

SIMULATION-BASED EVALUATION OF THE MANUFACTURING PROCESS OF AN AIRCRAFT FIN BASED ON THERMOMECHANICAL MEASUREMENTS

Robert Hein, 05.05.-07.05.2025

Regional User Meeting – EuroCentral - Bamberg

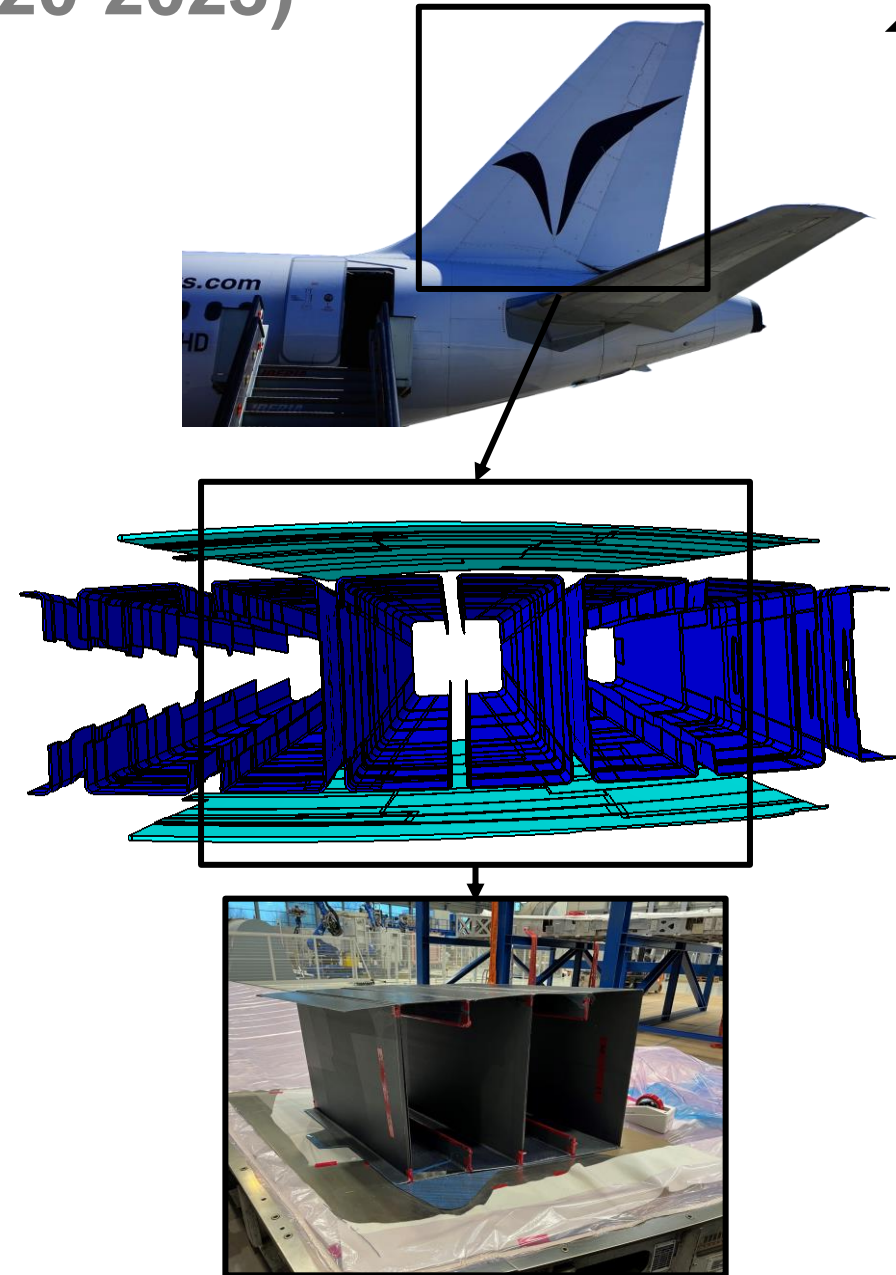
AIRBUS


BROETJE
AUTOMATION

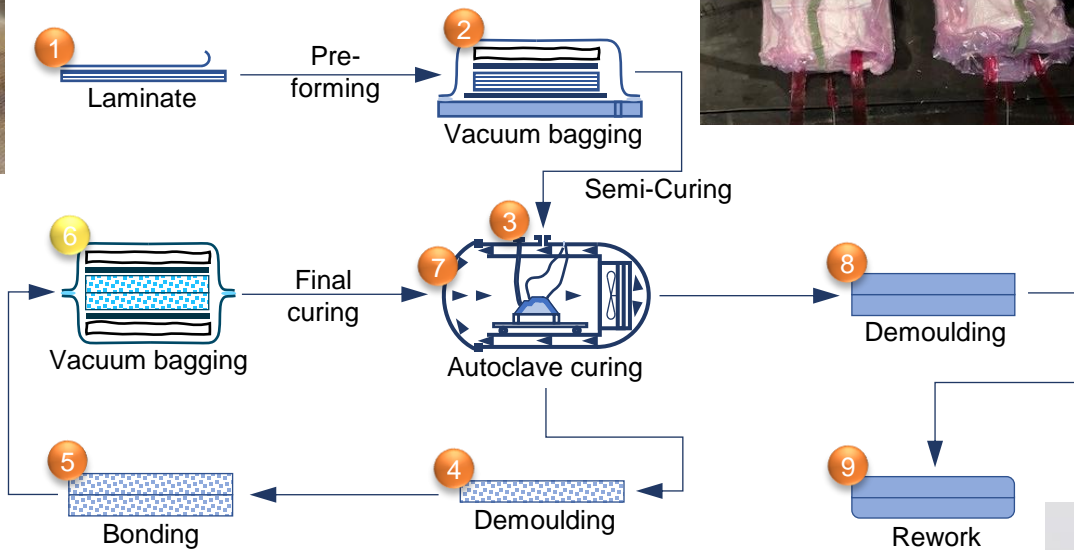
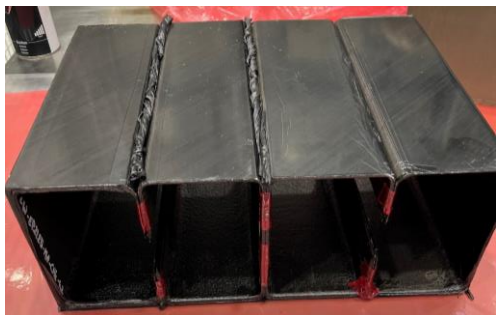

DLR

Motivation – Project LEITWERK (2020-2023)

- Development of a new process route for multi-spar concept for an aircraft fin
- Typical challenges of full integral manufacturing are the need for complex tooling designs
- Innovative approach: Multi-step cure process

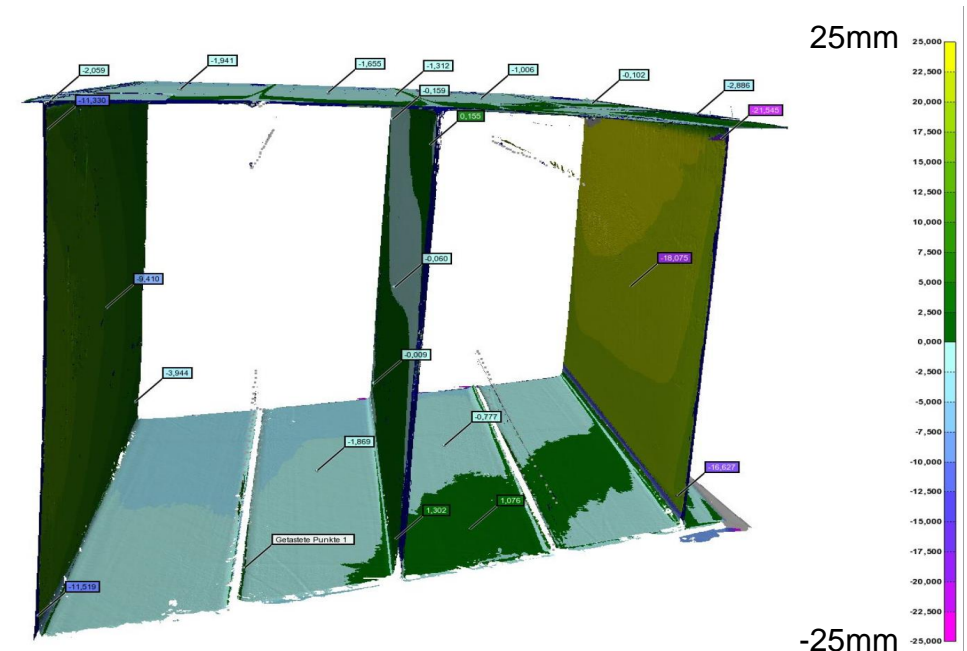
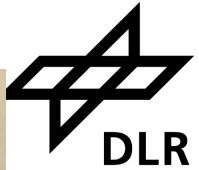
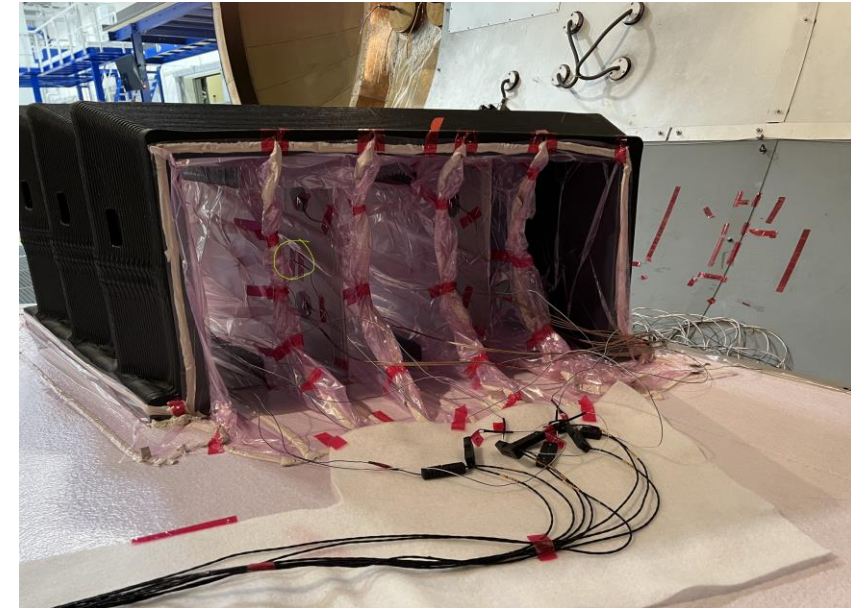


Motivation - Project LEITWERK (2020-2023)



Motivation – Challenge

- Demonstrator with unexpected high part deformations observed
- Research Question: What are the causes for the high part deformations observed?
- Manufacturing process simulation can be beneficial to provide answers



25mm

-25mm

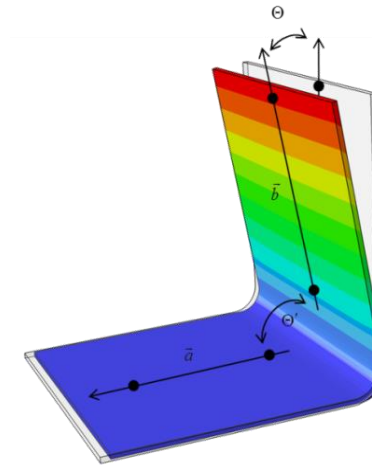
Outline



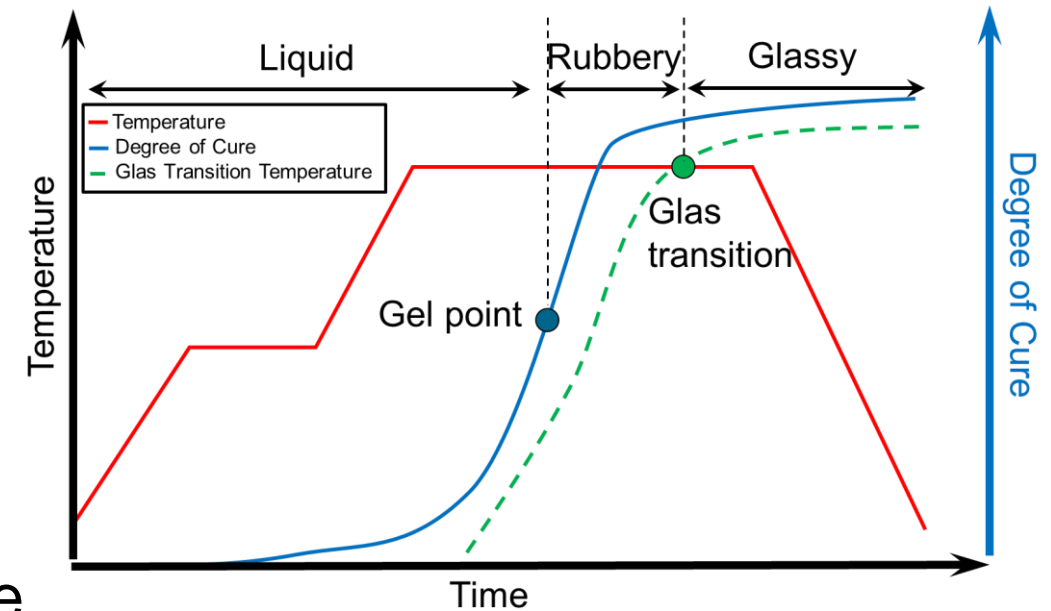
- Simulation challenge
- Material characterization and model calibration
- Simulation approach
- Comparison with measurements
- Summary

Simulation Challenge

- Objective: Prediction of process-induced part deformation (PID) in order to derive distortion-compensating tool design
- Multi-physics problem
 - Chemical shrinkage
 - Anisotropic thermal shrinkage
 - Different material states (liquid, rubbery, glassy)
 - Stress relaxation
 - Tool-part interactions
- Stiffness = f (Degree of Cure X, Temperature, Time)



PID (Spring-in) of L-shaped specimen

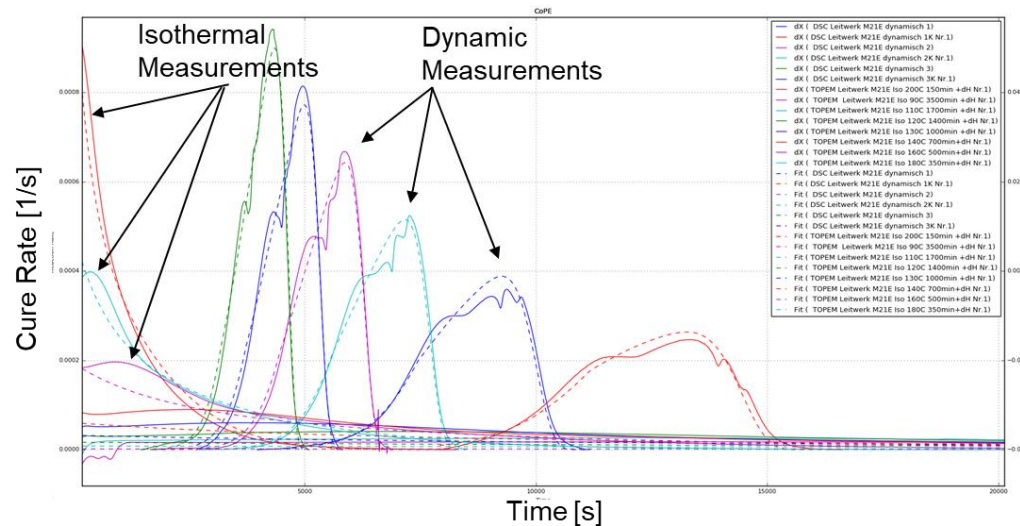


Material characterization: Reaction Model

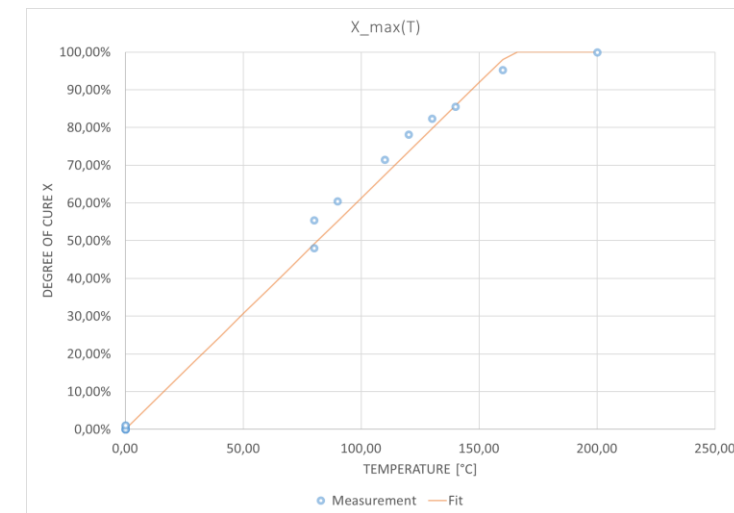
- Fit of a reaction model to DSC measurements
- Cure model: $A \xrightarrow[k_2]{k_1} B, C, \frac{dX}{dt} = k(T) \cdot f(X), k_i = A_i \exp\left(\frac{-E_{Ai}}{RT}\right)$
- $\frac{dX}{dt} = k_1(X_{max} - X)^l + k_2 X^m (X_{max} - X)^n$



CoPE – Inhouse Fitting Tool for Cure Kinetics

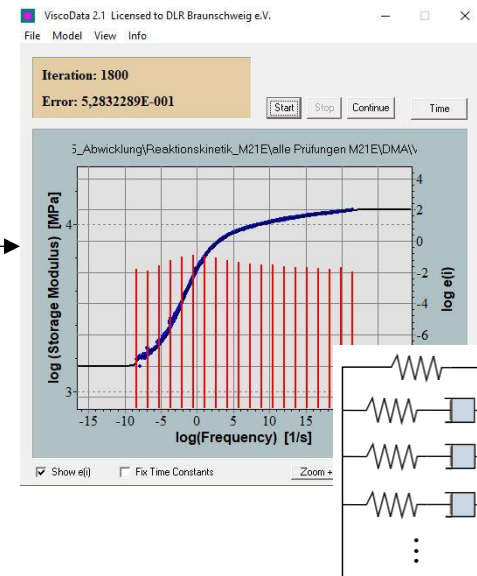
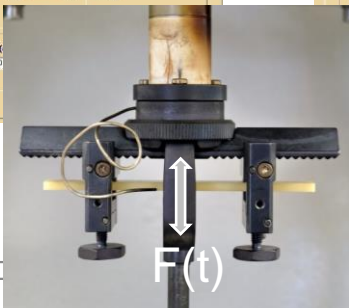
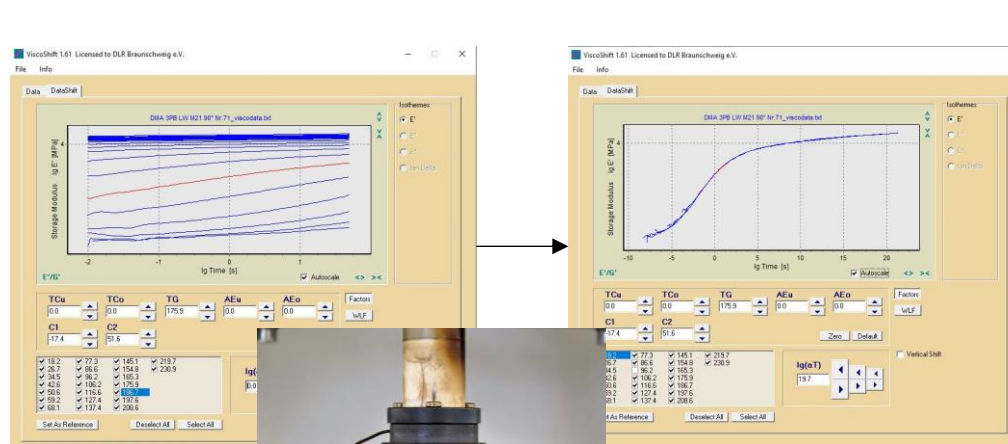


X_{Max} -Function covers diffusion-controlled reactions

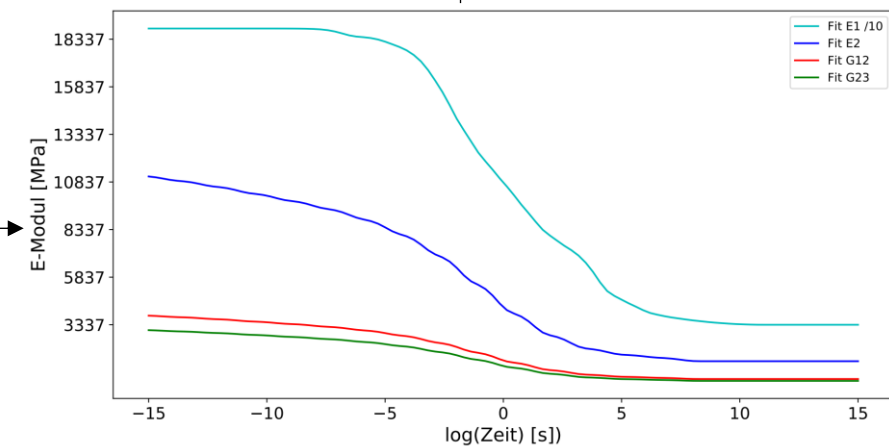


Material characterization: Temperature and Time Dependency (UMAT)

- Development of a viscoelastic material model from DMA measurements
 - Construction of master curve (0° and 90°)
 - Fit with prony-series
 - Calculation of master curves
 - Generation of material card

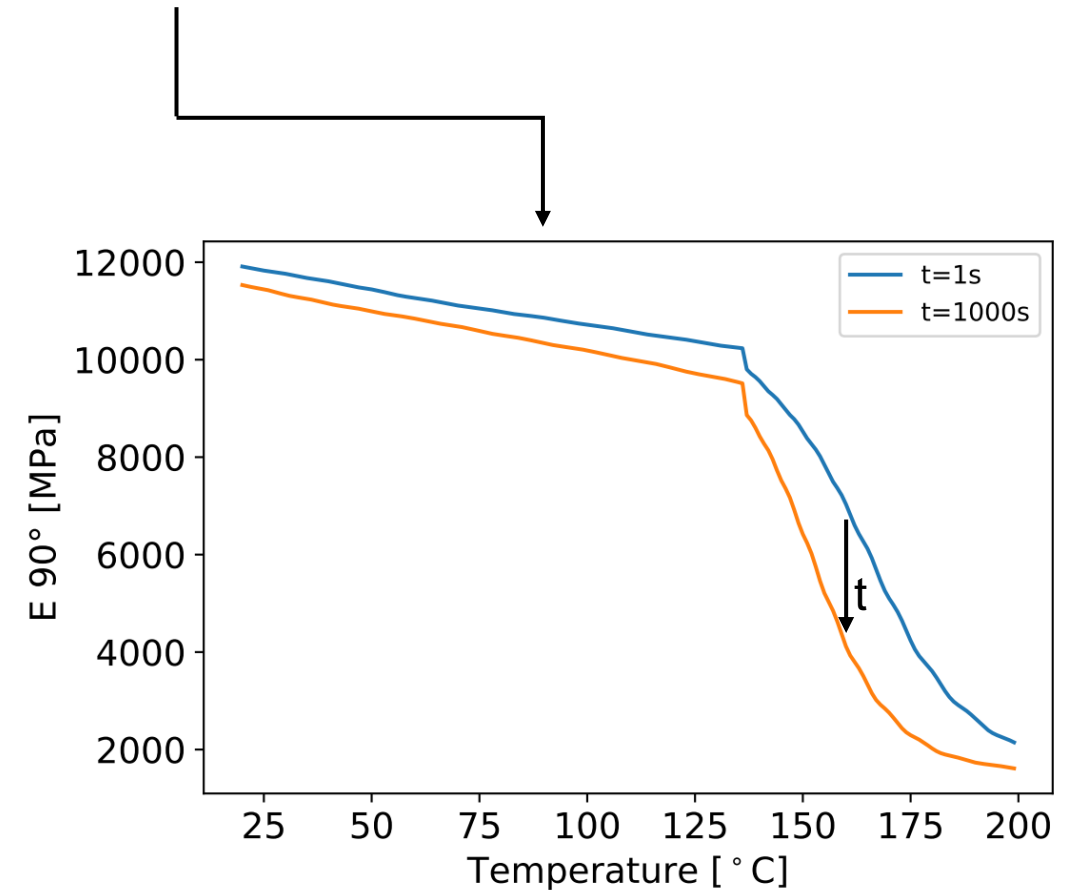
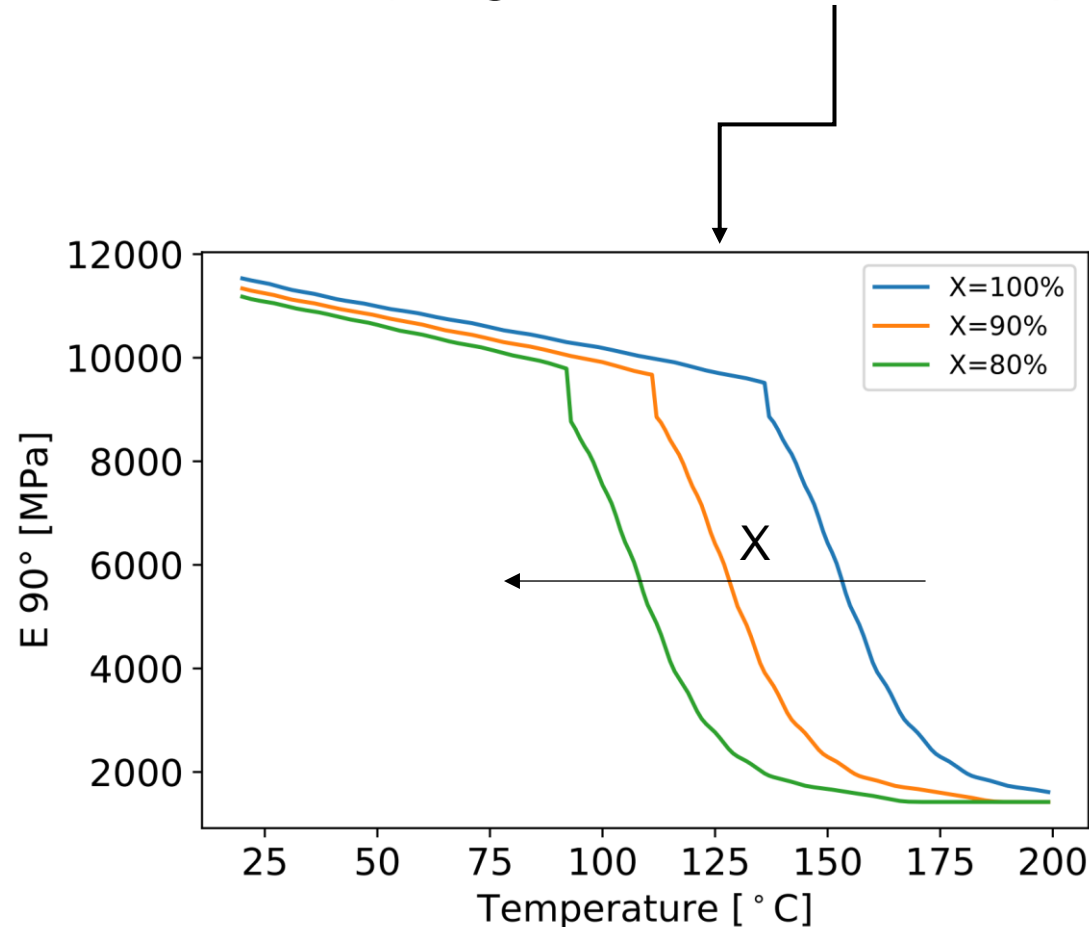


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*Depvar CRLE
500 CRLE
*User Material, constants=228 CRLE
.....13,.....24,.....24,
.....3162.0568055,.....4294.3253968,.....0.00490771,
.....0.149882,.....2756.78,.....0.134074,
.....0.0194822,.....0.666365,.....0.00455366,
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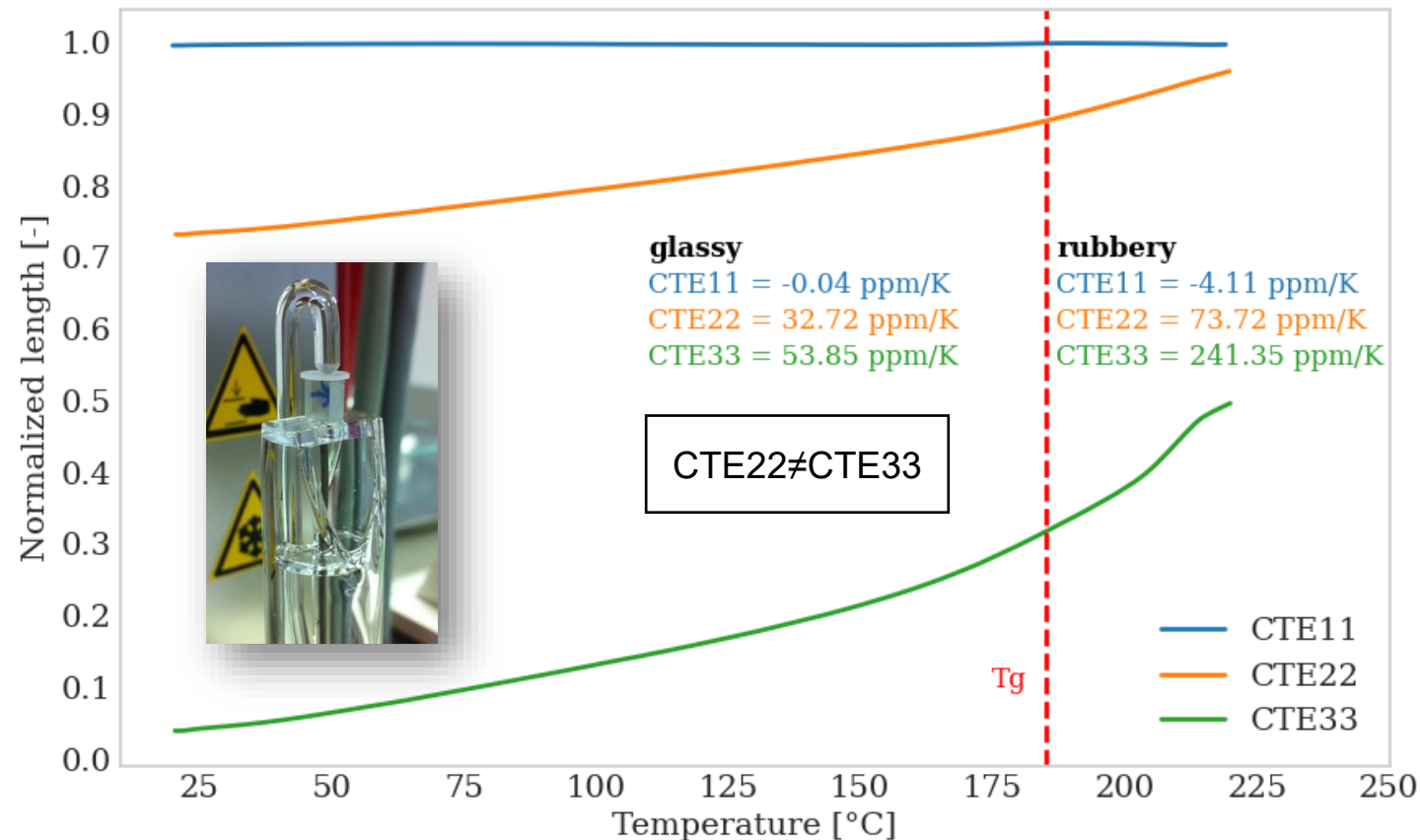
Material characterization: Cure and Time Dependency

- Stiffness = f (Degree of Cure X, Temperature, time)



Material characterization: Further thermal Mechanical Properties (UEXPAN)

■ Coefficient of Thermal Expansion (CTE) by TMA



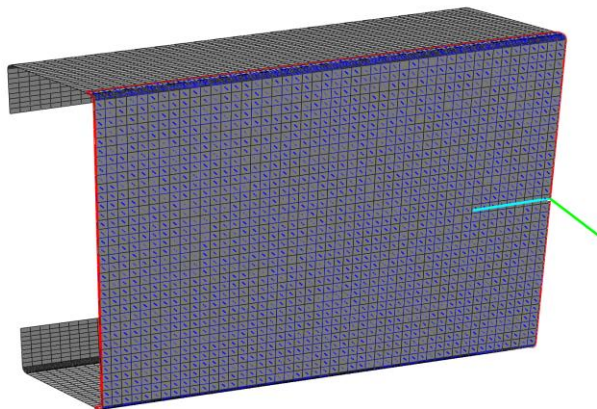
Not shown:

- Heat Capacity by DSC
- Thermal Conductivity
- Density
- Fiber Volume Fraction

Simulation Approach

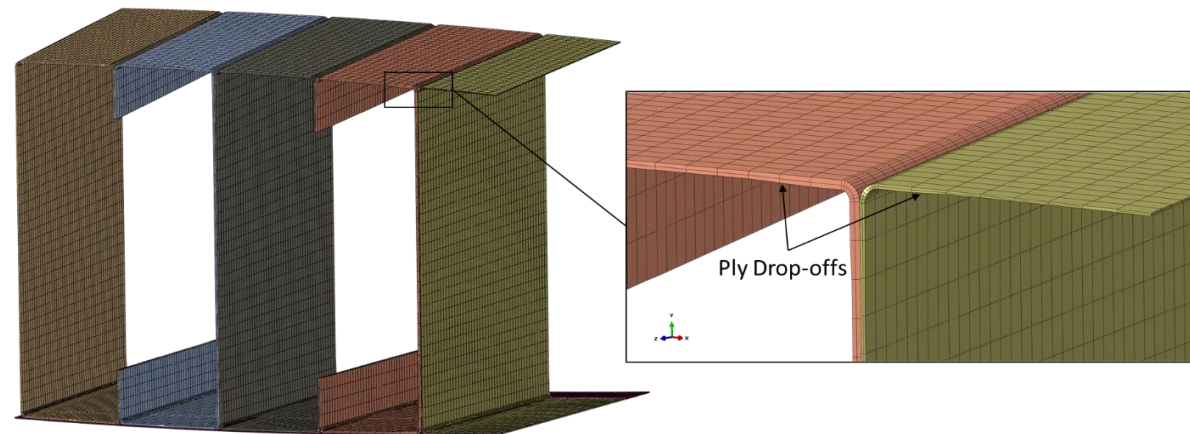
- Sequentially coupled temperature-displacement analysis
- Ply-based model according manufacturing process (Abaqus CMA for CAE)
 - Draping effects
 - Thickness variations through ply-drops
- Extrusion to solid model and assembling by tie constraints

Simple Geometries



Assembling
→

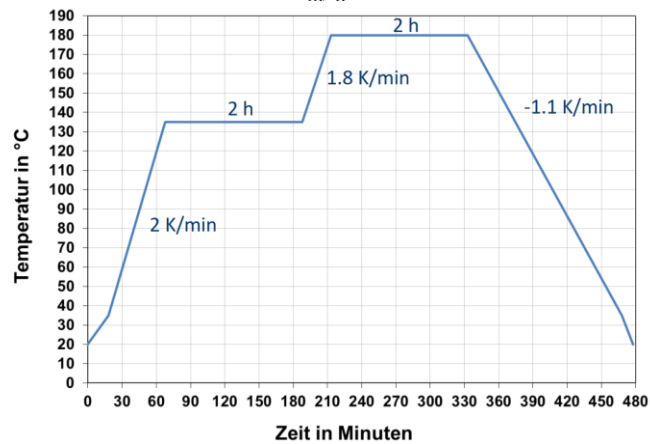
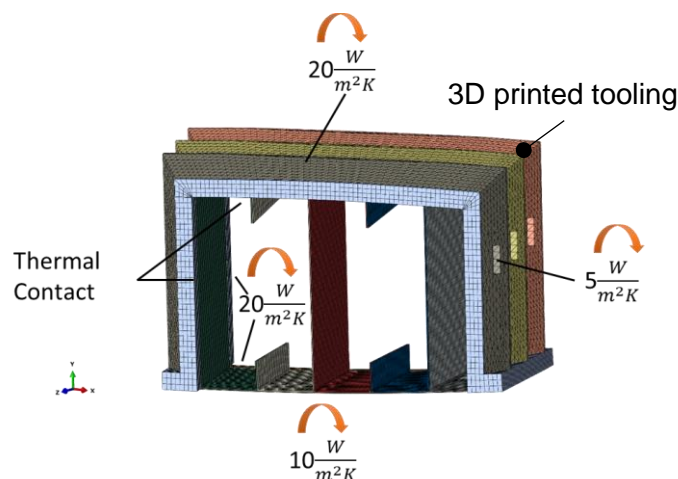
Final Demonstrator



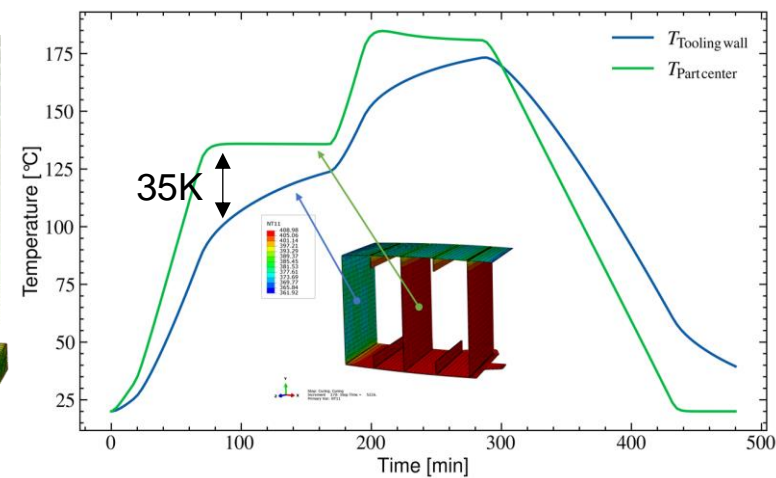
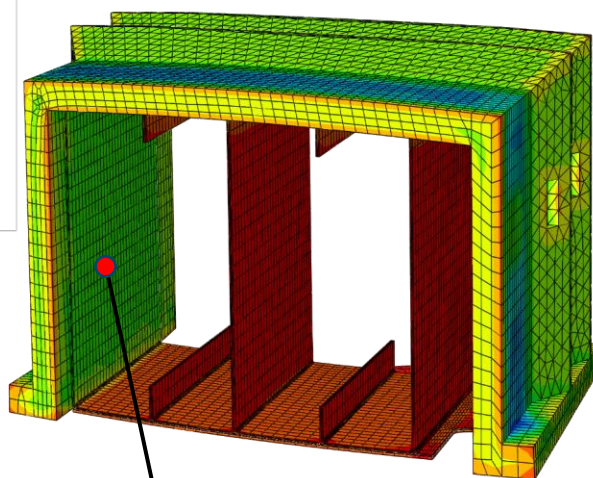
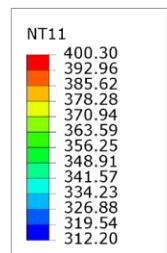
Simulation Approach – Thermal Analysis



Thermal BC



Temperature distribution for isothermal curing at 135°C

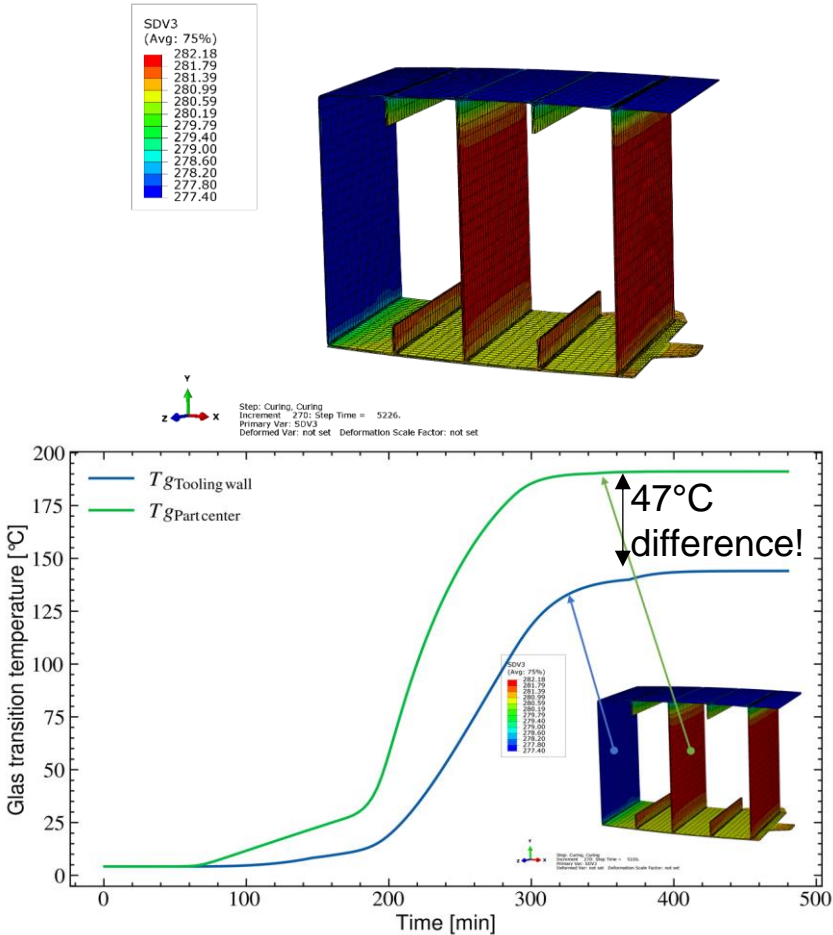
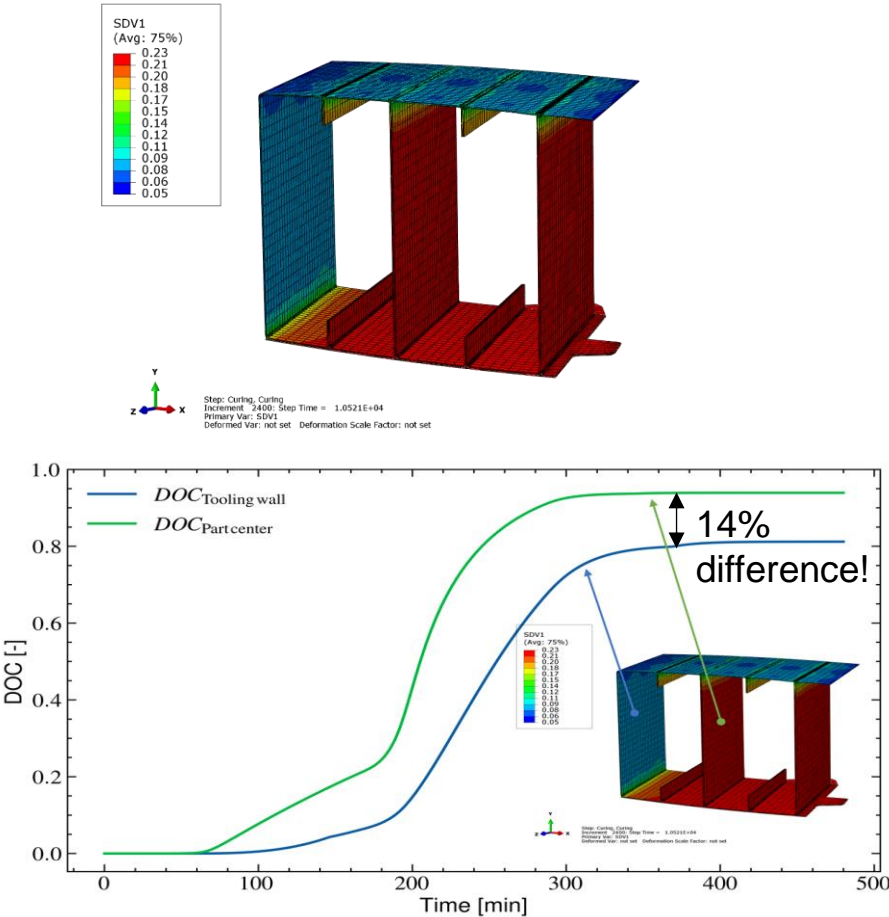


Tool contact result in inhomogenous heating ($\Delta T=35K$)

Simulation Approach – Curing state

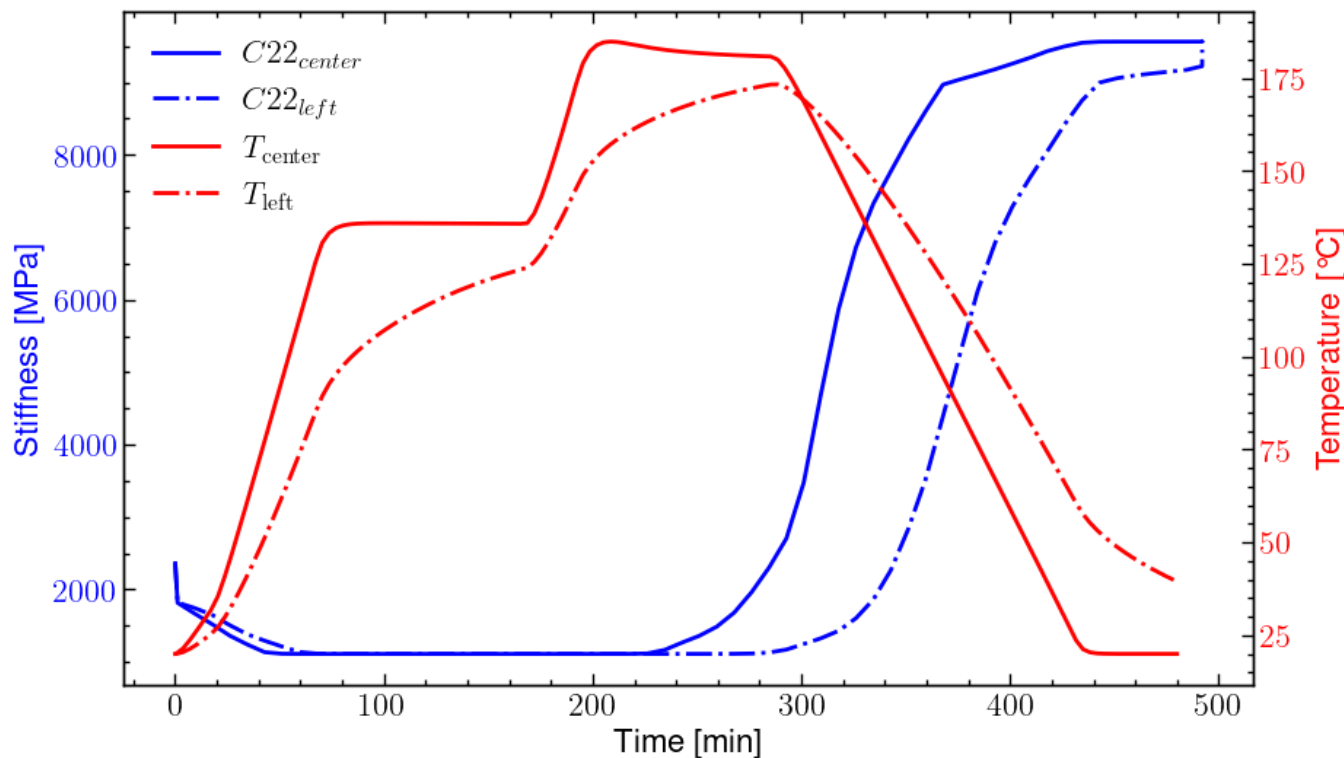
Inhomogenous and insufficient curing

Inhomogenous glass transition temperature



Simulation Approach – Stiffness Development

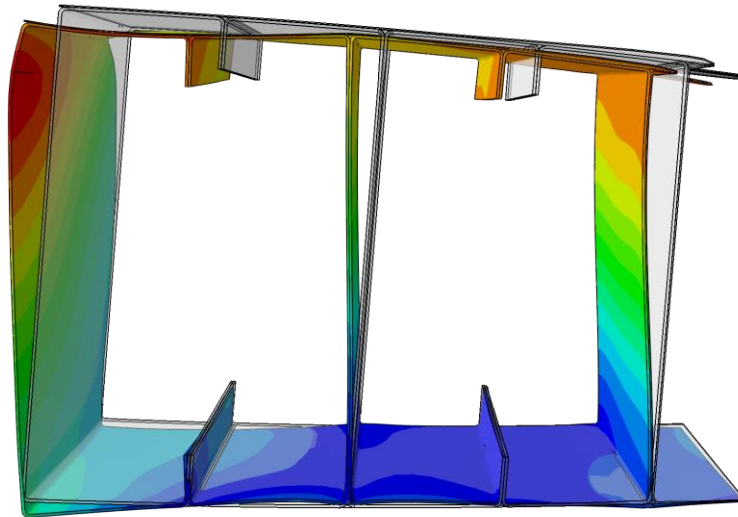
Stiffness in fiber cross direction



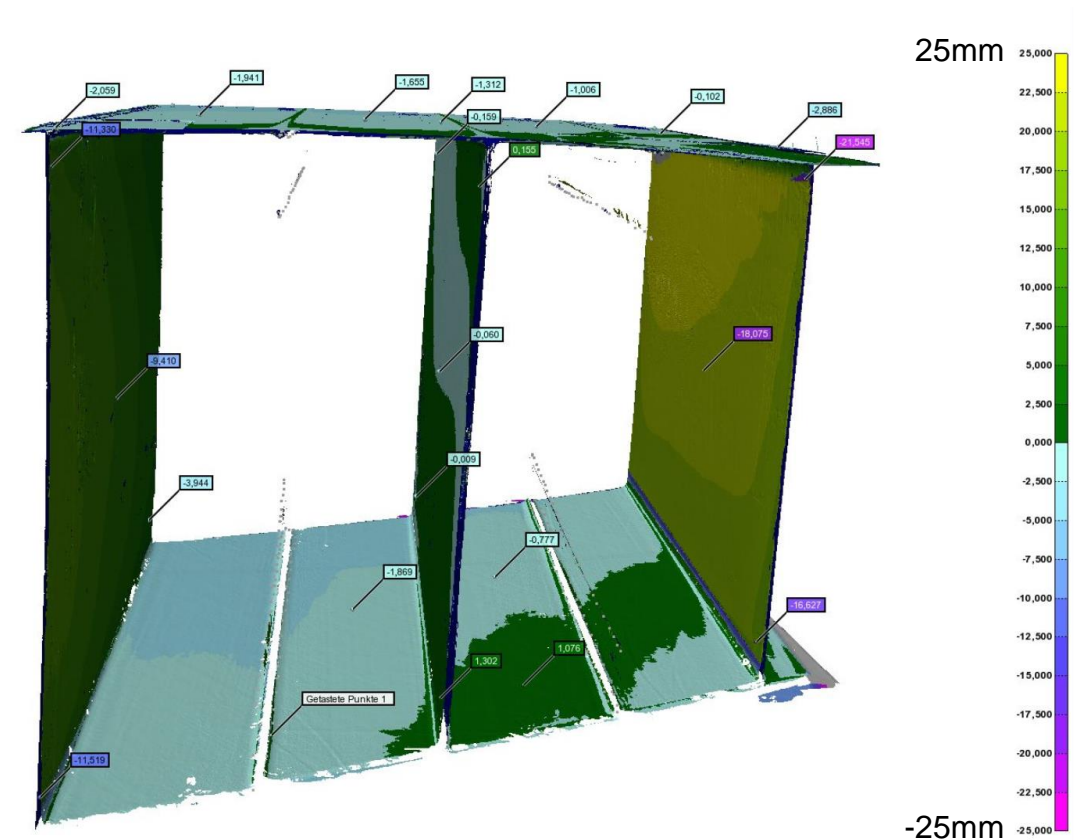
Inhomogeneous temperature leads to:

- Shifts in the development of stiffness
- Regions with different stiffnesses
- Reduction in absolute stiffness

- U, Magnitude

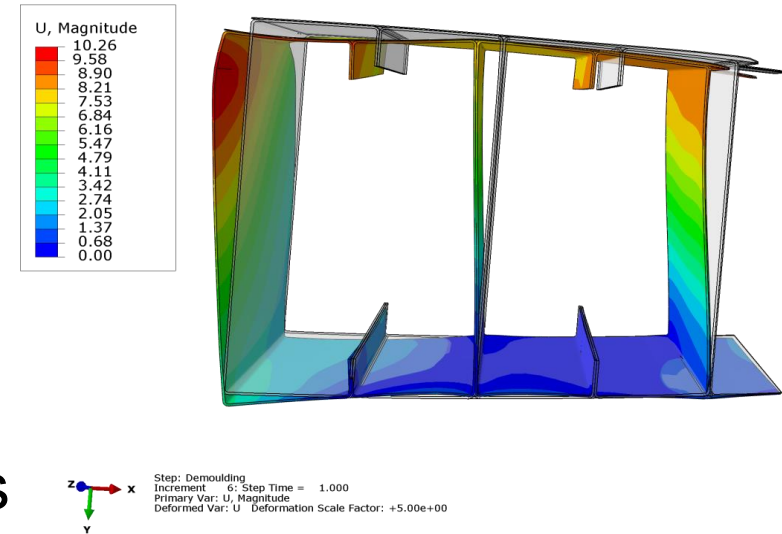


Step: Demoulding
Increment 6: Step Time = 1.000
Primary Var: U, Magnitude
Deformed Var: U Deformation Scale Factor: +5.00e+00



Summary and Conclusion

- Introduction of a novel multi-step cure process
- High part deformation observed
- Multi-physic process simulation developed
- Basis are thermomechanical measurements
- Inappropriate tooling design result into inhomogeneous curing and caused high part deformations
- Process simulation exhibit significant potentials for improvements



Contact



Thank you for your attention.

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