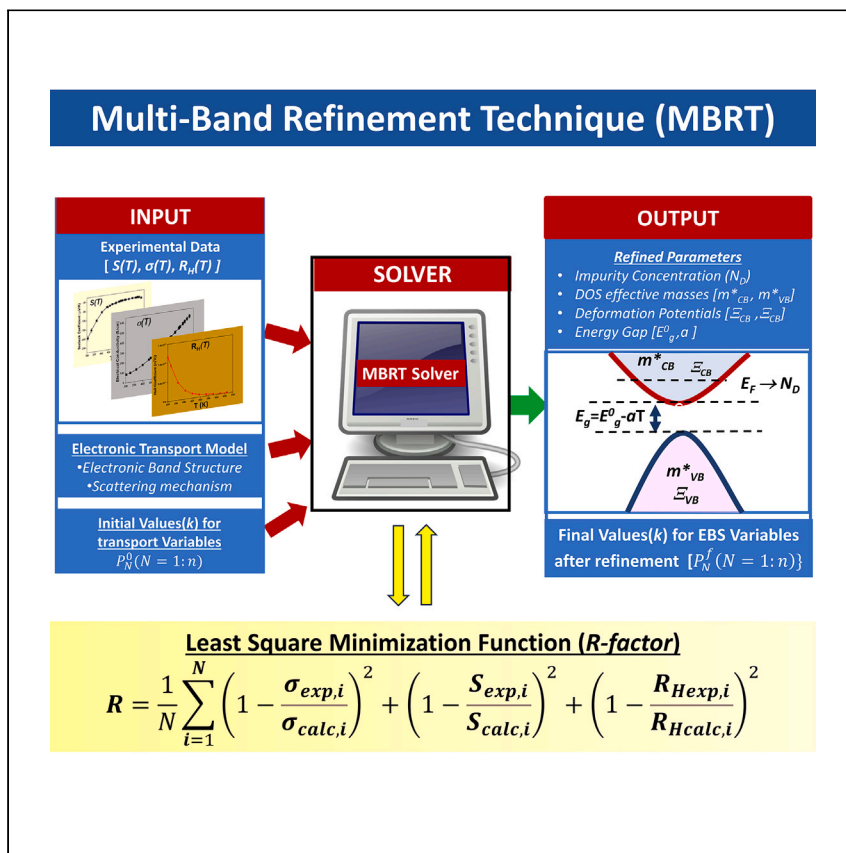


Article

# A multi-band refinement technique for analyzing electronic band structure of thermoelectric materials



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Highlights

Refinement-based approach for extracting electronic band structure information

Experimental data of electrical properties and a transport model as inputs

Applicable to semiconductors with multiple-band-dominated charge transport

Method validated using silicon and magnesium silicide

Agrawal et al. report a multi-band refinement technique for analyzing the electronic band structure of thermoelectric materials. They demonstrate that the effects of temperature, doping, and alloying on the electronic band structure and scattering parameters can be easily captured by this technique.

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## Article

## A multi-band refinement technique for analyzing electronic band structure of thermoelectric materials

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## SUMMARY

Investigation of electronic band structure (EBS) plays a pivotal role in the advancement of thermoelectric materials and devices. Sophisticated experiments and theoretical calculations are required to obtain EBS information, representing a bottleneck in studying the vast and increasing number of thermoelectric materials. Herein, we propose a refinement-based approach, referred to as the multi-band refinement technique (MBRT), that combines routine laboratory measurements with computationally inexpensive calculations to acquire EBS information. Experimental data of electrical conductivity, Seebeck coefficient, and Hall coefficient along with an electronic transport model act as inputs. The MBRT solver uses this information to iteratively refine electronic structure and scattering parameters by a least-square minimization technique. The efficacy of the MBRT has been validated using silicon, an archetypal semiconductor, and Mg<sub>2</sub>Si, a well-known thermoelectric material. The results demonstrate that the MBRT can be a powerful tool for studying the effects of temperature, doping, and alloying on the EBS of thermoelectric materials.

## INTRODUCTION

Thermoelectric (TE) technology can be used to directly convert waste heat into electricity, making it an important avenue for renewable energy harvesting.<sup>1,2</sup> Discovery of efficient TE materials<sup>3,4</sup> can thus contribute to the reduction of fossil fuel consumption, which has a high carbon footprint. The performance of a TE material is defined by the dimensionless parameter<sup>5</sup>

$$zT = \frac{S^2 \sigma}{\kappa} T. \quad (\text{Equation 1})$$

Here,  $S$  is Seebeck coefficient,  $\sigma$  is electrical conductivity,  $\kappa$  is thermal conductivity, and  $T$  is absolute temperature. These TE properties are strongly influenced by charge-transport behavior. Thus, tuning of various electronic band structure parameters (which include Fermi level position, band effective mass, band degeneracy, band gap, inter-band separations) and scattering mechanisms<sup>5</sup> is essential for the development of high-performance TE materials. Historically, estimation of these parameters has been done using a combination of experimental techniques like cyclotron resonance,<sup>6–8</sup> Shubnikov-de Haas measurement,<sup>9</sup> angle-resolved photoemission spectroscopy (ARPES), and UV/infrared (IR) spectroscopy.<sup>10,11</sup> These methods have created a wealth of information on standard semiconductors like Si, Ge, and GaAs.<sup>12–14</sup> However, these experiments usually require high-quality single crystals and hence can be difficult to replicate on the vast number of known TE

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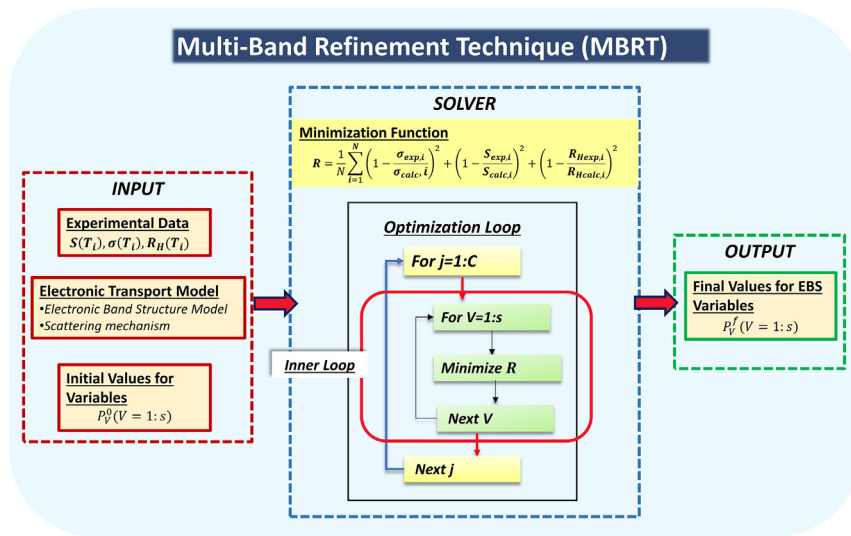
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compounds.<sup>15–17</sup> Further, these are niche experiments and cannot be performed using routine laboratory equipment. Thus, in recent years, there has been a shift toward first-principles-based theoretical methods for studying the electronic band structure of TE semiconductors.<sup>18</sup> These *ab initio* techniques can be used to calculate the energy dispersion near the band edge at 0 K and thus provide information about bands relevant to charge transport. Recent advances also indicate accurate estimation of carrier scattering rates from first-principles calculations.<sup>19</sup> However, there are limitations to these techniques that include under-estimation of the band gap and accuracy in strongly correlated systems. Thermal vibration of atoms also results in changes in their interaction with the charge carriers. Thus, various parameters associated with the electronic band structure (EBS) have a temperature dependence that needs to be taken into account for the calculation of charge-transport properties. Density functional perturbation theory (DFPT)<sup>20</sup> can be utilized for this but is computationally expensive, thereby limiting its usage. The other problem associated with traditional *ab initio* techniques is their limited ability to handle disorder/defects, which are inherently present in all materials. Thus, TE applications, which require temperature-specific EBS information, rely on experimental transport measurements like  $\sigma$ ,  $S$ , Hall coefficient, and Nernst coefficient.<sup>21</sup> The EBS information is then deconvoluted from these data using phenomenological models based on the Boltzmann transport equation.<sup>22–24</sup> This method has been shown to estimate and predict electronic-transport-related information in numerous TE materials, which include features of the EBS (e.g., band convergence effect,<sup>25–29</sup> changes in inter-band separation with temperature,<sup>30</sup> band-gap estimation<sup>31</sup>), scattering mechanism,<sup>32–34</sup> charge-carrier optimization and performance prediction,<sup>35–39</sup> and materials design.<sup>40</sup> However, there are drawbacks, as most of these models assume a single effective band to mimic the majority carrier transport while neglecting minority carriers. This is done to obtain a unique solution but restricts the number of parameters that can be handled. Recent studies<sup>23,41</sup> indicate that this can result in incorrect EBS parameters in semiconductors with complex band structures (presence of multiple valleys near the band extrema). For some materials, multi-band models have been developed.<sup>42–46</sup> These are, however, pointwise solutions, and the methodology for arbitrary material systems is missing. Furthermore, it has not been clarified if the employed models are indeed the best descriptions of the respective material systems.

Thus, an approach that can provide information on all EBS and scattering parameters and at the same time be obtained from routine laboratory measurements would be highly beneficial for studying TE materials. In this work, a refinement technique (referred to as the multi-band refinement technique [MBRT]) has been proposed. The MBRT method requires experimental data of electrical properties and an electronic transport model as inputs and sequentially refines the associated EBS and scattering parameters. The technique uses least-square minimization for the refinement process, which is similar to the Rietveld method.<sup>47,48</sup> The refinement process involves iterative adjustments in the parameters and is continued until an acceptable match is obtained between the experimental and calculated electrical properties. The advantages of this technique are that (1) the MBRT can refine multiple parameters, which is unlike existing solution-based methods. It can thus account for materials with complex band structures with multiple bands close to the band extrema. The effects of temperature, doping concentration, and alloying on the EBS can also be studied using this technique, and subtle changes can be detected. To account for these features, the temperature dependence of parameters like band gap and inter-band separation has been considered. (2) Apart from EBS information, this technique allows for extracting charge scattering information. Acoustic phonon



**Figure 1. Block diagram representation of the multi-band refinement technique (MBRT)**

The schematic represents an overview of MBRT. The set of input, i.e., experimental thermoelectric properties, electronic transport model, and initial values for variables, are mentioned in the input block, followed by the solver block presenting sequential refinement of individual variables. The output block represents the results of the MBRT, which are the refined electronic transport parameters.

scattering is considered to be the dominant scattering mechanism in TE materials at high temperatures.<sup>24</sup> Accordingly, the deformation potential values for individual bands can be calculated using the MBRT. Currently, grain-boundary scattering, which is relevant in many TE materials,<sup>34,49</sup> can also be studied. (3) The MBRT is computationally inexpensive and can be easily adopted.

The MBRT method has been tested on (1) n-type silicon, a well-known semiconductor for which EBS information is available,<sup>12</sup> and (2) n-type Mg<sub>2</sub>Si, which is a state-of-the-art TE material.<sup>50</sup> The results from the MBRT for both Si and Mg<sub>2</sub>Si show an excellent match of the refined parameters with literature reports, highlighting its applicability for studying TE semiconductors.

## RESULTS AND DISCUSSION

### Methodology

The block diagram representation of the MBRT is shown in Figure 1. Input to the model consists of (1) temperature-dependent experimental data of  $S$  ( $S(T)$ ),  $\sigma$  ( $\sigma(T)$ ), and Hall coefficient ( $R_H(T)$ ), (2) an electronic transport model, and (3) initial values for all the variables ( $P_V^0$ ). The experimental data can be obtained from standard measurements.<sup>51–59</sup> It is necessary to have the experimental data of  $S(T_i)$ ,  $\sigma(T_i)$ , and  $R_H(T_i)$  at fixed temperature points ( $i =$  first temperature data point; last temperature data point at regular intervals). Polynomial fitting (usually of the 2<sup>nd</sup> or 3<sup>rd</sup> order) of the raw data has been done to obtain this. A uniform temperature interval of  $\Delta T = 10$  K has been used in this study. The electronic transport model consists of EBS and charge-carrier scattering information specific to the given material system. The EBS model contains details regarding those energy bands that contribute to charge transport. This can be obtained from literature reports or calculated by *ab initio* methods for any TE material. In the case of solid solutions, the EBS model can be inferred from the end members, assuming linear variations in the band positions and band curvatures.<sup>26,60</sup>

It is then important to identify the bands relevant to charge transport. This depends on the position of the Fermi level, e.g., in heavily doped TE materials, the minority bands can be neglected.<sup>24</sup> Similarly, at low doping or high temperatures, mixed conduction is usually relevant, hence both majority and minority bands need to be included.<sup>42–44,46,61,62</sup> The position of these bands in k-space can be used to obtain their valley degeneracy number ( $N_V$ ). Once the EBS model is finalized, the list of variables needs to be decided. The band effective mass ( $m_b^*$ ) for each band, the band gap ( $E_g$ ), and the inter-band energy separations ( $E_i$ ) are variables to be optimized. Since the band gap and inter-band separations are known to have a temperature dependence, a linear variation has been considered in this study that results in one additional variable per considered band.<sup>11</sup> The temperature-dependent changes in the inter-band separations and band gap are important to study in TE materials, as they provide vital information regarding band convergence, mixed conduction, and bipolar thermal effects. The  $m_b^*$  and deformation potentials ( $\Xi$ ) can also have a temperature dependence, but the change is usually negligible compared to the temperature dependence of energy-gap parameters.<sup>63</sup> Considering the coupling between  $m_b^*$ ,  $\Xi$ ,  $E_g$ , and  $E_i$  parameters, the temperature dependence of  $m_b^*$  and  $\Xi$  has been neglected in this study. The other information required in the electronic transport model is the charge-carrier scattering mechanism.<sup>22,64,65</sup> For heavily doped TE materials and at high temperatures, acoustic phonon (AP) scattering is the dominant mechanism and has been considered in the study.<sup>24</sup> Thus, deformation potentials of the individual bands are additional variables to be refined. Other scattering mechanisms might also need to be incorporated depending on the material system and studied temperature range (e.g., in  $Mg_2Si$ , grain boundary scattering has been considered<sup>34</sup> in this study). In the case of multiple scattering mechanisms, the overall mobility parameter ( $\mu_0$ ) can be defined using Matthiessen's rule<sup>66</sup>: ( $\mu_0 = \left(\sum \frac{1}{\mu_{0,i}}\right)^{-1}$ ). Here,  $\mu_{0,i}$  represents the mobility expression for individual scattering mechanisms.

For each variable ( $P_V, V = 1 : s$ ), here,  $V$  represents an individual variable and  $s$  defines the total number of refinement variables. Initial guess values ( $P_V^0$ ) are required and serve as the starting point for the optimization routine. Since the MBRT utilizes a least-square minimization technique, refinement of the initial guess values always leads to the closest minimum. Thus, the guess values need to be close to the global minimum. This information can be obtained for any TE material using a combination of n- and p-type heavily doped compositions. Since the minority band contributions can be neglected in heavily doped compositions and at low temperatures, information about the conduction/valence band edge can be extracted from these compositions utilizing single-band (SPB or SKB)-based models. Further, the variation of SPB/SKB density of states (DOS) mass with carrier concentration can be used as an indicator of the presence of additional bands close to the edge, and this information can be exploited while deciding the electron transport model. Another approach to obtain initial value information of materials would be from DFT calculations on defect-free materials, which are computationally inexpensive. This can be used to obtain ground-state information of relevant bands and can act as the guess values. Literature reports of EBS parameters can be further used to supplement the data. Discussion on the guess values for the studied materials is provided in the [results and discussion](#) section and in the [supplemental information](#) (see [Notes S3](#) and [S4](#)). This input information is fed to the MATLAB-based MBRT solver. Refinement of the variables is then performed iteratively by minimizing the difference between the experimental and calculated transport properties. A least-square minimization function<sup>67</sup> ( $R$ ) has been defined for this purpose and is given in [Table 1](#). In this expression, the subscripts *exp* and *calc* refer to the experimental and theoretical values, respectively.  $N$  refers to the total number of temperature points, and  $i$  represents

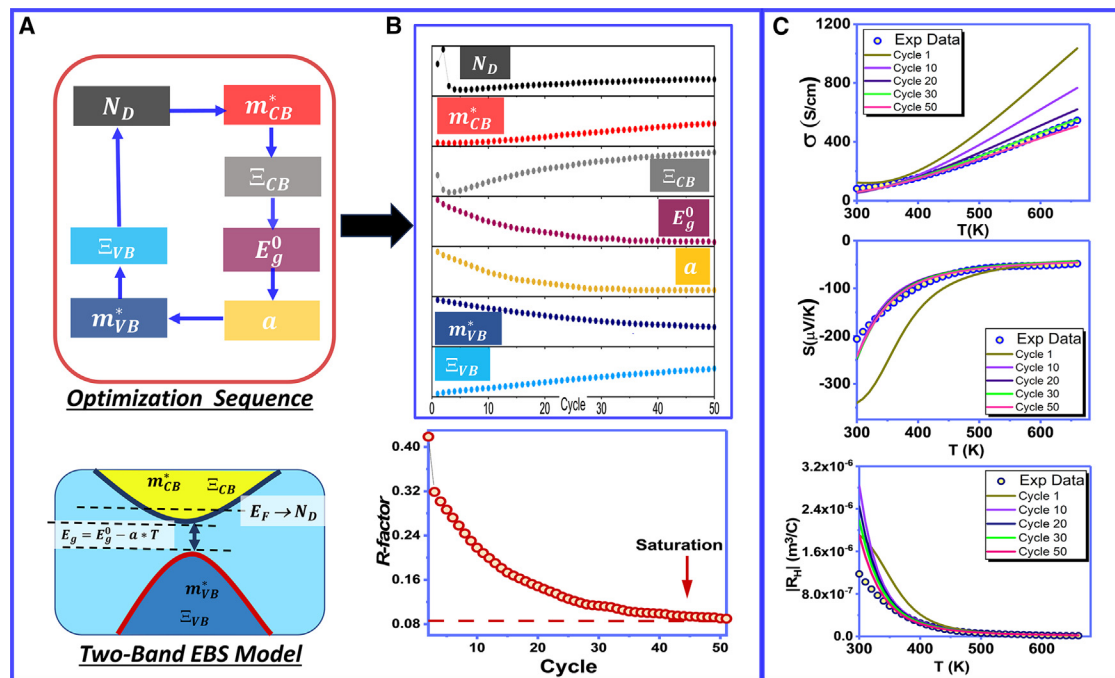
**Table 1. List of equations used in the MBRT code**

	Expression
Individual band ( $i^{\text{th}}$ )	
Charge-carrier concentration ( $n_i$ )	$n_i = \frac{(2m_D^* k_B T)^2}{2\pi^2 \hbar^3} F_1(\eta) \frac{3}{2}$
DOS effective mass ( $m_D^*$ )	$m_D^* = N_V^{2/3} m_b$
Electrical conductivity ( $\sigma_i$ )	$\sigma_i = \frac{8\pi e}{3\hbar^2} \mu_0 (2m_D^* k_B T)^2 F_0(\eta) \frac{3}{2}$
Seebeck coefficient ( $S_i$ )	$S_i = \left( -\frac{k_B}{e} \right) \left( \frac{2F_1(\eta)}{F_0(\eta)} - \eta \right)$
Hall coefficient ( $R_{H,i}$ )	$R_{H,i} = \frac{3}{4} \frac{F_{0.5}(\eta) F_{-0.5}(\eta)}{F_0(\eta) F_0(\eta)} \frac{1}{n_i e}$
Multi-band	
Charge balance equation	$\sum_{i=1}^M n_i + N_A = \sum_{i=1}^Q p_i + N_D$
Electrical conductivity ( $\sigma$ )	$\sigma_{\text{calc}} = \sum_i^{M+Q} \sigma_i$
Seebeck coefficient ( $S$ )	$S_{\text{calc}} = \frac{\sum_i^{M+Q} \sigma_i S_i}{\sum_i^{M+Q} \sigma_i}$
Hall coefficient ( $R_H$ )	$R_{H\text{calc}} = \frac{\sum_i^{M+Q} R_{H,i} \sigma_i^2}{\left( \sum_i^{M+Q} \sigma_i \right)^2}$
Charge-carrier scattering mechanism	
Acoustic phonon (AP)	$\mu_{0,AP} = \frac{e\pi\hbar^4 d v_l^2}{\sqrt{2} \Xi_n^2 m_b^{5/2} (k_B T)^{3/2}}$
Grain boundary (GB)	$\mu_{0,GB} = L e \left( \frac{1}{2\pi m_b^* k T} \right)^{1/2} e^{-\frac{E_b}{kT}}$
Minimization function (R factor)	$R = \frac{1}{N} \sum_{i=1}^N \left( 1 - \frac{\sigma_{\text{exp},i}}{\sigma_{\text{calc},i}} \right)^2 + \left( 1 - \frac{S_{\text{exp},i}}{S_{\text{calc},i}} \right)^2 + \left( 1 - \frac{R_{H\text{exp},i}}{R_{H\text{calc},i}} \right)^2$
Quality of refinement	$\chi = \frac{R}{R_{\text{exp}}}$

List of equations used in the MBRT code. <sup>6,22,24,34,43,67</sup>  $i$ , band number;  $m_D^*$ , DOS effective mass;  $m_b^*$ , band effective mass;  $N_V$ , valley degeneracy;  $T$ , temperature;  $\eta$ , Fermi level;  $F_j(\eta)$ , Fermi integral;  $\mu_0$ , free mobility;  $n/p$ , electron/hole concentration;  $M$ , number of conduction bands;  $Q$ , number of valence bands;  $N_A$ , acceptor concentration;  $N_D$ , donor concentration; \*\_calc, calculated data; \*\_exp, measured data;  $v_l$ , longitudinal velocity of sound;  $\Xi_n$ , deformation potential;  $d$ , density;  $E_b$ , grain boundary activation energy;  $L$ , average grain size;  $N$ , number of temperature points;  $\chi$ , goodness of fit factor.

individual temperature points. At each temperature point, the theoretical values for the electrical properties ( $S$ ,  $\sigma$ ,  $R_H$ ) are calculated. Multi-band charge-transport equations (given in Table 1) have been formulated based on the electronic transport model to obtain the theoretical values. In these equations, the individual band contributions are estimated from the Boltzmann transport equation.<sup>68</sup> Also, bands have been considered as parabolic and rigid with respect to temperature. AP scattering has been assumed to be the dominant charge-carrier scattering mechanism. The  $R$  factor is calculated for a set of variables using the experimental and calculated values of  $S$ ,  $\sigma$ , and  $R_H$  at each temperature point. All the variables are sequentially optimized within each refinement cycle with guess values as starting point. In general, the number of refinement cycles ( $C$ ) depends on the initial parameters and electronic transport model. In this study, a convergence limit (relative change between two consecutive  $R$  factor values) of  $10^{-2}$  has been used.

An example of the MBRT is shown in Figure 2. A two-band (one conduction band [CB] and one valence band [VB]) EBS model and AP scattering have been taken as input. This gives a total of seven variables ( $V = 1 : 7$ ) as shown in Figure 2A. Defining the sequence in which the different variables need to be optimized is the first step of the refinement process. This is decided based on the impact of each variable



**Figure 2.** Illustration of processes involved during multi-band refinement

(A) The optimization sequence of the variables along with a schematic representation of a two-band EBS model (here,  $N_D$  is donor concentration;  $m_{CB}^*$  and  $m_{VB}^*$  represent the DOS effective mass of the conduction and valence bands, respectively;  $\Xi_{CB}$  and  $\Xi_{VB}$  are the corresponding deformation potentials;  $E_g$  is the band gap;  $E_g^0$  is the band gap at 0 K;  $a$  is the temperature dependence of the band gap; and  $E_F$  is the Fermi level). (B) Top: incremental changes in the variables with the number of refinement cycles. Bottom: the corresponding  $R$  factor as a function of number of refinement cycles.

(C) Progression in the fitting quality for  $\sigma$ ,  $S$ , and  $R_H$ , respectively, with the number of refinement cycles.

on the electrical properties. In general, the donor or acceptor concentration is always the first variable to be refined, as it regulates the position of the Fermi level. This is followed by the majority band variables, i.e., related to the CB if n-type and to the VB if p-type. Variables associated with band gap are refined after the majority band variables. Finally, the minority band variables are refined. The reason for prioritizing band-gap variables over the minority band variables is their higher influence on the TE properties. Further details regarding sequence of optimization have been discussed in the [supplemental information \(Notes S3 and S4; Figure S3\)](#). The example in [Figure 2](#) is that of an n-type TE material; thus, the highest priority variables are  $N_D$  (donor concentration) and CB variables ( $m_{CB}^*$  and  $\Xi_{CB}$ ). This is followed by the band-gap variables ( $E_g^0$  and  $a$ ) and finally the VB variables ( $m_{VB}^*$  and  $\Xi_{VB}$ ).

In [Figure 2B](#), the changes in each variable as a function of the refinement cycle ( $C$ ) is depicted. The bottom image in [Figure 2B](#) depicts the  $R$  factor, which saturates after  $\sim 50$  cycles. Thus, the refinement process can be described as an incremental adjustment of the variables in each iteration step in order to lower the  $R$  factor values. In [Figure 2C](#), the progression in the fit of all the calculated electrical properties with the number of refinement cycles is shown. The difference between experiment (hollow circle) and calculated data decreases with an increase in number of refinement cycles.

Since the MBRT method has similarities to the Rietveld refinement technique,<sup>47,48,69</sup> which is an established technique, a direct comparison between the two helps in

**Table 2. Comparison of the MBRT and the Rietveld refinement method**

	MBRT method	Rietveld method <sup>47</sup>
Experimental input	electrical properties ( $S(T), \sigma(T), R_H(T)$ )	diffraction data (intensity vs. $2\theta$ )
Structural model	electronic band structure (EBS) and charge-carrier scattering information	crystal structure information
Minimization function	$R = \frac{1}{\theta_N} \sum_{i=1}^{\theta_N} \left( 1 - \frac{\sigma_{exp,i}}{\sigma_{calc,i}} \right)^2 + \left( 1 - \frac{S_{exp,i}}{S_{calc,i}} \right)^2 + \left( 1 - \frac{R_{Hexp,i}}{R_{Hcalc,i}} \right)^2$	$\sum_i w_i (y_i^{obs} - y_i^{calc})^2$
Constitutive equations	BTE-based multi-band equations (given in Table 1)	$y_{ic} = y_{ib} + \sum_{\varphi} S_{\varphi} \sum_k G_{\varphi} (2\theta_i - 2\theta_k) l_k$ $l_k = m_k L_k  F_k ^2 P_k A_k$
Refined variables	band-structure parameters: band effective mass, band gap, inter-band separation, scattering terms (deformation potential, alloy scattering potential, grain boundary energy, etc.)	crystal structure parameters: lattice constant, atomic position, occupancy, thermal displacement parameter, etc.
Quality of refinement	$R$ factor and goodness-of-fit factor ( $\chi$ )	$R_{wp} = \left[ \frac{\sum_i w_i (y_i^{obs} - y_i^{calc})^2}{\sum_i w_i (y_i^{obs})^2} \right]^{1/2}$ $\chi^2 = \frac{R_{wp}}{R_{exp}}$

understanding its capabilities and limitations. In Table 2, the analogies between the two methods have been presented. As seen from the table, both methods rely on experimental data and a structural model as inputs. Also, the minimization functions are based on the least-square error (LSE) method. The critical requirement during Rietveld refinement is to prevent the minimization function from settling at a local minimum. This is done by a sequential refinement of various crystal structure parameters. Similarly, avoiding false minima during MBRT refinement is crucial to identify the correct EBS variables. A sequential refinement of the EBS variables based on their impact on the transport data has been adopted to overcome this problem. Finally, the quality of refinement in the Rietveld method is quantified using cost functions ( $R_{wp}$  factor and  $\chi^2$  are listed in Table 2). In the MBRT method, the quality of refinement is defined by the  $R$  factor, which is mathematically similar to the  $R_{wp}$  factor. In addition, the goodness of fit (GoF) parameter  $\chi = \frac{R}{R_{exp}}$  has been defined, where  $R_{exp}$  is a measure of the ideal  $R$  factor and is defined by

$$R_{exp} = (\delta\sigma)^2 + (u\sigma)^2 + (\delta S)^2 + (uS)^2 + (\delta R_H)^2 + (uR_H)^2 \quad . \text{(Equation 2)}$$

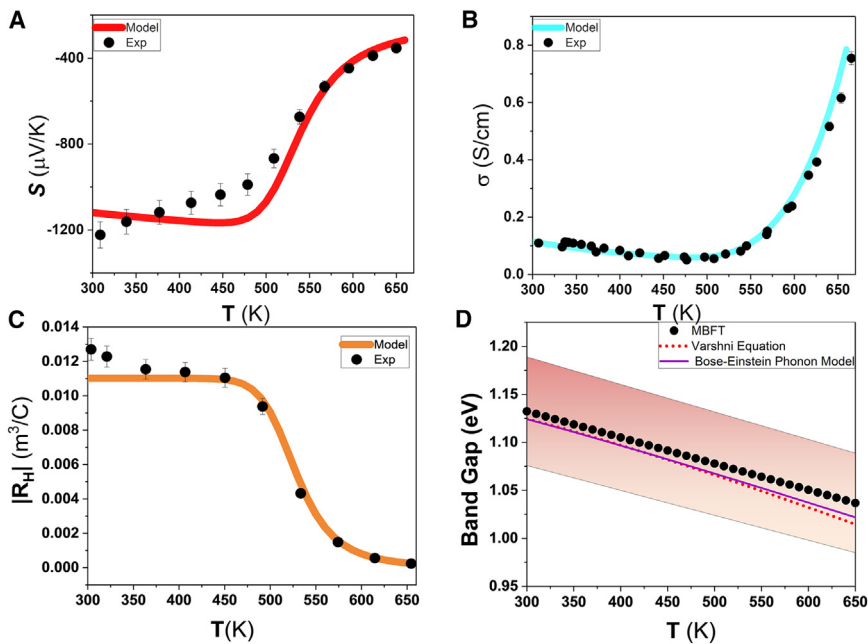
In this equation, the prefixes “ $\delta$ ” and “ $u$ ” refer to the relative precision and accuracy of the measurement instruments, respectively. An  $R_{exp}$  value of 0.0271 is obtained based on the uncertainties in the measurements used in this study. The GoF parameter ( $\chi$ ) defines the quality of refinement.  $\chi$  values much larger than unity indicate false minima or an incorrect EBS model or scattering mechanism. Details about the quality of refinement are provided in Note S2 and Table S1.

The applicability of the MBRT method was tested on elemental silicon and n-type  $Mg_2Si$  compositions. Silicon was chosen due to the availability of a vast amount of literature on its EBS.<sup>12,45,64,70–74</sup> This provides the ideal platform for validation of the obtained refined variables. n-Type  $Mg_2Si$  compositions, a low-cost TE material, have been studied by the MBRT due to their potential application in TE devices.<sup>36,50,75,76</sup> Details of the obtained results are provided in this section.

### Silicon wafer

A commercial phosphorus-doped silicon wafer (Wafer World, grade: prime, dopant: phosphorus) was used for this study. The data obtained from polynomial fitting of





**Figure 3. Multi-band refinement results for n-type low-doped silicon wafer**

(A–C) Comparison of the experimental (Exp) and calculated data (Model) of  $R_H$ ,  $\sigma$ , and  $S$  as a function of temperature, with error bars representing 5%, 3%, and 5% measurement uncertainties, respectively.

(D) The estimated band-gap values are compared with literature models. The shaded region indicates a  $\pm 5\%$  error bar of the measurement uncertainty.

the experimental measurements  $S(T)$ ,  $\sigma(T)$ , and  $R_H(T)$  have been used as inputs to the solver (see Figure S2). A two-band model consisting of a single CB and a single VB was used as the input EBS model for the solver. The initial values for the variables were taken from literature and are provided in Table S2. In Figures 3A–3C, the calculated  $R_H$ ,  $\sigma$ , and  $S$  data, along with the experimental data, are plotted (details of the EBS models, guess values, and optimization process are provided in Note S3; Figure S4 explains the cause of mismatch in  $R_H$  and  $S$  data near room temperature). An  $R$  factor value of 0.0226 was obtained after saturation. The refined EBS variables are given in Table 3 along with literature reports.

The obtained DOS effective masses ( $m_{CB}^*$ ,  $m_{VB}^*$ ) are within  $\sim 10\%$  of that obtained from cyclotron measurements. Similarly, the deformation potential values ( $\Xi_{CB}$ ,  $\Xi_{VB}$ ) have a similar deviation ( $\sim 10\%$ ) compared to DFPT<sup>79</sup> calculations. It is to be noted that for materials with anisotropic band masses, the effective anisotropy parameter ( $K^*$ )<sup>80</sup> needs to be considered while utilizing the mobility expressions, as the inertial effective mass ( $m_l$ ) can no longer be considered the same as the band mass ( $m_b^*$ ). The  $K^*$  value can be obtained from the anisotropy parameter ( $m_{\parallel}^*/m_{\perp}^*$ ) as suggested by Gibbs et al.<sup>80</sup> The other refined variables ( $E_g^0$ ,  $a$ ) related to the band gap are also close to reported experimental data. In Figure 3D, the temperature variation of the estimated band gap in silicon is plotted along with literature reports (obtained from Varshni's formula and the Bose-Einstein phonon model, including optical phonons). The shaded region indicates a range of  $\pm 5\%$ .

Overall, all the refined variables converge to values close to literature reports, indicating the efficacy of the MBRT method. The deviations in the refined values lie between 3% and 12% and reflect the cumulative effect of various error sources. These include errors due to deficiencies in the starting EBS model, proximity of initial guess

**Table 3. Comparison of the refined EBS variables for silicon with literature reports**

EBS variable	This work (MBRT)	Literature	$\delta$ (%)
$m_{CB}^*/m_0$ (CB DOS effective mass)	1.36	1.19 (cyclotron measurement) <sup>12</sup>	12.5
		1.14 (DFT calculation with HSE06 xc) <sup>77</sup>	16.1
		1.40 (two-band model) <sup>45</sup>	2.9
$\Xi_{CB}$ (eV) (deformation potential CB)	9.32	9.0 (ToF data with Monte Carlo) <sup>78</sup>	3.4
		8.21 (DFPT calculation with PBE xc) <sup>79</sup>	11.9
$m_{VB}^*/m_0$ (VB DOS effective mass)	0.74	0.81 (cyclotron measurement) <sup>12</sup>	9.4
$\Xi_{VB}$ (eV) (deformation potential VB)	5.80	5.48 (DFPT calculation with PBE xc) <sup>79</sup>	5.5
$E_g^0$ (eV) (band gap at 0 K)	1.21	1.17 (experiment) <sup>12</sup>	3.3
		1.08 (DFT calculation with HSE06 xc) <sup>77</sup>	10.7
		1.13 (two-band model) <sup>45</sup>	6.6
$a$ (eV/K) (temperature dependence of band gap)	0.000273	0.000316 (Varshni model) <sup>12</sup>	15.7
		0.000293 (Bose-Einstein phonon model) <sup>9</sup> <sup>74</sup>	7.3

$\delta$  indicates the percentage of deviation of the data from literature.

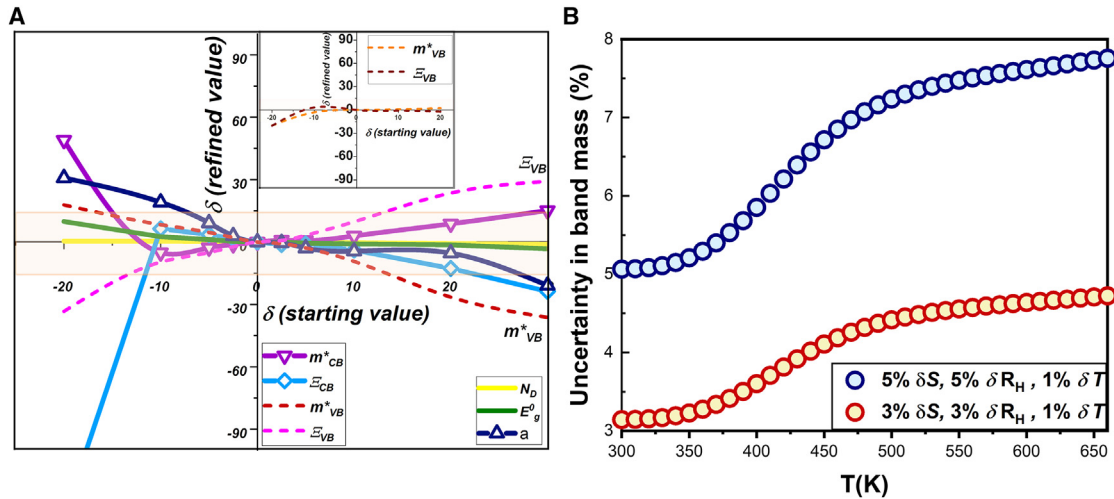
<sup>a</sup>Calculated assuming a linear temperature dependence.

values, and errors in the measured experimental data.<sup>51–59</sup> In Figure 4A, the influence of the proximity of the guess value (referred to as  $\delta$  [starting value]) on the refined values is shown for the different variables ( $\delta$  [refined value]). The variables shown in Figure 4A have been categorized depending on the extent of deviation in the refined value.  $N_D$  and  $E_g^0$ , which have the least errors, are marked by solid lines, and these variables converge to the final values even when the guess values deviate significantly (up to  $\pm 30\%$ ). At the other extreme are the minority band variables ( $m_{VB}^*$ ,  $\Xi_{VB}$ ) (shown by dashed lines), which can have significant errors in the final values depending on the starting position. The errors in the majority band variables ( $m_{CB}^*$ ,  $\Xi_{CB}$ ) (shown by solid lines with symbols) lie in between. It is to be noted that these calculations were performed considering uniform deviation of the guess values for all the variables. The errors can be reduced significantly for non-uniform deviations (only  $m_{VB}^*$  and  $\Xi_{VB}$  were deviated), as shown in the inset of Figure 4A. Thus, it can be inferred that (1) starting with initial values that are close to the final ones is important to avoid false minima, (2) variables for minority carriers are more sensitive, which reflects their lower contribution in the experimental data, and (3) a sequential approach to the refinement is the best option to reach the global minimum.

The other source of error in the data originates from inaccuracies in the measured data. The associated uncertainties are difficult to extract in a multi-band scenario due to the unavailability of analytical expressions. However, rough estimates can be obtained from reported single-band expressions. In Figure 4B, the fractional uncertainty in  $m_D^*$  has been estimated using Snyder's expression<sup>81</sup>:

$$m_s^* = \frac{h^2}{2k_B T} \left( \frac{3n_H}{16\sqrt{\pi}} \right)^{2/3} \left[ \frac{\left( \exp \left[ \frac{|S|}{k_B/e} - 2 \right] - 0.17 \right)^{2/3}}{1 + \exp \left[ -5 \left( \frac{|S|}{k_B/e} - \frac{k_B/e}{|S|} \right) \right]} + \frac{\frac{3}{\pi^2} \left( \frac{2}{\sqrt{\pi}} \right)^{2/3} \frac{|S|}{k_B/e}}{1 + \exp \left[ 5 \left( \frac{|S|}{k_B/e} - \frac{k_B/e}{|S|} \right) \right]} \right] \quad (\text{Equation 3})$$

Here,  $m_s^*$  is defined as the Seebeck effective mass with  $m_s^* = m_D^*$  for AP scattering and  $n_H$  represents the Hall carrier concentration.<sup>24</sup> The data indicate variations between 3% and 8% due to instrumental errors. Similarly an estimate of the uncertainty in the band-gap value can be obtained from the Goldsmid expression<sup>82</sup> ( $E_g = 2S_{max} T_{max}$ ),



**Figure 4. Uncertainty analysis of MBRT**

(A) The effect of deviation of the guess values on the error in the final data (inset shows the errors in  $m_{VB}^*$  and  $\Xi_{VB}$  when the other variables have no errors). The shaded region indicates an error of  $\pm 15\%$ .

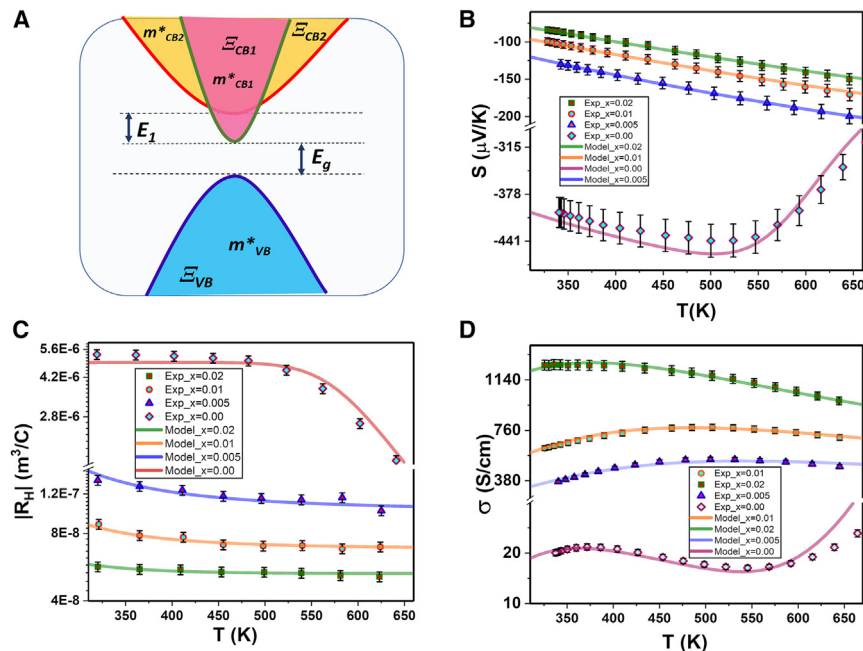
(B) The fractional uncertainty in the density of states mass ( $\delta m_D^*/m_D^*$ ) as a function of temperature for two different combinations of errors in  $S, R_H$ , and  $T$ .

which yields deviations between 4% and 6% ( $\delta S = 3\%, 5\%, \delta T = 1\%$ ). Comparing these values with the deviations obtained in Table 3, it can be inferred that instrumental uncertainties are the major contributors to the obtained  $\delta$  values.

### Mg<sub>2</sub>Si compounds

Polycrystalline compositions of n-type Mg<sub>2.2</sub>Si<sub>1-x</sub>Bi<sub>x</sub> ( $x = 0.0, 0.005, 0.01, 0.02$ ) were prepared for this study and experimental data of  $S(T)$ ,  $\sigma(T)$  and  $R_H(T)$  were collected between 300 K and 660 K (data provided in Figure 5). Polynomial fitting of the TE data is shown in Figure S5. Reported ground-state EBS calculations indicate that the CB edge consists of two bands (denoted here as CB1 and CB2).<sup>50</sup> Both these bands are centered around the X k-point and are separated by an energy difference of  $\sim 0.2$ – $0.4$  eV. The VB edge in Mg<sub>2</sub>Si is similar to that of silicon and consists of three bands (heavy hole, light hole, and the split-off band). Since all the studied compositions were n-type, these bands were approximated by a single effective band (denoted by VB). The input EBS model therefore consisted of two bands (CB1 and VB) for the undoped composition ( $x = 0$ ) and three bands (CB1, CB2, and VB) for all the doped compositions. The rationale behind considering only two bands for the undoped composition is the large inter-band separation ( $E_1$ ) between CB1 and CB2. The measured  $\sigma$  data (shown in Figure 5 (d)) indicates a non-monotonous temperature variation. This has been attributed to resistive grain boundaries (GBs), which hinder charge flow at lower temperatures. To account for this an additional contribution ( $\mu_{0,GB}$ ) to the overall mobility ( $\mu_0$ ) has been considered. The analytical expression provided by Seto<sup>83</sup> ( $\mu_{0,GB} = Le \left( \frac{1}{2\pi m_e^* kT} \right)^{\frac{1}{2}} e^{-\left( \frac{E_b}{kT} \right)}$ ) is used to model the GB contribution. Here,  $E_b$  represents the GB activation energy, while  $L$  represents the average grain size. The AP scattering and the GB scattering were assumed to be independent processes, and thus the total contribution can be obtained from Matthiessen's rule<sup>66</sup>

( $\mu_0 = \left( \frac{1}{\mu_{0,AP}} + \frac{1}{\mu_{0,GB}} \right)^{-1}$ ). In total, there are nine variables that have been refined for both the two-band and the three-band model (Tables S4 and S5). The initial values for all the variables were taken from literature reports. Details regarding the electron transport model and guess values are provided in Note S4.



**Figure 5. Multi-band refinement of n-type  $\text{Mg}_2\text{Si}$ .**

(A) EBS schematic for n-type  $\text{Mg}_2\text{Si}$ .

(B–D) Temperature dependence of  $S$ ,  $R_H$ , and  $\sigma$  for all the compositions of  $\text{Mg}_{2.2}\text{Si}_{1-x}\text{Bi}_x$  with  $x = 0.00, 0.005, 0.01, 0.02$ . Solid lines represent the modeled data, while symbols indicate experimental measurements. Error bars represent 5%, 5%, and 3% measurement uncertainties in  $S$ ,  $R_H$ , and  $\sigma$ , respectively.

Initially, the undoped composition is refined. This is followed by the (individual) refinement of the doped compositions, in which the VB and band-gap ( $m_{VB}^*$ ,  $\Xi_{VB}$ ,  $E_{g,0}^0$ ,  $a$ ) parameters are taken from the refined undoped data (details about the optimization sequence and refinement process are in [Note S4](#)). In [Table 4](#), the refined data for all the variables along with literature reports are given. The modeled  $S$ ,  $\sigma$ , and  $R_H$  data for all the compositions are provided in [Figure 5](#). As seen from the figure, the modeled data are in close agreement with the experimental data. This is also indicated from the obtained  $R$  factor (0.00078–0.012) and GoF ( $\chi$ ) values (0.029–0.044) (see [Table S6](#)).

The refined variables match well with literature reports (given in [Table 4](#)). Of specific note are the  $m_{VB}^*$  and  $E_{g,0}^0$  values, for which a huge discrepancy is reported between experimental and DFT data.<sup>89,90</sup> Our results suggest values that are closer to DFT reports. Further, the band-gap value ( $E_{g,0}^0$ ) agrees with experimental reports. A comparison of the lower CB (CB1) properties as a function of doping content (for which extensive literature reports exist<sup>50</sup>) has been carried out. Data provided in [Table S5](#) and [Figure S6](#) indicate no systematic variation of  $m_{CB1}^*$  with Bi doping content (mean value:  $0.80 m_0$ , standard deviation:  $0.05 m_0$ ). This is in accordance with literature reports, where variations between  $0.6$  and  $1.4 m_0$  has been reported. Thus, both literature reports and the MBRT results indicate a rigid lower CB with Bi doping. The MBRT data of the deformation potential have a mean value of  $18.4$  eV and a standard deviation of  $0.8$  eV; however, no systematic variation of  $\Xi_{CB1}$  with  $N_D$  is observed. While no such studies are reported in literature, the small scatter in the data ( $\sim 4.5\%$ ) and no systematic variation can be taken to be a signature of a rigid CB (CB1) with Bi doping in the  $\text{Mg}_2\text{Si}$  system.

**Table 4. Band structure parameters of Mg<sub>2</sub>Si, obtained from the MBRT along with reported theoretical and experimental data**

EBS Variable/variable	This Work work (MBRT)	Literature
$m_{CB1}^*/(m_0)$ (CB1 DOS effective mass)	0.76–0.79	0.73 (DFT) <sup>84</sup> 0.6–1.433 (SPB data) <sup>50</sup>
$\Xi_{CB1}$ (eV) (deformation potential CB1)	17.2–18.8	15–17 (SPB data) <sup>42,85</sup>
$m_{CB2}^*/(m_0)$ (CB2 DOS effective mass)	1.06–1.31	1.41 (k.p. method) <sup>86</sup> 0.62 (LDA data) <sup>87</sup>
$\Xi_{CB2}$ (eV) (deformation potential CB2)	9.09–10.63	9.51 (multi-band fitting) <sup>87</sup>
$m_{VB}^*/(m_0)$ (VB DOS effective mass)	1.79	1.83 (DFT) <sup>88</sup> 4 (SPB) <sup>89</sup>
$\Xi_{VB}$ (eV) (deformation potential VB)	10.39	9 (SPB data) <sup>39</sup>
$E_g^0$ (eV) (band gap at 0K)	0.84	0.7–0.8 (IR data) <sup>90</sup> 0.78 (Hall and conductivity data) <sup>91</sup>
$a$ (eV/K) (temperature dependence of band gap)	–0.000615	–0.0005 (IR data) <sup>90</sup>
$E_1^0$ (eV) (inter-band separation at 0 K)	0.14–0.15	0.21–0.26 (DFT) <sup>86</sup> 0.4 (IR data) <sup>90</sup>
$d_1$ (eV/K) (temperature dependence of inter-band separation)	$1.0\text{--}1.6 \times 10^{-4}$	$0.89 \times 10^{-5}$ (fitting of two-CB Kane model) <sup>87</sup>
$E_b$ (eV) (GB activation energy)	0.05–0.13	0.095 (SPB data) <sup>34</sup>
$L$ (m) (average grain size)	$0.5 \times 10^{-7}\text{--}1.7 \times 10^{-6}$	N/A

Overall, the MBRT method is shown to provide accurate EBS variables for the studied Mg<sub>2</sub>Si compositions (see Table S5). A point to note is that individual Mg<sub>2</sub>Si compositions were refined independently and still provide similar optimized values for different variables. This can be interpreted as a validation of the ability of MBRT to provide accurate band-structure-related information.

The MBRT is thus a powerful method for temperature- and doping-dependent EBS studies, with the only requirements being accurate electronic transport model, experimental data, and initial values for each refined variable. The use of this technique is manifold: first, it allows the extraction of microscopic material parameters, which are more fundamental than individual transport properties. EBS information are building blocks to improve the performance of all semiconductor devices in general. The MBRT can thus be an efficient technique to obtain, e.g., band-gap behavior, which is a key factor in determining the performance of devices like TE generators, solar cells, lasers, and opto-electronics. Second, the impact of various strategies like alloying, doping, and process engineering on TE performance can also be understood and used to tune the EBS in a more profound manner using this technique. Third, this technique can be used as a predictive tool<sup>39,92,93</sup> for materials discovery. Material parameters ( $B, B^*$ ), which are defined using intrinsic material properties, have been successfully used in the past for prediction of optimal doping concentrations. The output from the MBRT can be used directly in these parameters as discussed in the supplemental information (see Note S5). An alternate approach for using the MBRT as a search tool has been suggested by Kamila et al.<sup>39</sup> The multi-band information from the MBRT can be utilized in place of SPB data to generate carrier-concentration- and composition-dependent 3D performance maps. Fourth, temperature-dependent EBS information can be used to model behavior of TE generators that operate under large temperature gradients and can help enhance the conversion efficiency. Our results also highlight the important role played by the initial guess values in reaching the global minimum. Thus, methods for identifying these guess values require investigation and would be beneficial to make the MBRT an even more robust tool for TE research.

The refined EBS results obtained for  $Mg_2Si$  and silicon show the utility of the MBRT. Consistency of EBS parameters with the existing literature proves the validity of the MBRT. In addition, the efficiency of this technique in terms of execution time (can be performed on a standard desktop PC; 1.6 GHz 4 Core CPU, 8 GB RAM) makes it a readily accessible tool that would enable users to study the vast number of TE compounds. Thus, the manifold benefits of the MBRT make it a prominent technique for probing the EBS and for accelerating the discovery of high-performance TE materials.

## EXPERIMENTAL PROCEDURES

### Resource availability

#### Lead contact

Further information and requests for resources should be directed to and will be fulfilled by the lead contact, Dr. Titas Dasgupta ([titas.dasgupta@iitb.ac.in](mailto:titas.dasgupta@iitb.ac.in)).

#### Materials availability

This study did not generate new unique reagents.

#### Data and code availability

All original code has been deposited at Zenodo under <https://doi.org/10.5281/zenodo.10286334> and is publicly available as of the date of publication. Sample datasets and readme files have been deposited at Release v.1.0 TitasDasgupta/MBRT-Codes ([github.com](https://github.com)) under <https://doi.org/10.5281/zenodo.10286334> and are publicly available as of the date of publication. Any additional information required to reanalyze the data reported in this paper is available from the [lead contact](#) upon request.

### Sample preparation

#### Silicon

The MBRT study on silicon was performed using a commercial n-type Si wafer (Wafer World, grade: prime, dopant: phosphorus, resistivity: 1–20  $\Omega$ cm). A rectangular sample of the dimension 10 × 10 mm was precision cut with a diamond scribe and used for the electrical measurements.

#### $Mg_2Si$

Bi-doped  $Mg_2Si$  (n-type) was prepared by a two-step process of induction melting followed by hot pressing. Nominal compositions of  $Mg_{2.2}Si_{1-x}Bi_x$  ( $x = 0.00, 0.005, 0.01, 0.02$ ) were prepared for this study. Mg coarse powder (99.9%; SRL), Si lump (99.9999%, Alfa Aesar), and Bi pieces (99.9% Loba Chemie) were used as precursors. 10% excess Mg was taken to compensate for the Mg loss. Mg coarse powder was cold compacted before induction melting. All the precursors (Mg green pellet, Si lumps, and Bi pieces) were taken as per stoichiometry in a boron nitride (BN)-coated graphite crucible. The mixture was then melted in an atmosphere-controlled induction furnace. Melting was done at 1,090°C for 5 min in Ar atmosphere (0.5 atm).<sup>94–96</sup> The obtained ingot was then hand crushed in an agate mortar and pestle for around 10 min to obtain a fine powder. The powder thus obtained was placed inside a 12.7 mm diameter graphite die and hot pressed for 5 min at 870°C in Ar atmosphere at 60 MPa uniaxial pressure in the compaction cum sintering induction furnace setup. The obtained pellets were then hand polished using different grades of emery paper and used for the measurements.

### Phase identification

The X-ray diffraction (XRD) pattern was recorded on the hot-pressed pellets using a PAN analytical setup with Cu K $\alpha$  radiation ( $\lambda = 1.54060 \text{ \AA}$ ). The indexed XRD patterns of all the compositions ( $x = 0.00, 0.005, 0.01, 0.02$ ) are provided in [Figure S1](#). Major reflections in all the compositions represent the standard Mg<sub>2</sub>Si anti-fluorite structure (space group: Fm-3m), confirmed with the ICDD 00-001-1192 database. The presence of a secondary MgO impurity phase was also detected around  $2\theta = 43^\circ$  in all the compositions, as is typically obtained during the synthesis of Mg<sub>2</sub>Si.<sup>34,94</sup>

### TE property measurements

The temperature-dependent  $R_H$ ,  $S$ , and  $\sigma$  were measured with the help of custom-built setups in the temperature range 300–670 K. The same sample was used for all the measurements to eradicate errors due to sample inhomogeneities. Also, the same sequence of measurement ( $S/\sigma$  followed by  $R_H$ ) was maintained in all samples. For the  $S/\sigma$  measurements, data were collected during both heating and cooling thermal cycles. The cooling cycle data of  $S/\sigma$  along with the heating cycle data of  $R_H$  were used for the MBRT analysis. This was done to minimize errors associated with changes in the samples during thermal cycling.

The van der Pauw geometry<sup>51,97</sup> was used for the measurement of the DC- $R_H$  of the disc-shape sample. A magnetic field was applied across the sample in the range of  $\pm 0.7$  tesla. The current, passed perpendicular to the direction of magnetic field, was in the range 0.1–0.3 A depending on the carrier concentration. A fast reversal of the current direction and averaging of the Hall voltages were carried out to overcome the errors associated with the Peltier effect. The temperature-dependent  $\sigma$  and  $S$  were measured sequentially in the same measurement cycle using an in-house-developed setup.<sup>56</sup> The van der Pauw four-probe method and the slope method<sup>98,99</sup> were used for the measurements of  $\sigma$  and  $S$ , respectively (see room temperature data in [Table S3](#)).

### Theoretical calculations

All the calculations associated with MBRT solver were performed using MATLAB software. A standard Lab desktop with 1.6 GHz, 4 Core CPU, and 8 GB RAM configuration was used. In general, it took 5–6 h for one complete run. The duration of refinement also depended on the number of parameters and the number of refinement cycles.

### SUPPLEMENTAL INFORMATION

Supplemental information can be found online at <https://doi.org/10.1016/j.xcrp.2024.101781>.

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### AUTHOR CONTRIBUTIONS

Conceptualization, B.A., J.d.B., and T.D.; methodology, B.A. and T.D.; software, B.A.; validation, B.A.; formal analysis, B.A., J.d.B., and T.D.; investigation, B.A.;

writing – original draft, B.A.; writing – review & editing, B.A., J.d.B., and T.D.; visualization, B.A. and T.D.; supervision, T.D.; funding acquisition, T.D.

## DECLARATION OF INTERESTS

The authors declare no competing interests.

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