

CHARACTERIZING AIRFLOW TURBULENCE IN THE ACOUSTIC WIND TUNNEL BRAUNSCHWEIG (AWB) USING TURBULENCE GRIDS

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- Experimental Setup
- Numerical Setup
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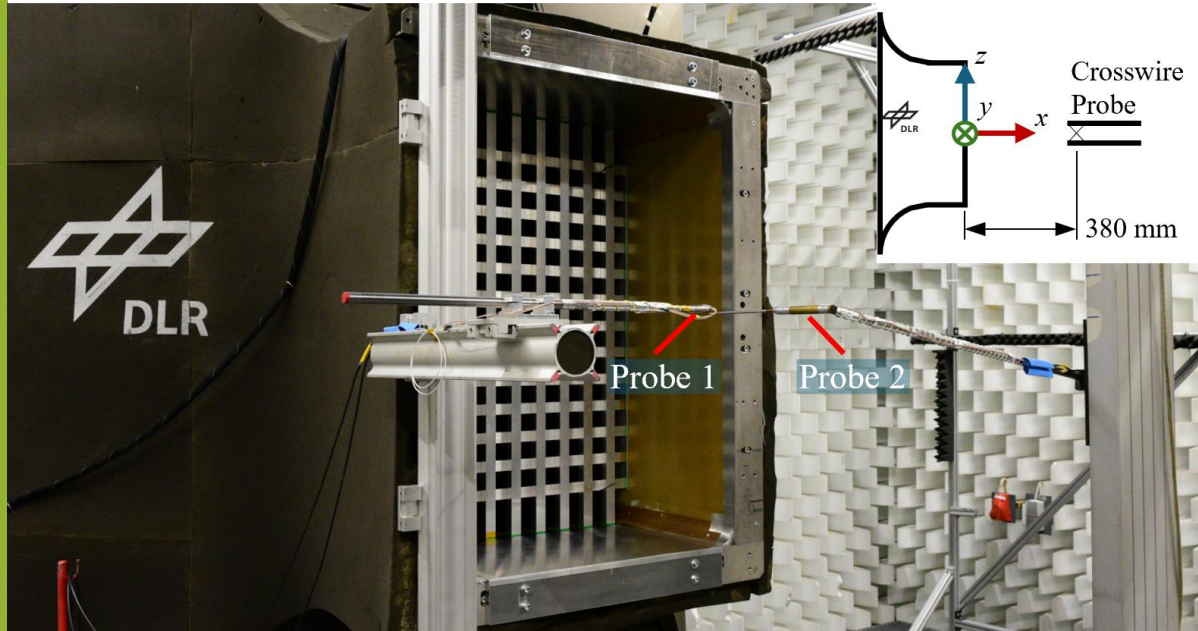


Introduction



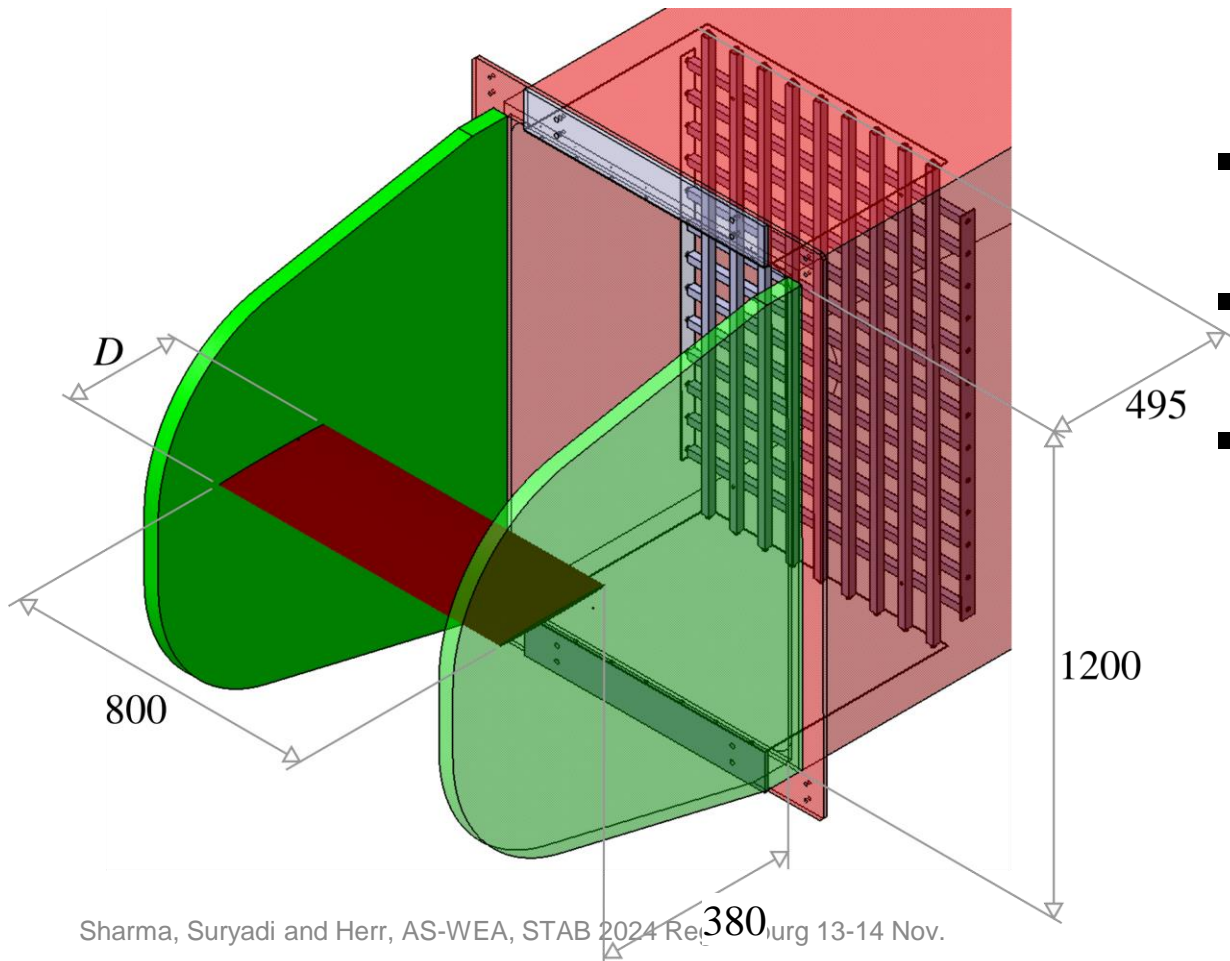
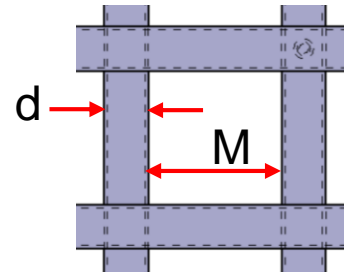
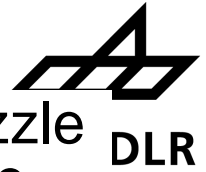
- Wind turbines immersed in atmospheric turbulence with eddies on a scale larger than the leading edge radius of the blade profile leads to excess noise radiated from the leading-edge.
- Wind tunnels are configured to have minimal inflow turbulence, hence unsuitable for leading-edge noise study.
- A turbulence grid generator is a well-known device to produce homogeneous and isotropic turbulence.
- In this study, the Acoustic Wind Tunnel Braunschweig is equipped with turbulence grid generators to produce large scale turbulence for the purpose of leading-edge noise research.
- Isotropy is not a constraint as anisotropy can be present in the atmosphere.

Experimental Setup



- Acoustic Wind Tunnel Braunschweig,
 - Max wind speed= 65 m/s
 - 0.3% turbulence intensity
 - Anechoic at $f > 200$ Hz
- HWA: 2 X-wire probes
 - Probe 1: stationary
 - Probe 2: traversing in x, y, z
- Probes are placed at $x = 380$ mm (< 10 mm from the leading edges of NACA 0012 and NACA 66-006)
- SR= 50 kHz, T=10s
- Discussion today is focused on flow measurements.

Turbulence Grid



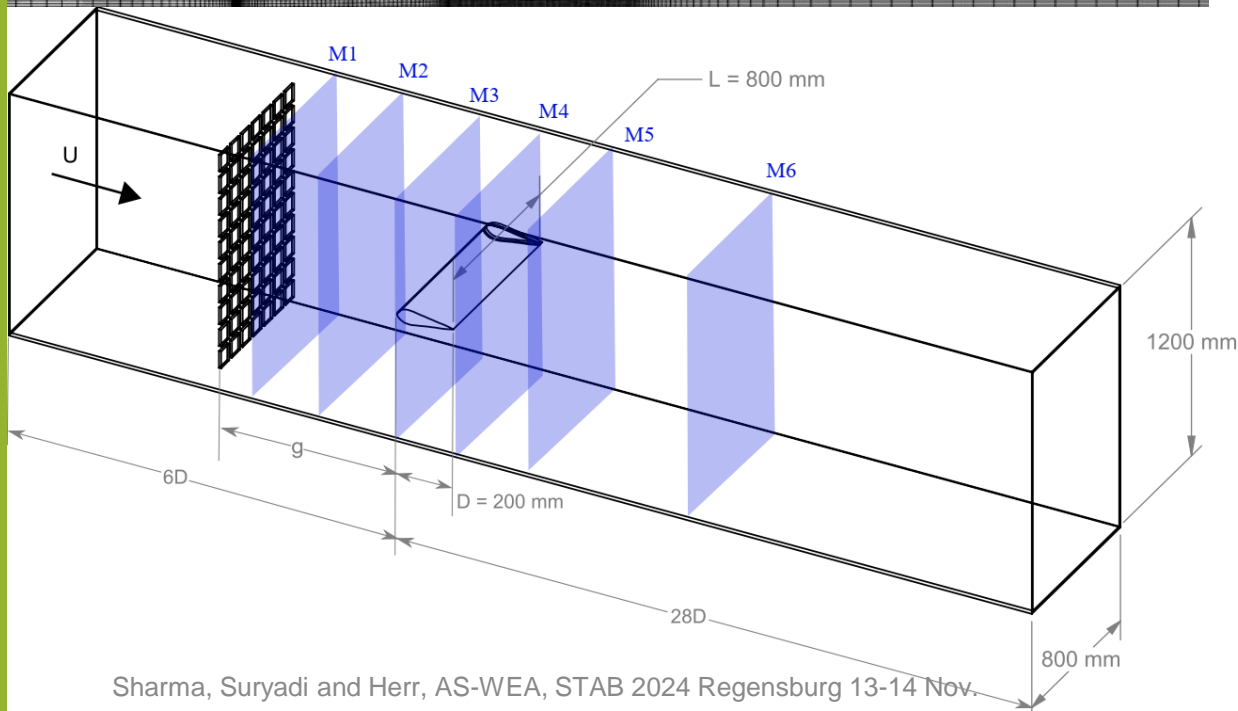
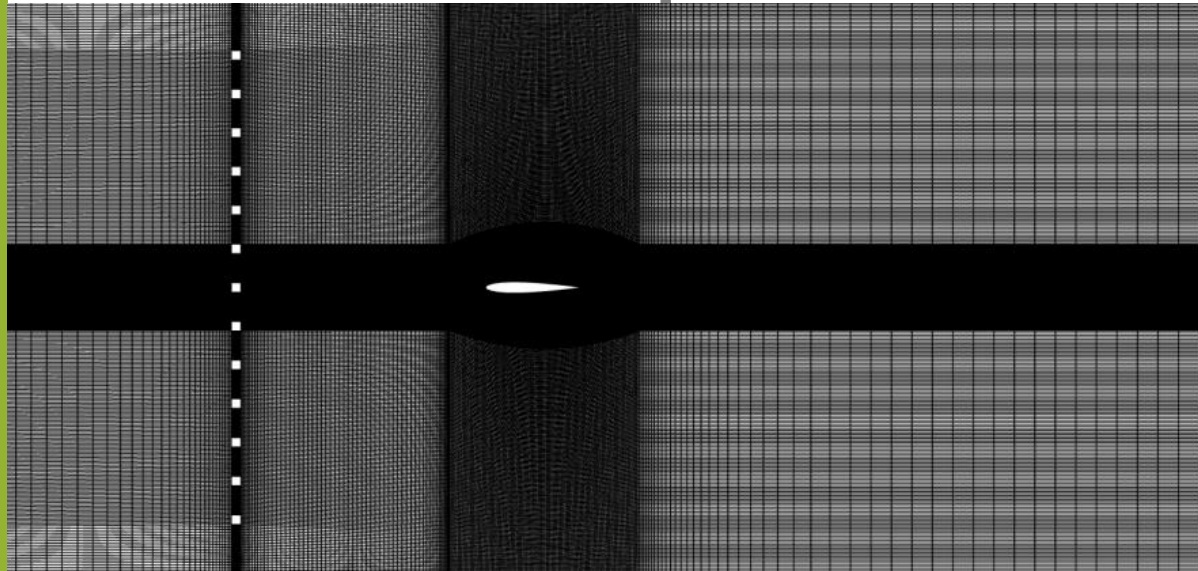
- Grid is placed 495 mm inside the nozzle held by 2 plates top and bottom of the nozzle fastened to the outside frame of the nozzle
- Vertical and horizontal square-profiled aluminium pipes: $d \times d$ mm, spaced by M
- 4 fastening points between the vertical and horizontal bars
- Side panels connects horizontal bars with each other
- Blockage ratio $>33\%$ reduces maximum velocity below 40 m/s

Grid	Blockage Ratio, %	$\max(U_\infty)$, m/s
20×20_M60	39.3	30
20×20_M140	22.7	40
30×30_M50	55.3	20
30×30_M130	33.0	40
40×40_M120	42.5	25

Anisotropic

Isotropic

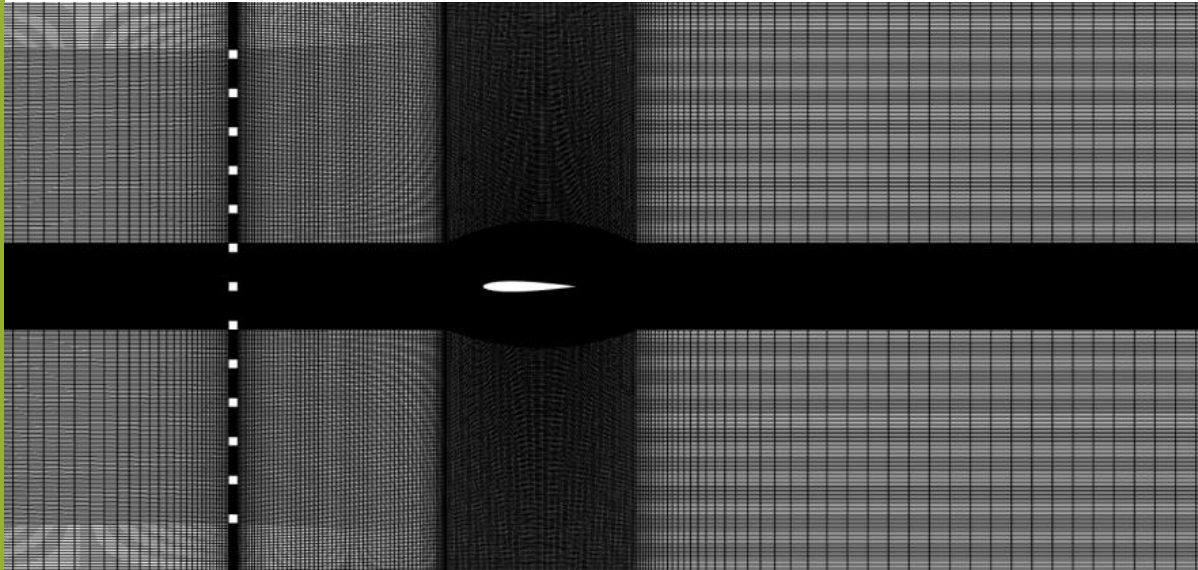
Numerical Setup



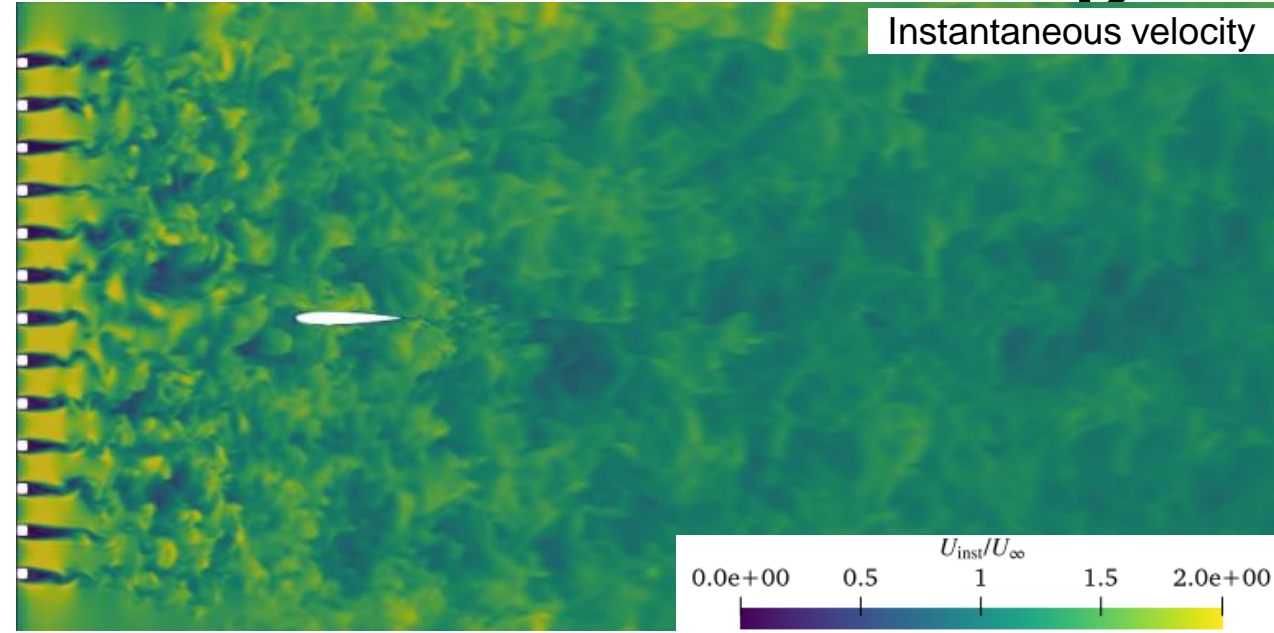
- LES implemented in OpenFoam
- Smagorinsky SGS
- Upper, lower boundary: symmetry planes
- Sides: periodic boundary conditions
- Airfoil and grid: no-slip walls
- Mesh refinement near airfoil, $y^+ < 1$
- 20.6 Million cells
- Nozzle is not defined in the simulation

Results

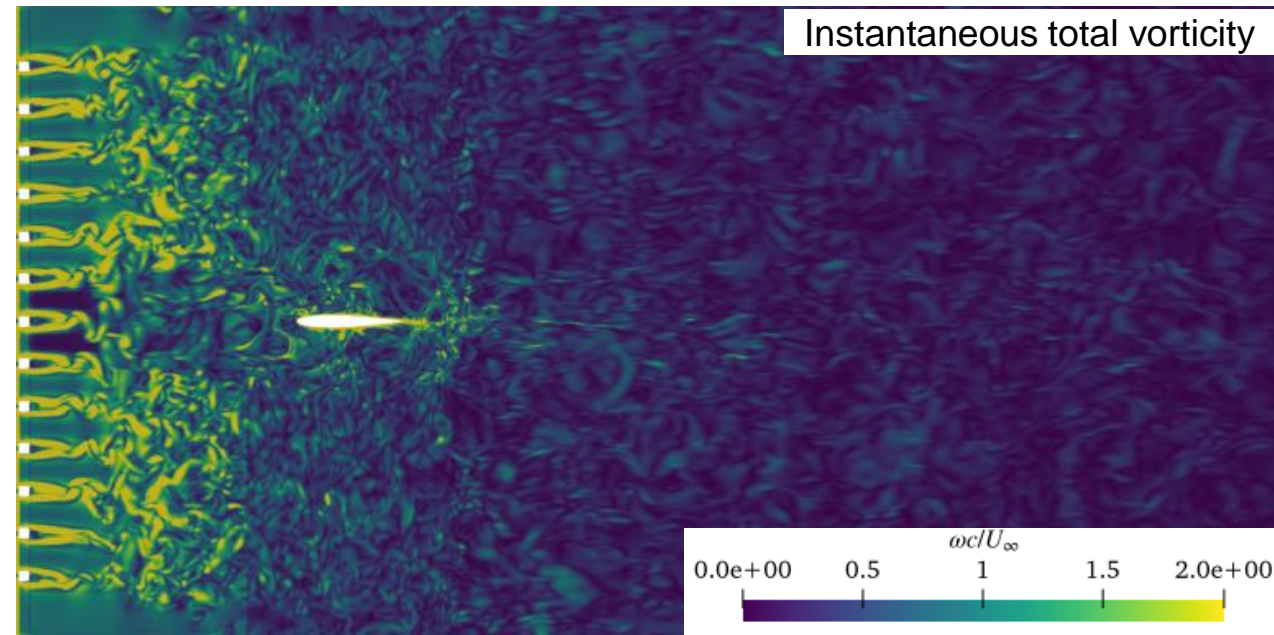
Numerical



Instantaneous velocity



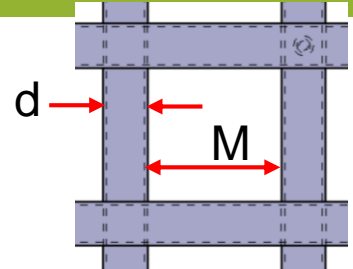
Instantaneous total vorticity



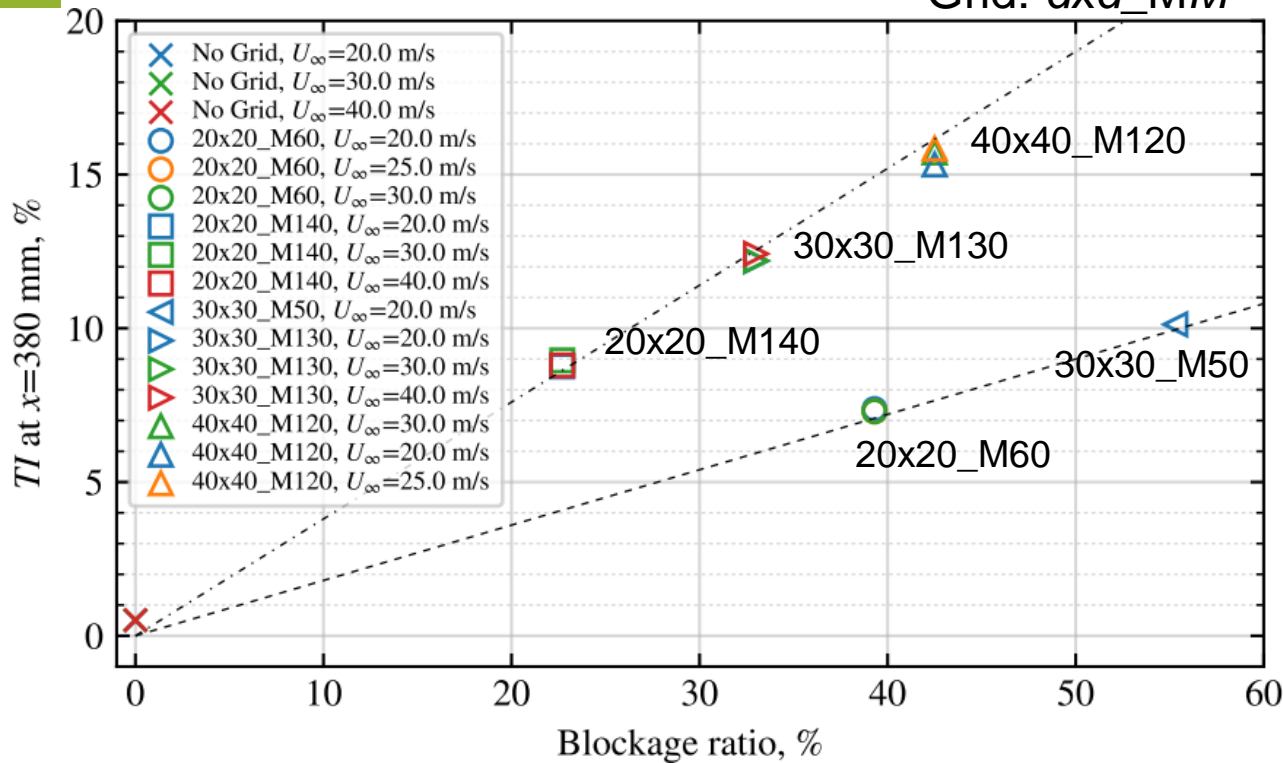
Results

Blockage Ratio vs Turbulent intensity

$$TI = \frac{\sqrt{u'u'}}{\sqrt{U^2 + V^2 + W^2}} \times 100\%$$



Grid: $d \times d$ MM

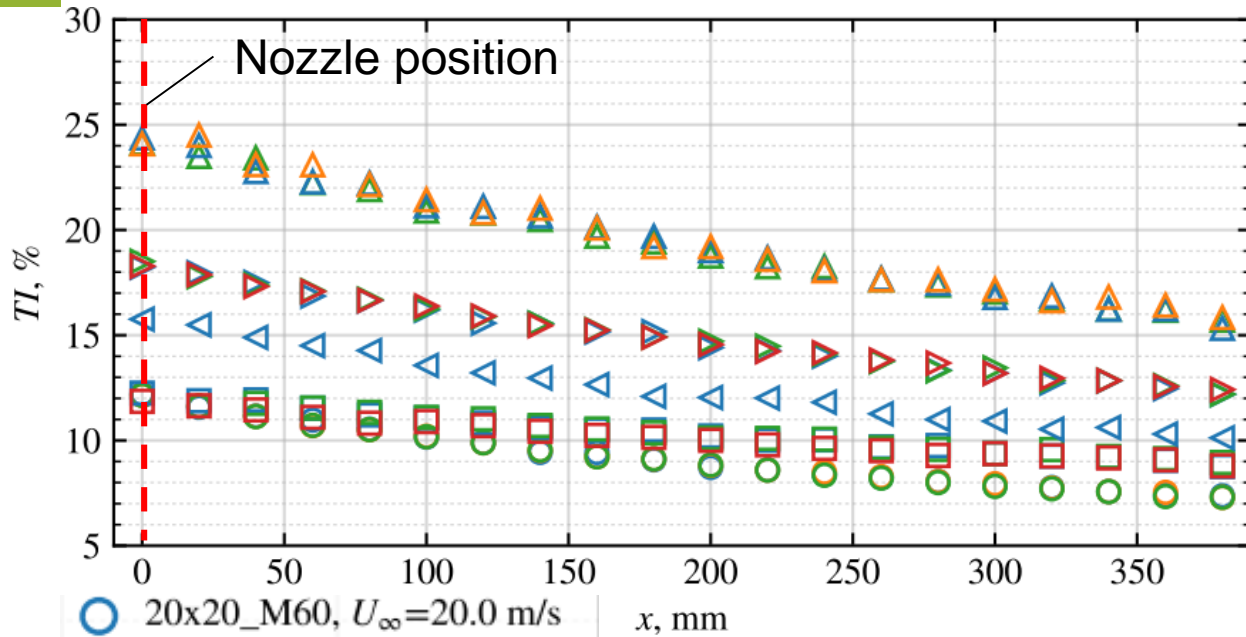


- Measured 875 mm downstream of grid
- Increased grid spacing reduces the blockage ratio but slightly increases the turbulence intensity
 - For $d=20$ mm, M60 \rightarrow M140.
 - For $d=30$ mm, M50 \rightarrow M130
- For approximately equal spacings, Turbulence intensifies with d

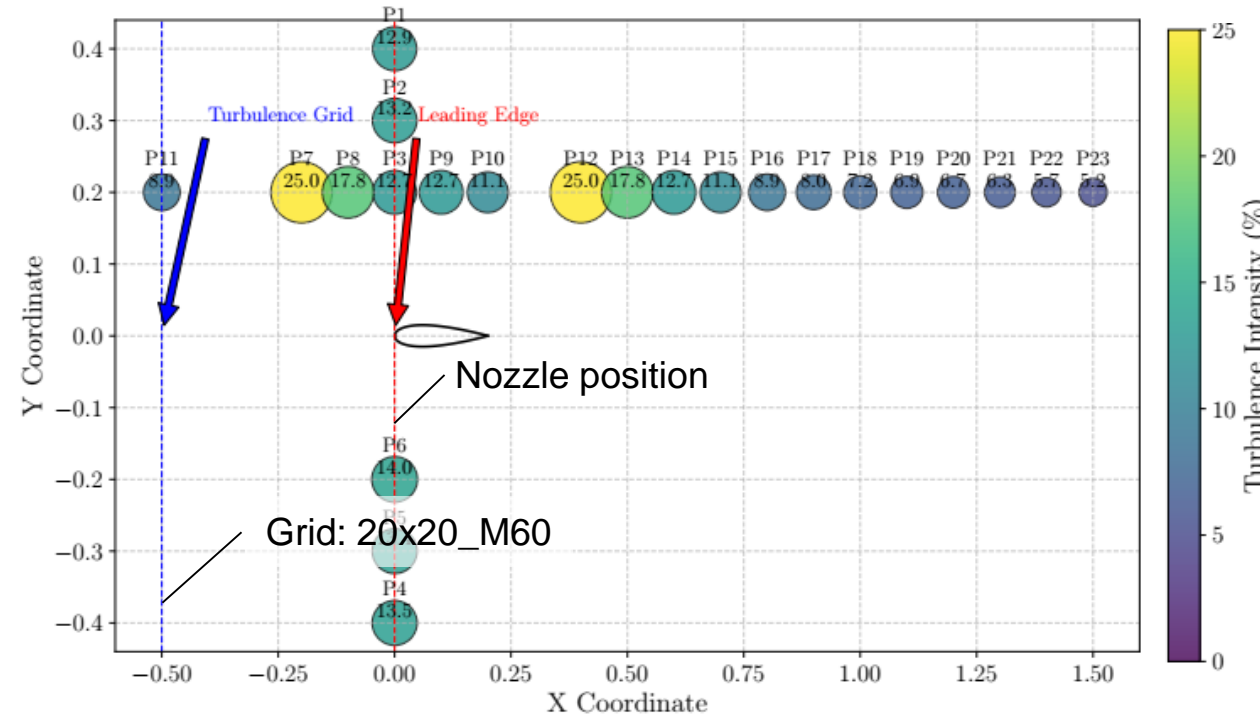
Results



Turbulent Intensity



- 20x20_M60, $U_\infty=20.0$ m/s
- 20x20_M60, $U_\infty=25.0$ m/s
- 20x20_M60, $U_\infty=30.0$ m/s
- 20x20_M140, $U_\infty=20.0$ m/s
- 20x20_M140, $U_\infty=30.0$ m/s
- 20x20_M140, $U_\infty=40.0$ m/s
- △ 30x30_M50, $U_\infty=20.0$ m/s
- △ 30x30_M130, $U_\infty=20.0$ m/s
- △ 30x30_M130, $U_\infty=30.0$ m/s
- △ 30x30_M130, $U_\infty=40.0$ m/s
- △ 40x40_M120, $U_\infty=30.0$ m/s
- △ 40x40_M120, $U_\infty=20.0$ m/s
- △ 40x40_M120, $U_\infty=25.0$ m/s



- Turbulence decay with x
- For 20x20_M60: Turbulence intensity at nozzle, $x=0$ mm, 12.7% - 14% in simulation, 12.5% in measurements.

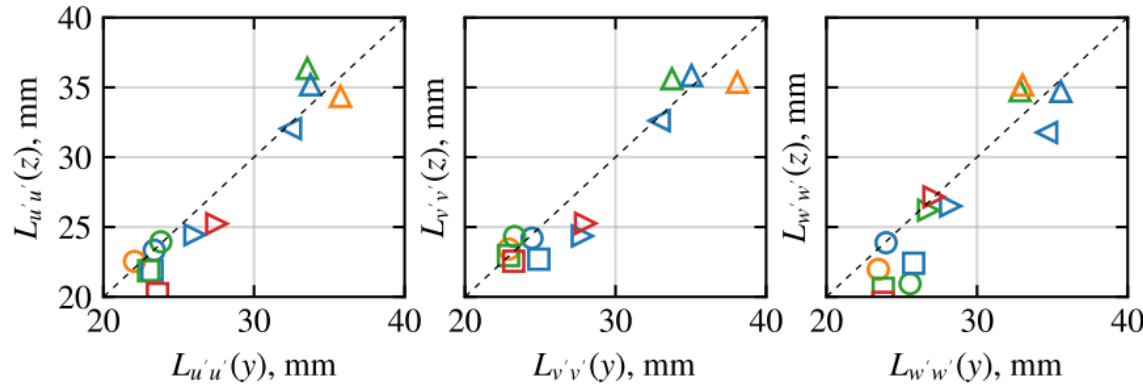
Results



Isotropy

$$L_{u'_{i}u'_{i}}(x_j) = \int_0^\infty R_{u'_{i}u'_{i}}(r) dr,$$

u' : stream vel., v' : vertical vel., w' : span vel.



- 20x20_M60, $U_\infty=20.0$ m/s
- 20x20_M60, $U_\infty=25.0$ m/s
- 20x20_M60, $U_\infty=30.0$ m/s
- 20x20_M140, $U_\infty=20.0$ m/s
- 20x20_M140, $U_\infty=30.0$ m/s
- 20x20_M140, $U_\infty=40.0$ m/s
- △ 30x30_M50, $U_\infty=20.0$ m/s
- △ 30x30_M130, $U_\infty=20.0$ m/s
- △ 30x30_M130, $U_\infty=30.0$ m/s
- △ 30x30_M130, $U_\infty=40.0$ m/s
- △ 40x40_M120, $U_\infty=30.0$ m/s
- △ 40x40_M120, $U_\infty=20.0$ m/s
- △ 40x40_M120, $U_\infty=25.0$ m/s

- Integral length scales in span (y) and vertical (z) directions.
- $L_{u'u'}$ and $L_{v'v'}$:
 - M60 and M50 produce equal length scales in both direction.
 - Larger spaced grids are more spread.
- $L_{w'w'}$:
 - No agreement with the diagonal line
 - Turbulence grid produces an approximate of isotropic turbulence [1]
- Alteration of the bar spacings to better approximate isotropy or induce more anisotropy

[1] Comte-Bellot and Corssin, 1966, The use of contraction to Improve the Isotropy of Grid-Generated Turbulence JFM 25(4): 657-682

Conclusions



- The effects of turbulence grid in an open-jet wind tunnel was evaluated experimentally and numerically.
- Grid configuration varies the resulting inflow turbulence
 - Equal bar sizes with larger spacings ($\sim 2x$) reduces the blockage ratio but increases turbulence intensity.
 - Increasing the bar size increases the blockage ratio and turbulence intensity
- The present study allows for the optimization of grid designs for wind energy applications.

Perspectives:

- Numerical simulation of the empty tunnel
- Analysis of leading-edge noise measurements
- Simulation of leading-edge noise
- Characterize the turbulence from WiValdi Research Wind Park at Krummendeich

Impressum



Thema: Characterizing Airflow Turbulence in the Acoustic Wind Tunnel Braunschweig (AWB) using Turbulence Grids

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Integral Length Scale



$$L_{u'_i u'_i}(x_j) = \int_0^\infty R_{u'_i u'_i}(r) dr,$$

$$R_{u'_i u'_i}(r) = \langle u'_i(x, t) u'_i(x + r, t + \tau_m) \rangle$$

$$R_{u'_i u'_i}(\tau_m) = \max(R_{u'_i u'_i}(\tau))$$

$$R_{u'_i u'_i}(\tau) = \langle u'_i(x, t) u'_i(x + r, t + \tau) \rangle$$

- 20x20_M60
- △ 30x30_M50
- 20x20_M140
- ▷ 30x30_M130
- △ 40x40_M120

