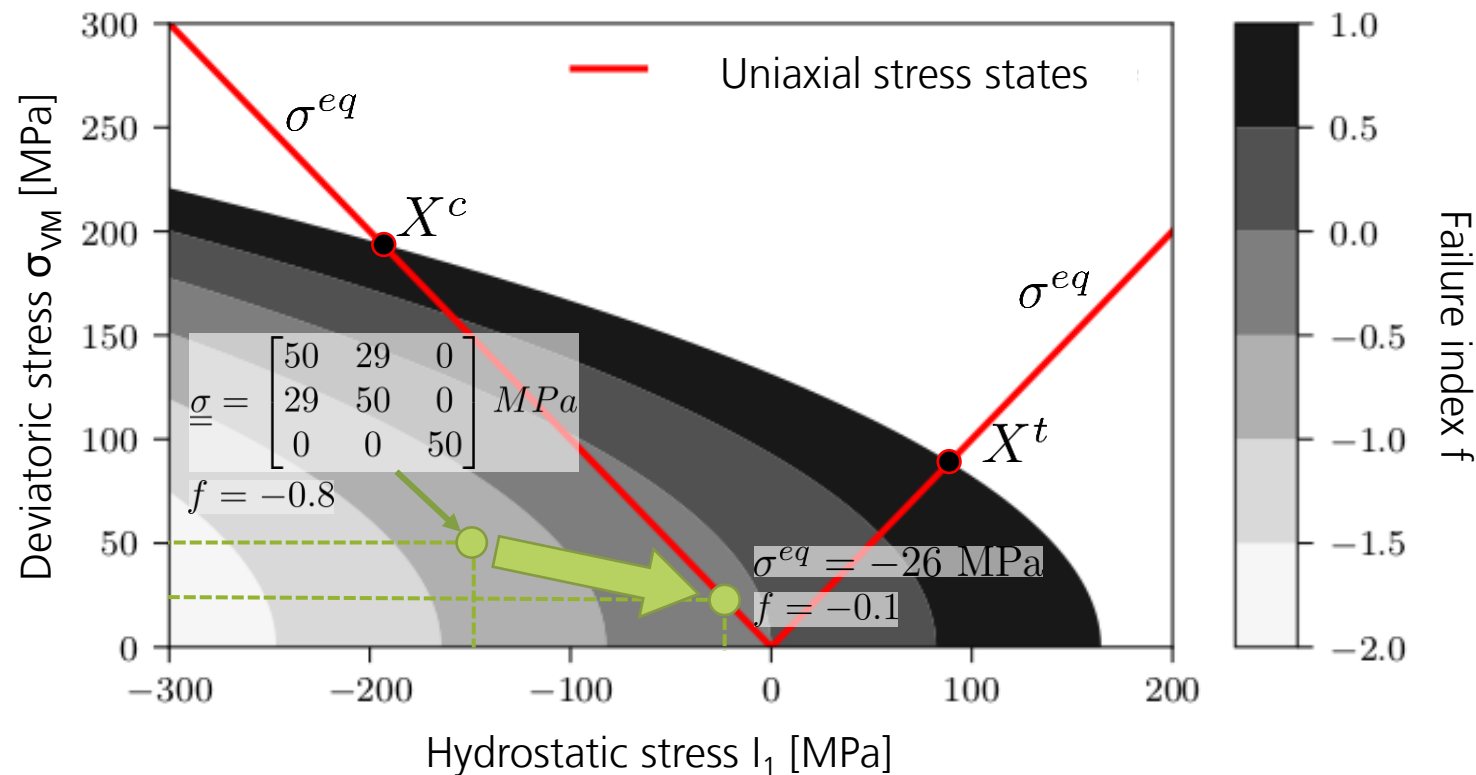
Fatigue strength underestimated at higher number of cycles [5]

→ SN curve for R_{cr} needed

[5] Kawai et. al., 2007, 10.1016/j.compositesa.2007.01.016

Challenges of stress-based fatigue modelling

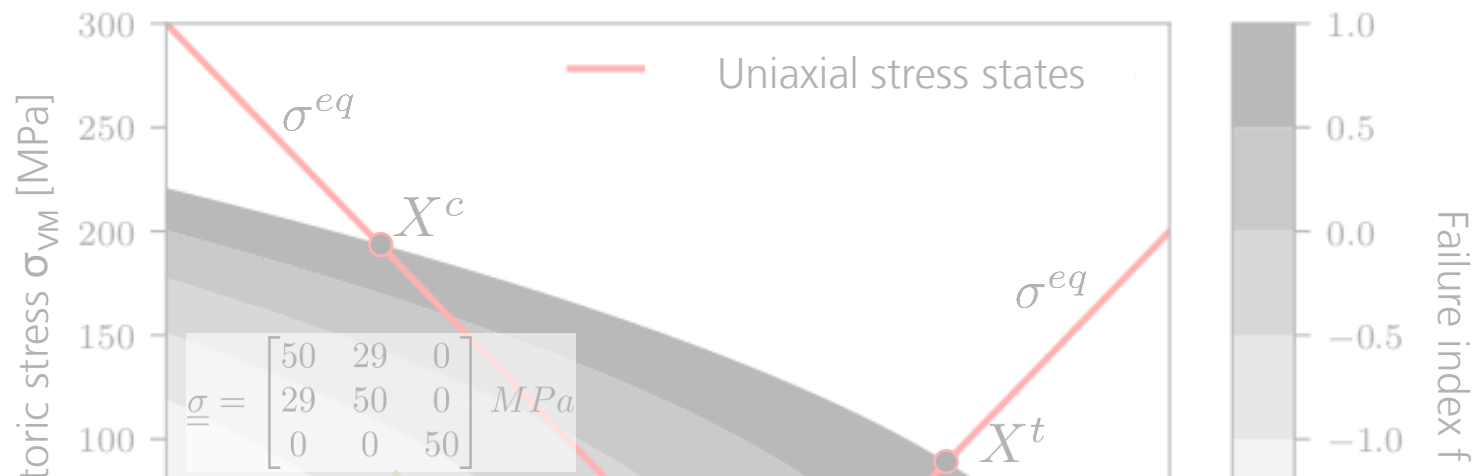
Equivalent uniaxial stresses



$$f = \frac{\sigma_{VM}^2}{X^t X^c} + \left[\frac{1}{X^t} - \frac{1}{X^c} \right] I_1 \quad [4]$$

Conclusion

Equivalent uniaxial stresses



$$f = \frac{\sigma_{VM}^2}{X^t X^c} + \left[\frac{1}{X^t} - \frac{1}{X^c} \right] I_1 \quad [4]$$

Proposed fatigue damage model captures mean stress effect of pure epoxy and epoxy composites qualitatively.

Drawbacks related to stress-based modelling have to be overcome.

Hydrostatic stress I_1 [MPa]

**Many thanks for your Attention!
Any Questions?**

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publications

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