

# **VARIOUS DESIGN AND ANALYSIS TASKS FROM CONCEPTUAL AND PRELIMINARY DESIGN APPLIED TO THE SMR AIRCRAFT CONFIGURATION DLR-D2AE**

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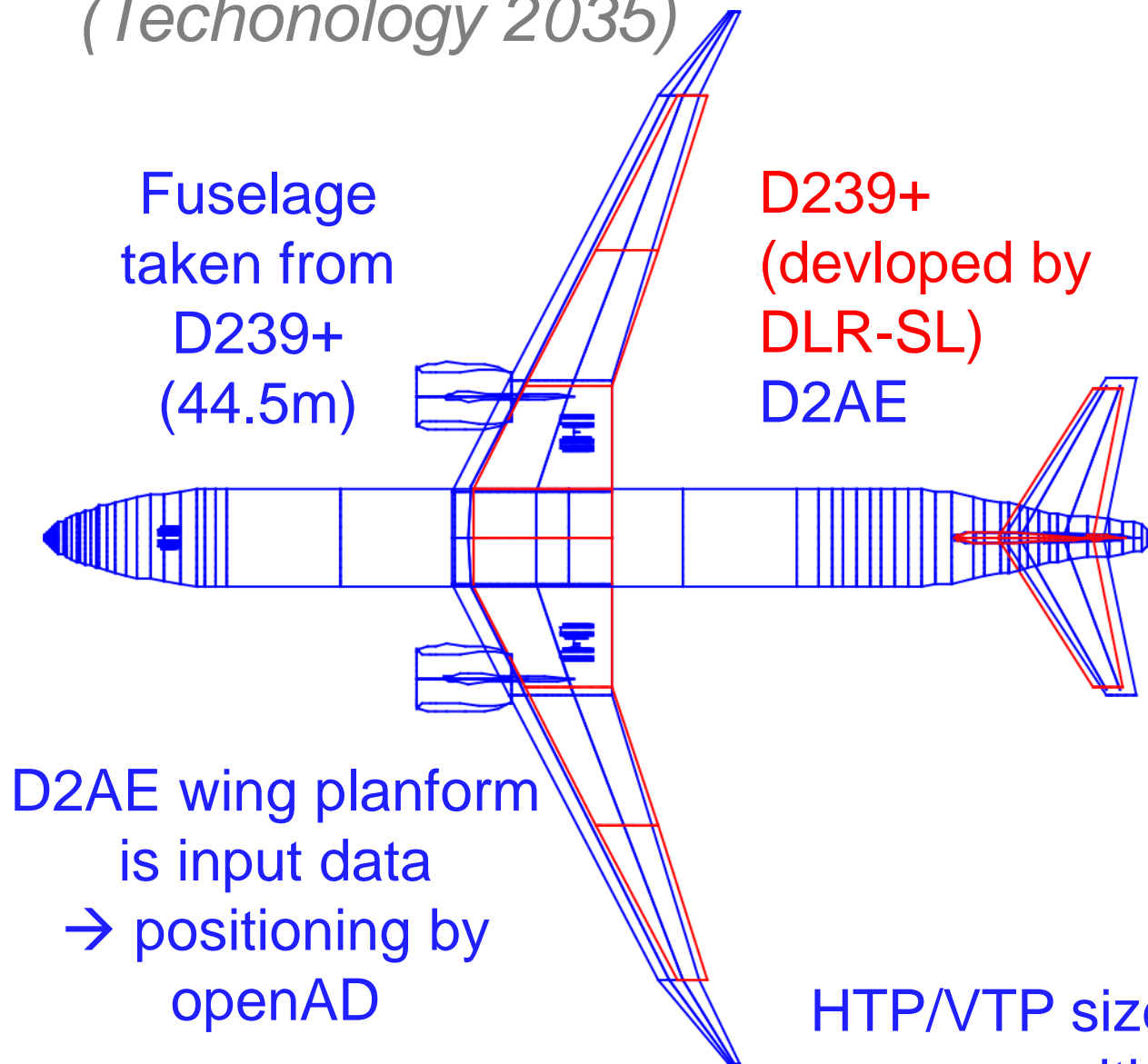
# Overview



- The D2AE configuration
- DLR-AE/LAE aeroelastic design group capabilities
  - Conceptual Design Loads
  - Parametric modelling for the fuselage structure
  - Aeroelastic design process cpacs-MONA
  - Composite structural optimization
  - Non linear structural analysis
- Summary and outlook

# D2AE Configuration – SMR Configuration for 239 PAX

(Technology 2035)



## TLARs D2AE

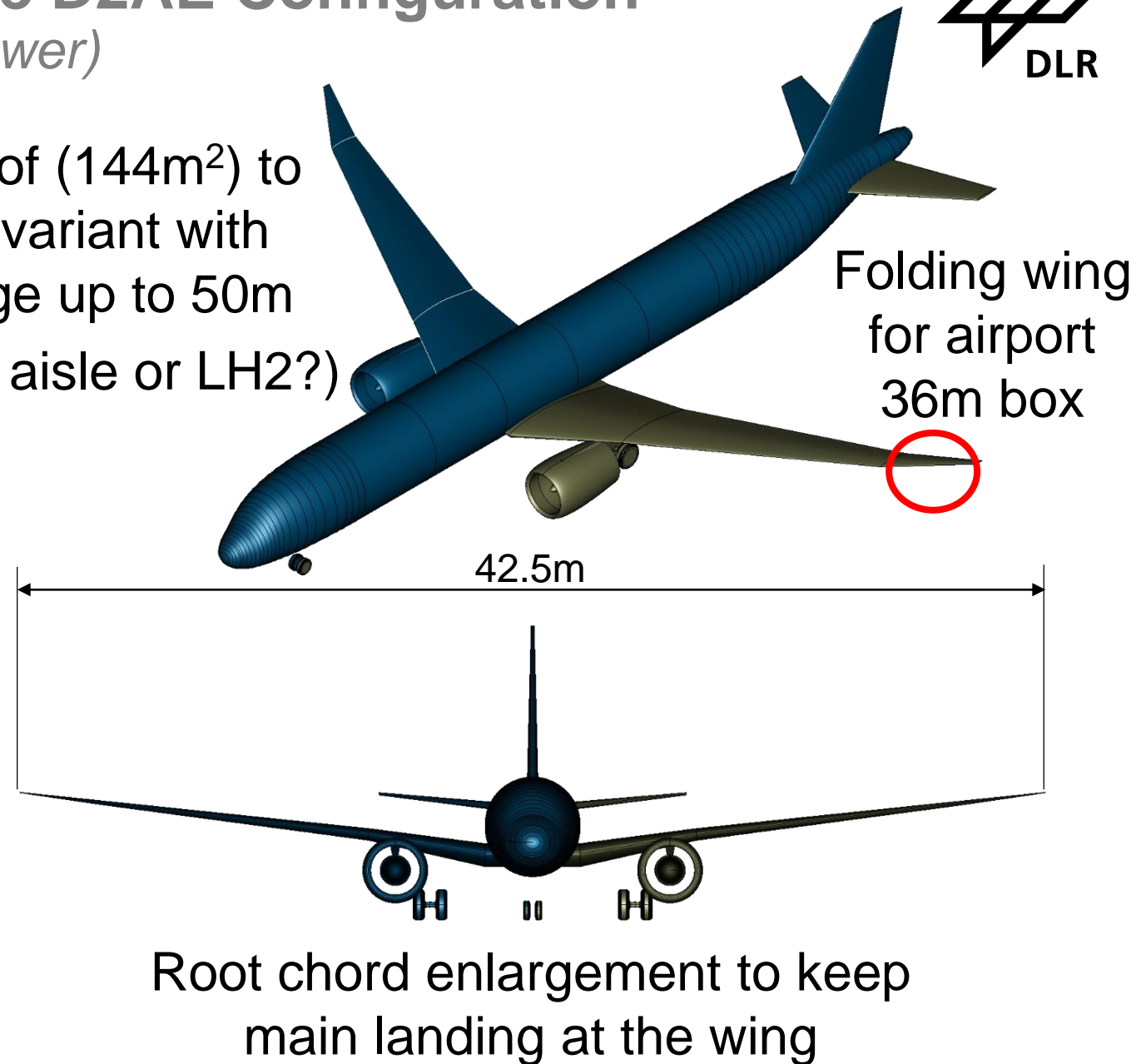
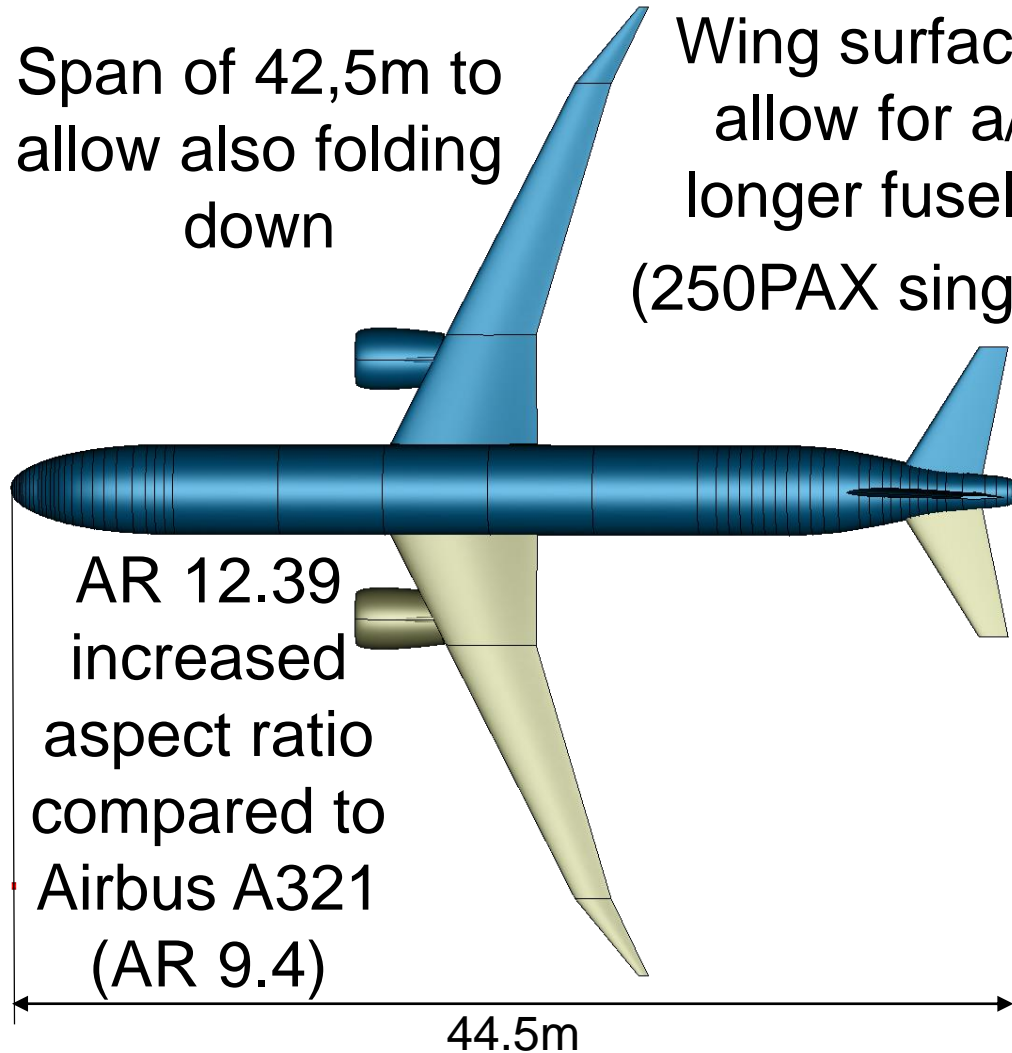
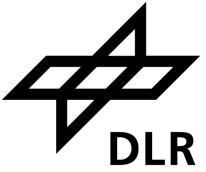
Design Range	[nm]	2500
Design PAX (single class)	[-]	239
Mass per PAX	[kg]	95
Design Payload	[kg]	25000
Max. Payload	[kg]	25000
Cruise Mach number	[-]	0.78
Max. operating Mach number	[-]	0.8
Max. operating altitude	[ft]	40000
TOFL (ISA +0K SL)	[m]	<2200
Rate of Climb @ TOC	[ft/min]	>300
Approach Speed (CAS)	[kt]	136
Wing span limit	[m]	<b>42.5</b>
Alternate Distance	[nm]	200
Holding Time	[min]	30
Contingency	[-]	3%

HTP/VTP size and position, and landing gear position estimated by openAD

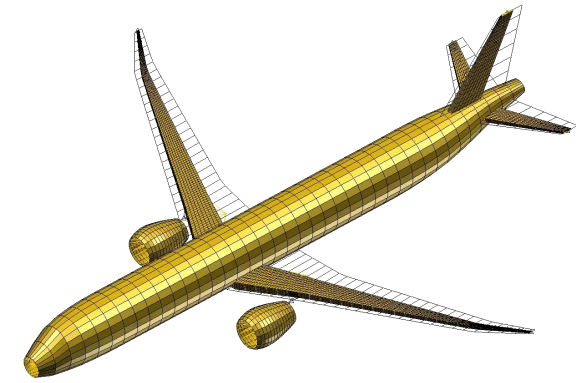
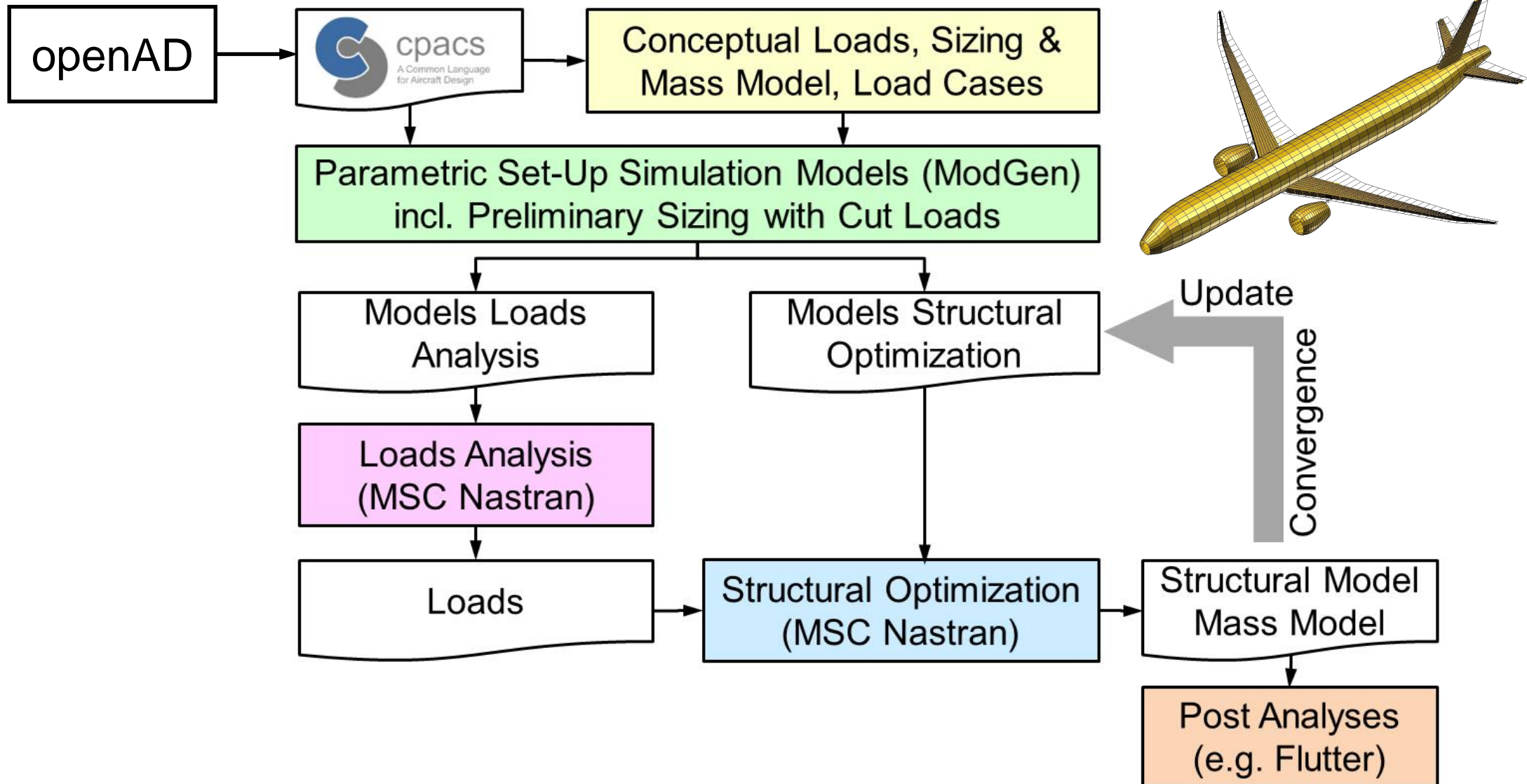


# Results openAD – View of the D2AE Configuration

(CPACS Visualization with TiGL Viewer)

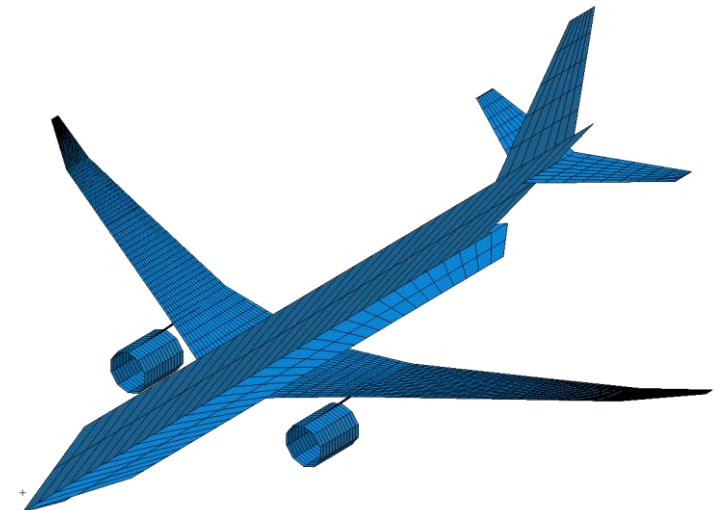
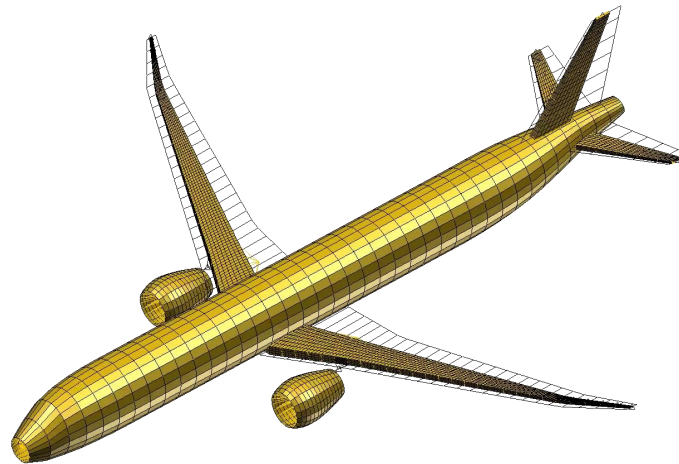
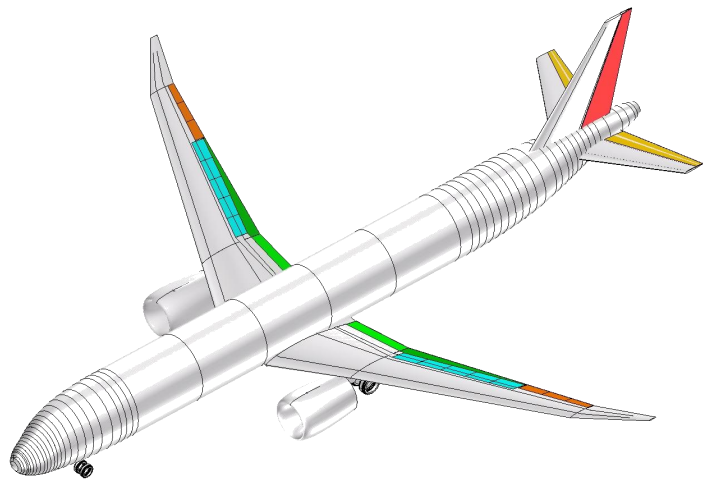


# cpacs-MONA – Parametric Aeroelastic Design Process



# Resulting Data cpacs-MONA

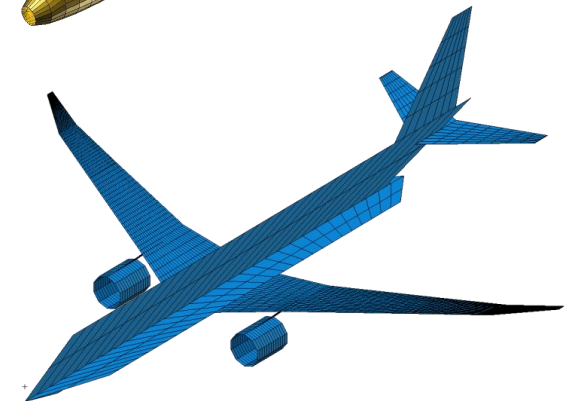
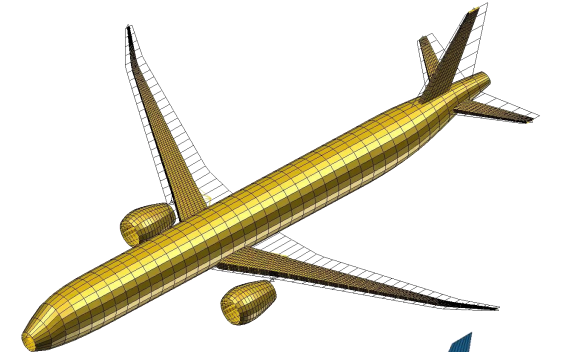
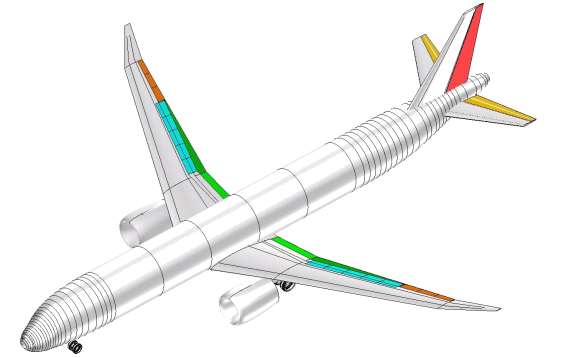
- Various loads for the complete aircraft (conceptual and preliminary)
- Mass estimation for aircraft components
- Structural model as finite element model for the complete aircraft (MSC Nastran)
- Detailed Mass model available for various mass configurations
- Aerodynamic Model as Doublet Lattice model (correction parameters implemented, e.g. camber data, fuselage correction)



# DLR-AE/LAE Aeroelastic Design Group Capabilities



- Conceptual Design Loads
  - Parametric modelling for the fuselage structure
  - Aeroelastic design process cpacs-MONA
  - Composite structural optimization
  - Non linear structural analysis
- 
- Applied to the D2AE configuration
  - Basis D2AE openAD CPACS-Dataset and cpacs-MONA results

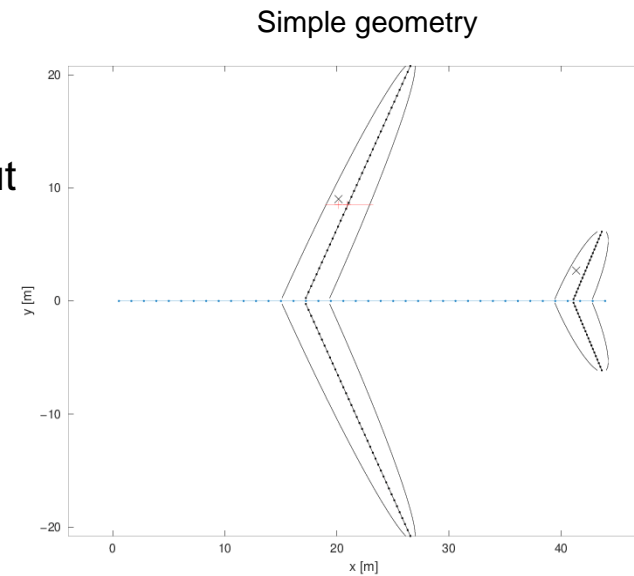


# Conceptual Design Loads

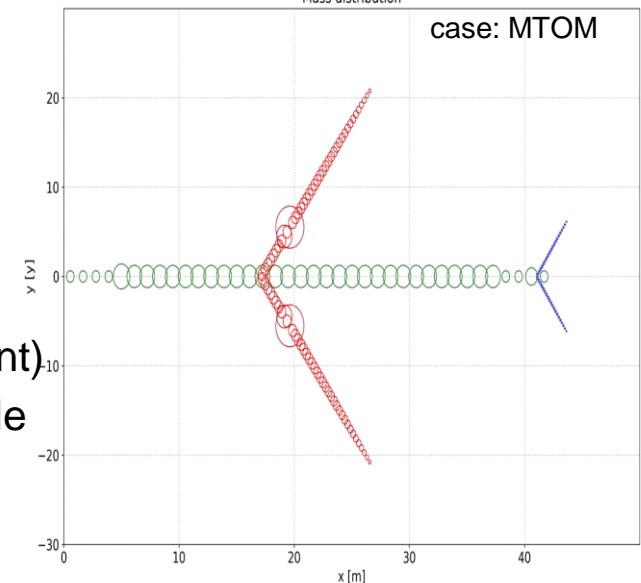
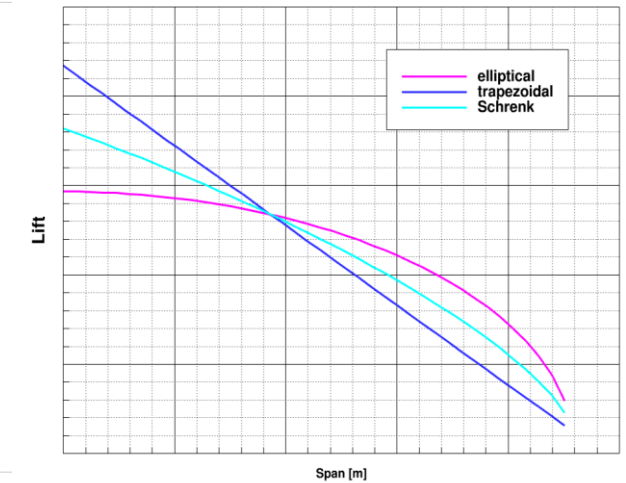
## Background

Fast and simple flight loads estimation with minimal input

- Set up of simple geometry model – rigid
  - Example – elliptical chord distribution
  - Resulting lift distribution is elliptical
  - Other lift distributions: trapezoidal and Schrenk (combined)
- Set up of simple mass model OEM, MZFM, MTOM
  - Point masses (e.g. engines)
  - Line related masses (e.g. fuselage)
  - Area related masses (e.g. wing)
  - Volume related masses (e.g. fuel)
- Set up of load cases (CS25) and resulting load factor (quasi-static)
  - Manoeuvre loads 2.5g Pull-up -1g push-down with EAS speed (altitude independent)
  - Gust loads according to Pratt – additional load factor (in CS23, for CS25 acceptable in conceptual design)
- Sum of loads for aerodynamics and inertia loads → nodal and cut loads

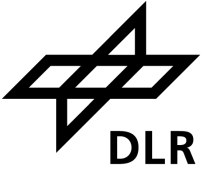


lift distributions

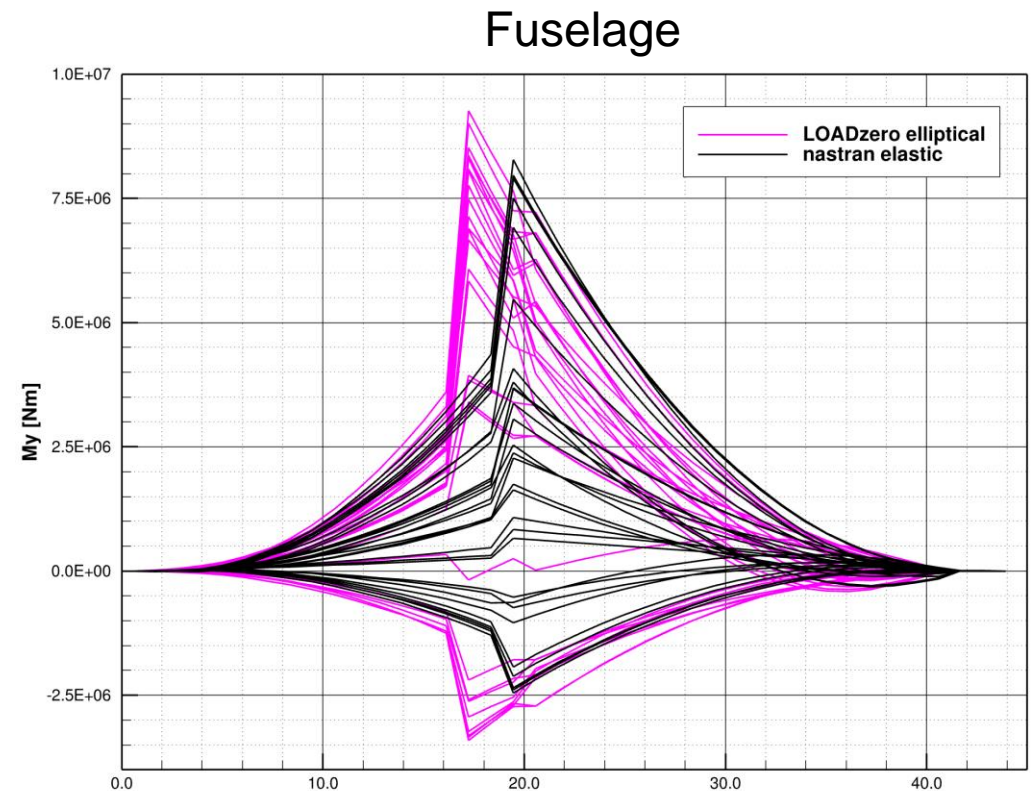
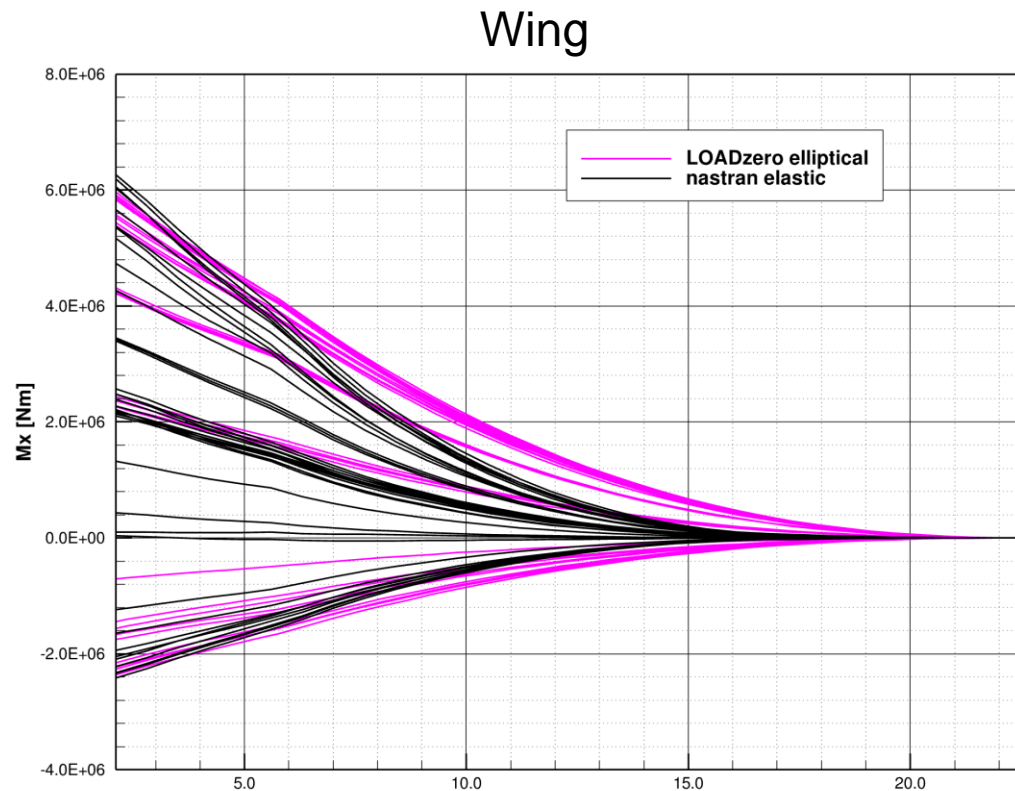




# Conceptual Design Loads



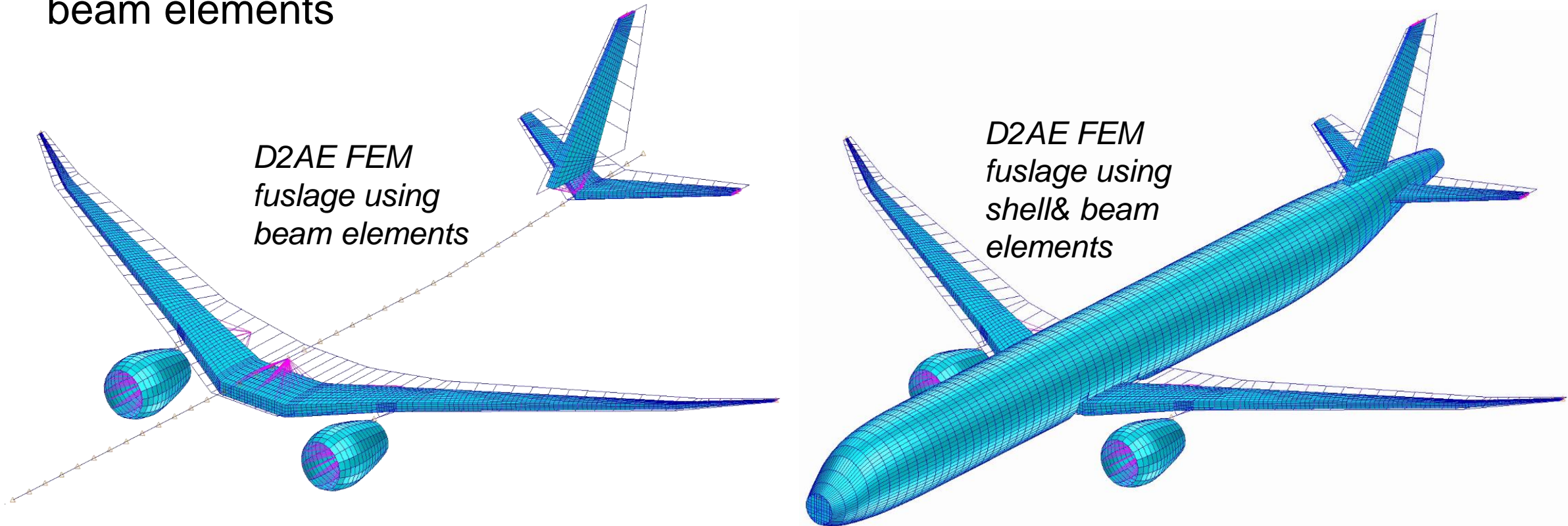
- Comparison conceptual loads with cpacs-MONA loads



➤ Overall good agreement at a conceptual level

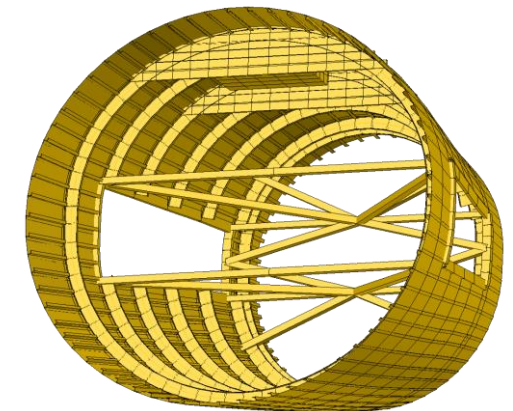
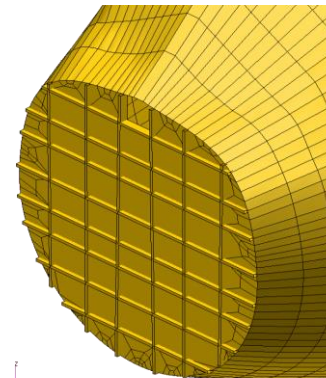
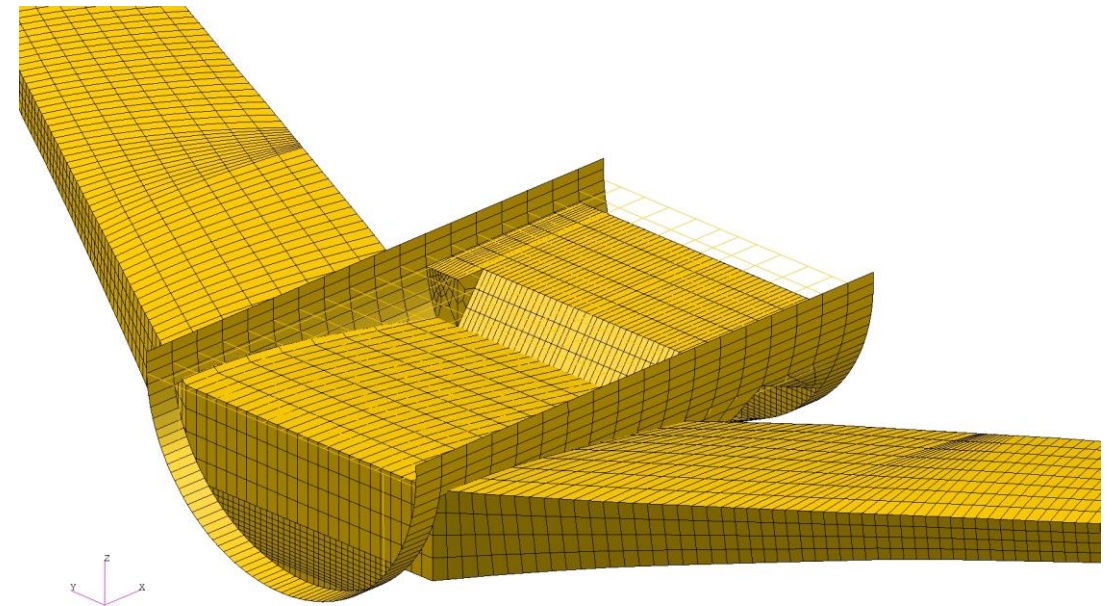
# Parametric modelling for the fuselage structure

- CPACS allows for a detailed structural description also for the fuselage
- Further development of ModGen to generate fuselage fems with shell and beam elements



# Parametric modelling for the fuselage structure

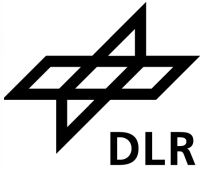
- Details of structural description
- Advantages
  - More realistic wing/fuselage integration
  - HTP and VTP integration
  - Loads transfer more realistic especially for landing loads
  - Better distributed mass estimation and modelling
  - More realistic stiffness and dynamic characteristics
- Structural optimization methods already predeveloped





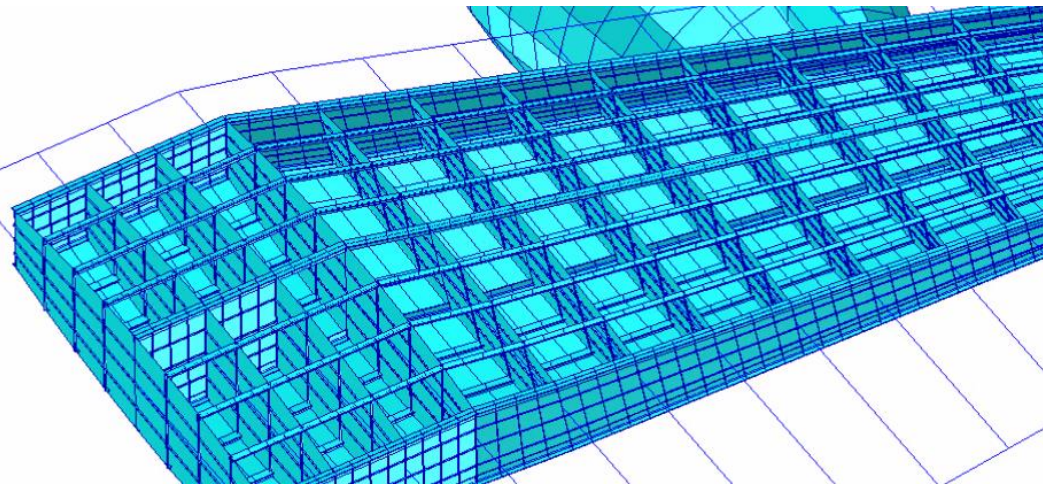
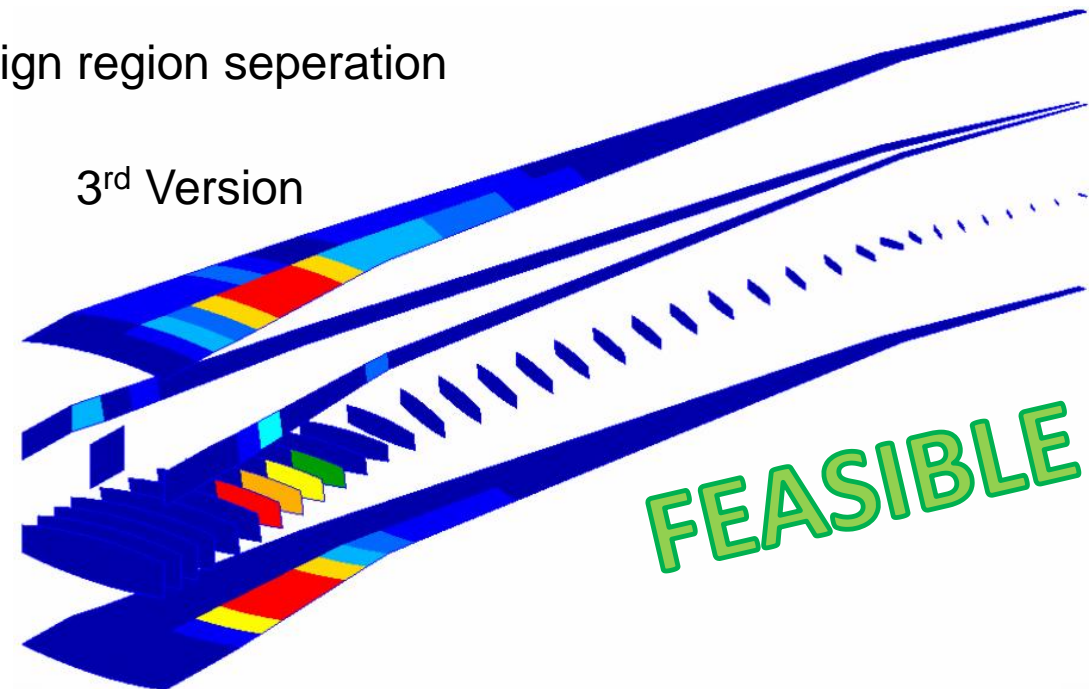
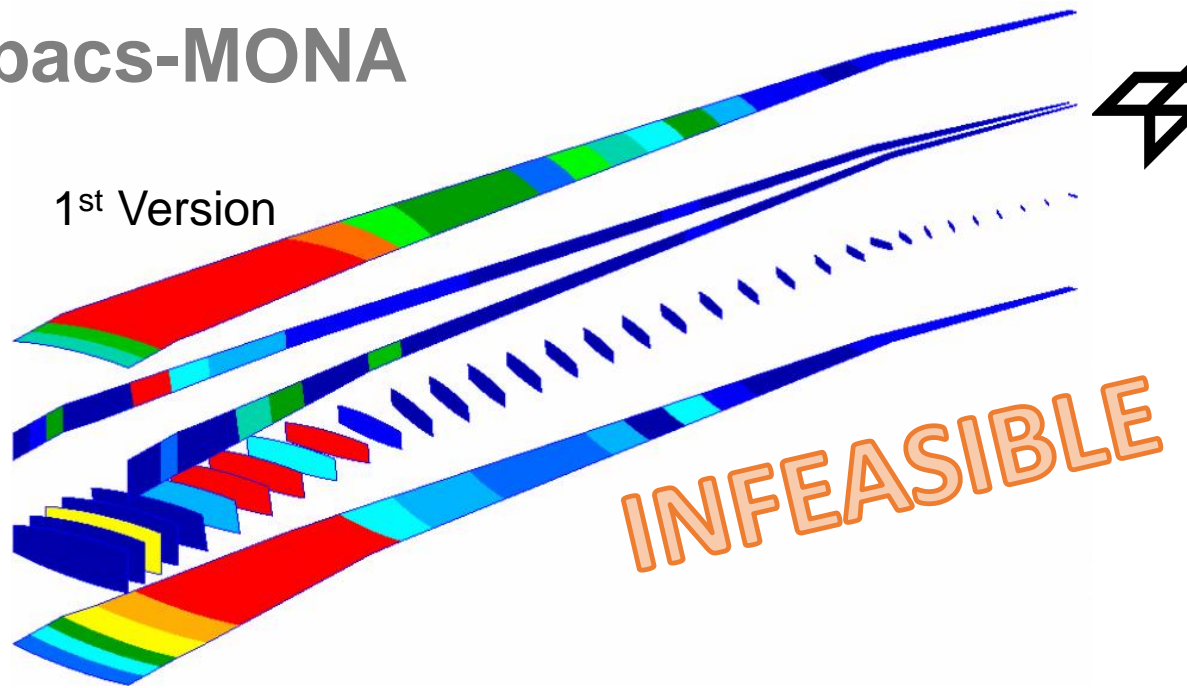
# Aeroelastic design process cpacs-MONA

## Design Adaption



- 1<sup>st</sup> version leads to infeasible design
  - High loads around the landing gear
- Adaptions for 2<sup>nd</sup> version:
  - Shifed rear spar backwards
  - Shifted landing gear forward
  - Introduced a mid-spar
- Adaptions for 3<sup>rd</sup> version:
  - Changed the mid-spar to a „tiny“-spar → design region seperation without a „stuctural“ reinforcement

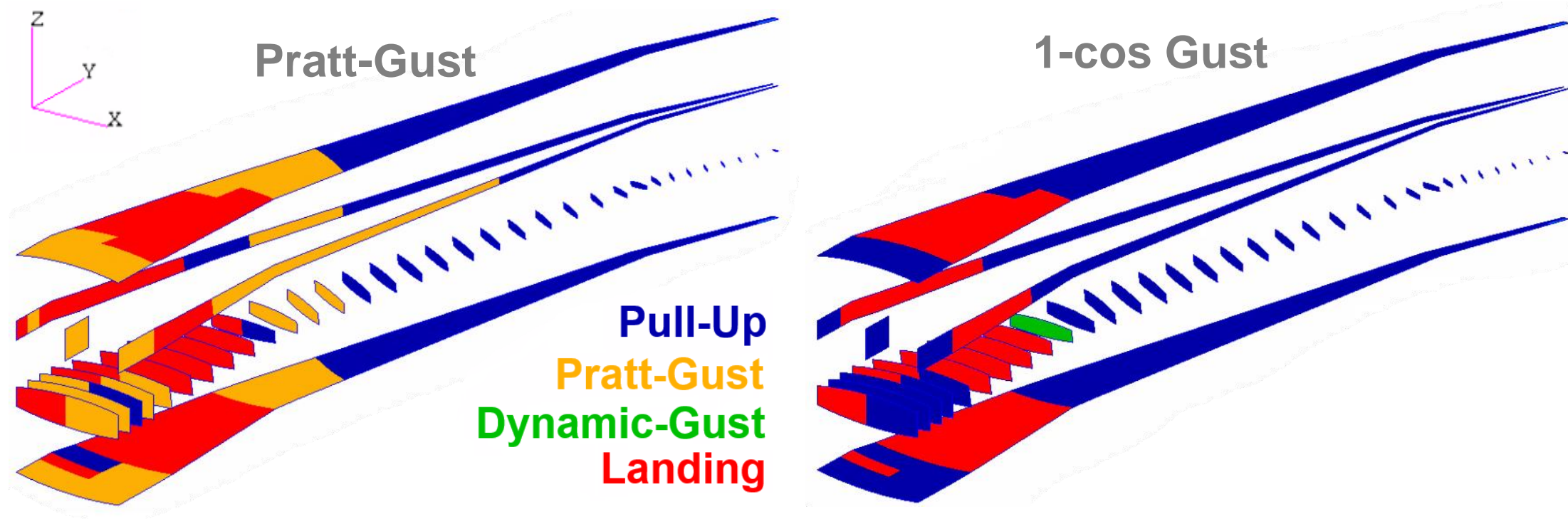
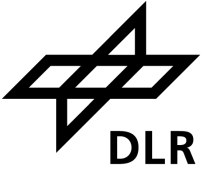
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# Aeroelastic design process cpacs-MONA

## Pratt-Gust vs. Dynamic 1-cos Gust



Parameter	Pratt-Gust	1-cos Gust
Wing primary mass	8832 kg	8597 kg
Max. Mx	7.08e <sup>6</sup> Nm	6.85e <sup>6</sup> Nm
1st elastic Eigenfreq. (OEM)	3,371 Hz	3.366 Hz

# Composite structural optimization

## Overview



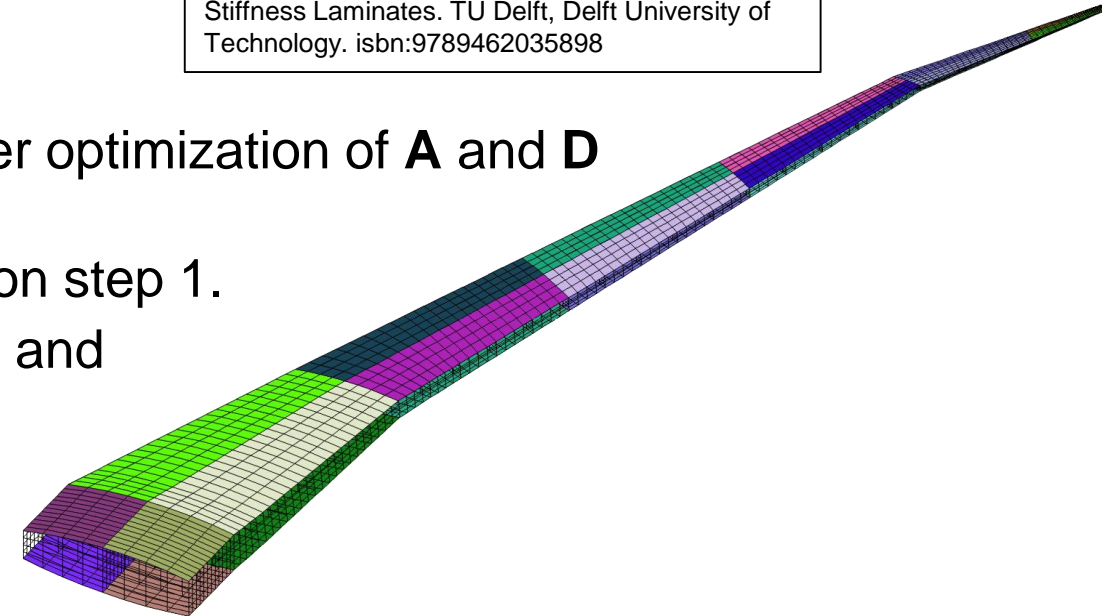
[1] Dillinger, J. K. S. et al. (2013). Stiffness optimization of composite wings with aeroelastic constraints. Journal of Aircraft  
[2] Dillinger, J. (2014). Static Aeroelastic Optimization of Composite Wings with Variable Stiffness Laminates. TU Delft, Delft University of Technology. isbn:9789462035898

### ■ two-step aeroelastic optimization process:

- continuous, gradient-based lamination parameter optimization of **A** and **D** stiffness matrices
- discrete stacking sequence optimization based on step 1.
- Nastran used to generate and export responses and sensitivities, optimization performed externally

### ■ optimization model setup:

- design field definition:
  - each featuring one set of **A** and **D** (sample: 14+14=28 fields)
- response definition:
  - e.g. **mass**, element stress to compute **strain and buckling failure**, displacement, twist, root bending moment, aileron efficiency, eigenfrequency, ...
- load case definition:
  - e.g. static **+2.5g pull-up, -1.0g push-down**, fixed angle of attack, aileron deflection, static loads



constraints in the following sample

objective in the following sample

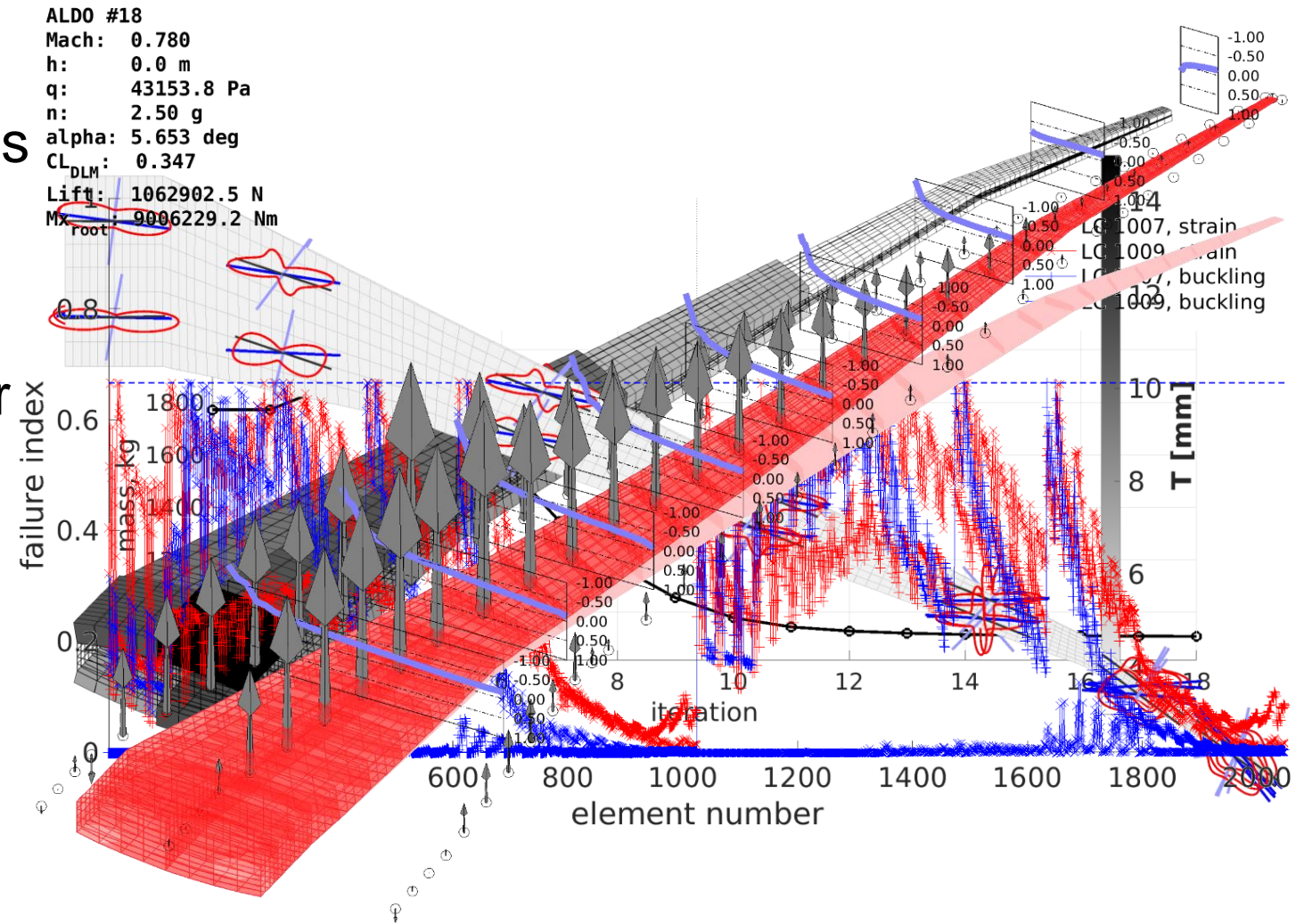
load cases in the following sample

# Composite structural optimization

## Sample Results

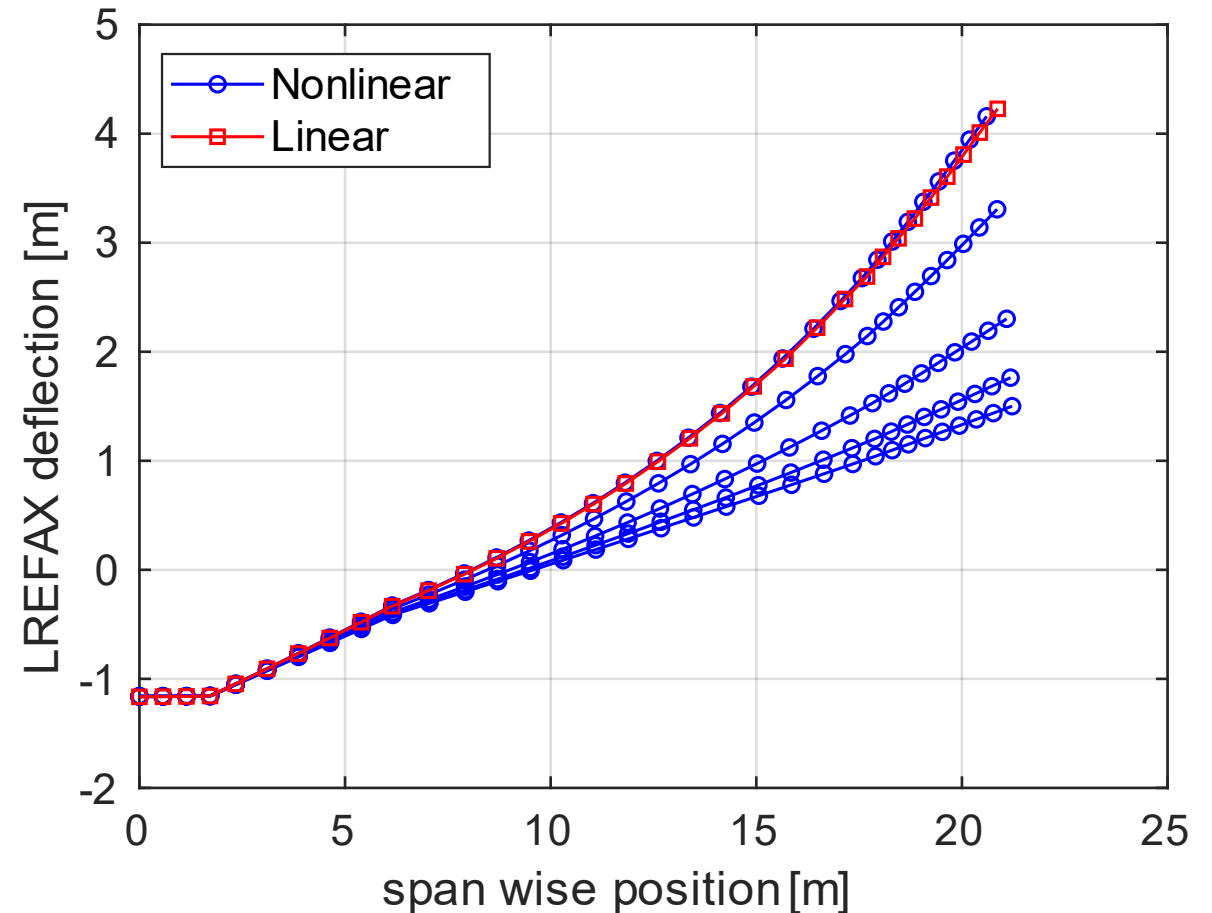


- development of wing skin mass throughout the iterations
- optimized thickness
- optimized polar E-modulus per design field
- failure indices for +2.5g and -1.0g load cases
- sample of aeroelastic loading generated with the coupled doublet lattice model



# Nonlinear structural analysis - Displacements

- Nonlinear analysis of the clamped wing structure conducted (SOL 400 MSC Nastran)
- 2.5g manoeuvre load case generating the maximum tip deflection ~13 % of half-span applied in the study.
- Nonlinear transverse displacement ~ 2.5 % lower than linear case
- Nonlinear spanwise in-plane displacement ~ 42 % higher than linear case.



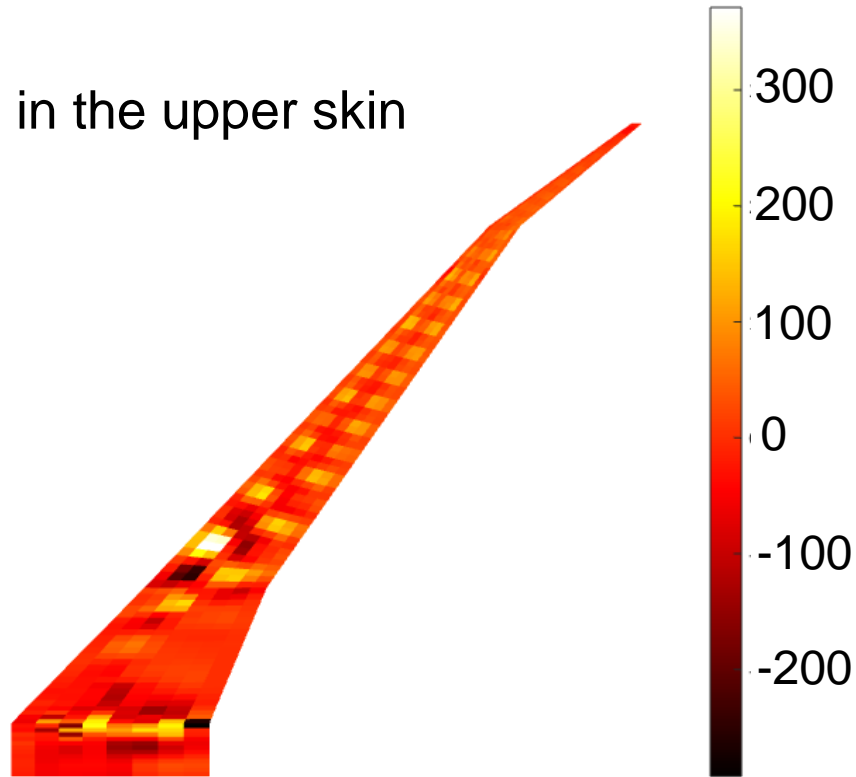
*Static deflection in the right wing for a 2.5g manoeuvre case*



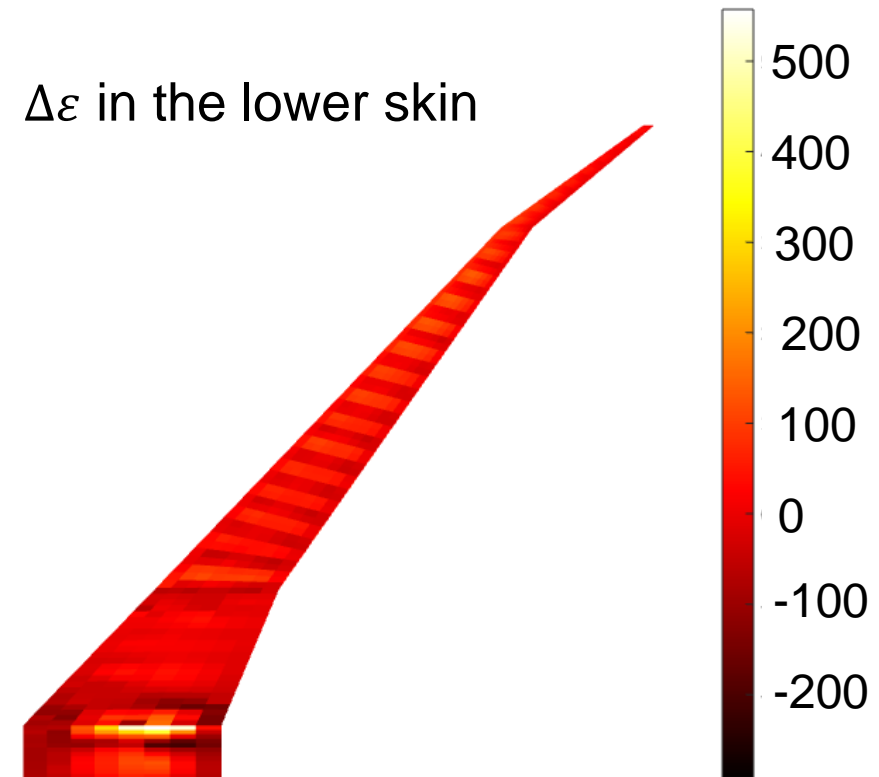
# Nonlinear structural analysis - Strains



$\Delta\varepsilon$  in the upper skin



$\Delta\varepsilon$  in the lower skin

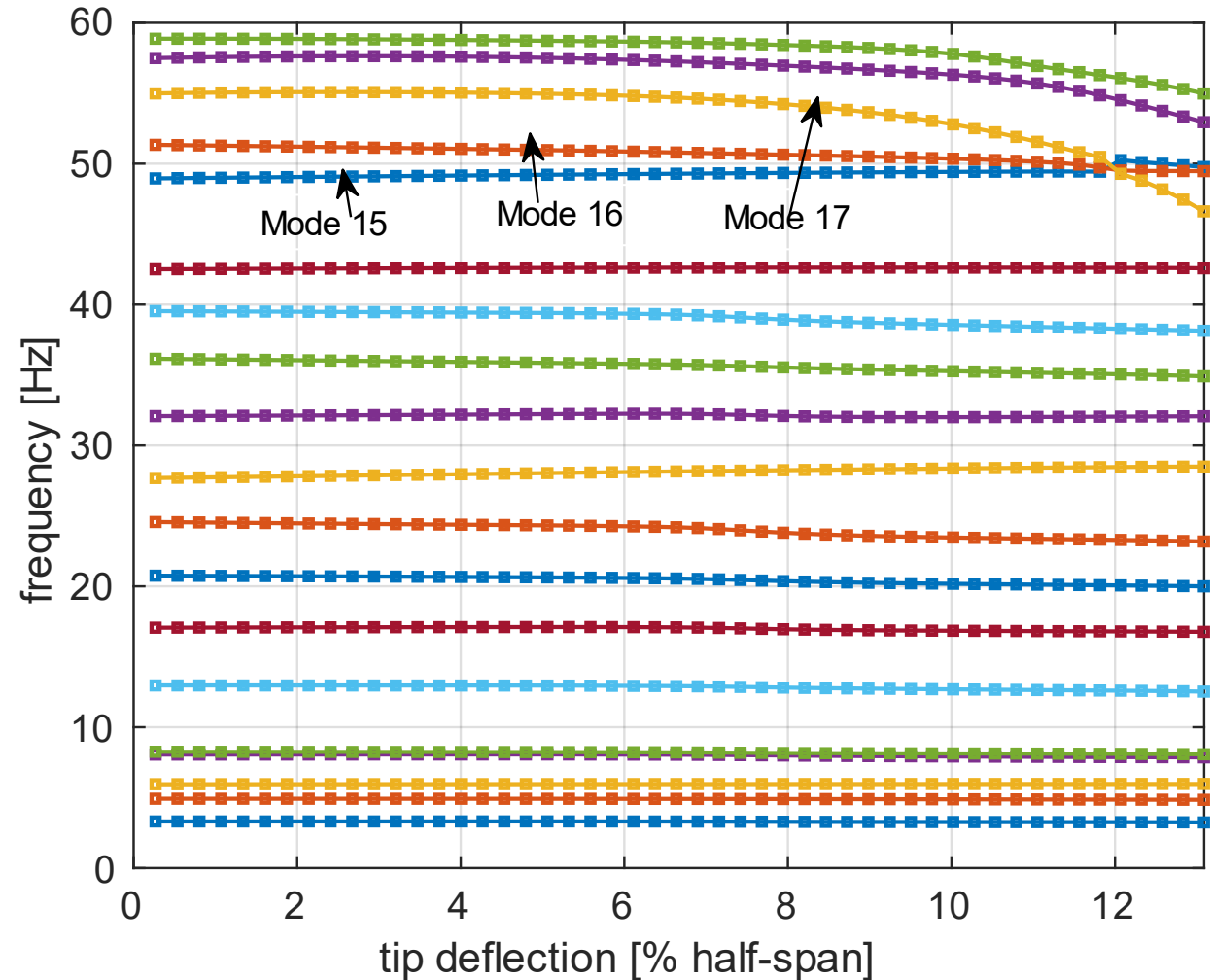


- Difference between linear and nonlinear strains in the range of  $-200 \mu\varepsilon$  and  $+500 \mu\varepsilon$ .
- Consideration of fully nonlinear strain models may have an impact on the sizing results.

# Nonlinear structural analysis – Frequencies



- Linear modal analysis conducted at different states of nonlinear deflection.
- Eigenfrequencies under 20 Hz do not show much variation.
- Certain eigenfrequencies above 50 Hz show drastic variations, onset already under 10 % tip deflection.
- Intersecting eigenfrequency curves of Modes 15, 16 and 17 indicate potential mode coupling and unstable oscillations.

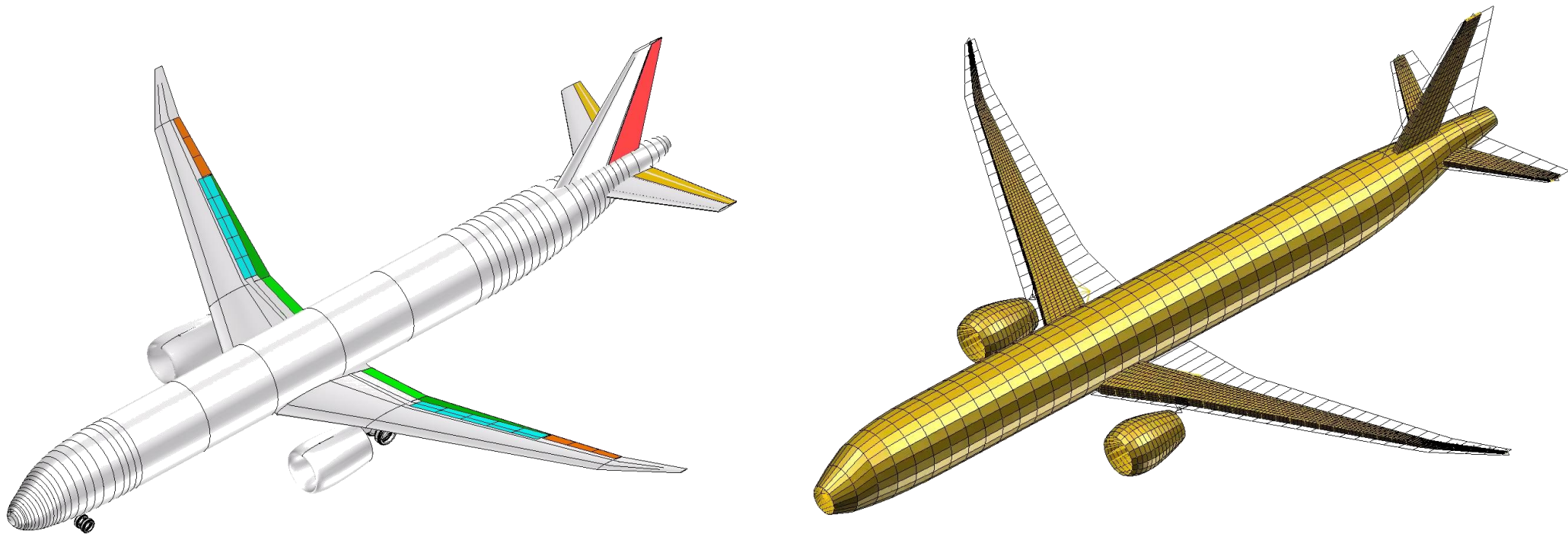


# Summary Outlook



- DLR AE's SMR configuration D2AE presented
- Various analysis and design capabilities of the design group presented from conceptual design to preliminary design
- D2AE is constantly further developed
  - Parametric modelling to smoothen the interfaces to the various analysis and design methods
  - New simulation models like structural modelling of the engine pylon with shell and beam elements → aeroelastic design tasks
  - Improvement of the geometry modelling in order to set-up CFD meshes → loads analysis

# Thank you very much for your attention!



D2AE – developed @ DLR-AE