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German Aerospace Center



HVG-DGG
Service und Forschung für die Glasherstellung



POWER-TO-X FOR SUSTAINABLE GLASS PRODUCTION (SYN-METHANE, SYN-MEOH, AND DIRECT H₂ COMBUSTION) A TECHNO-ECONOMIC AND LIFE CYCLE ASSESSMENT

Project Glas-CO₂: Carbon Capture and Utilization Cycles for a CO₂ Neutral Glass Production
KlimPro BMBF 01LJ2005 (A+B)

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GEFÖRDERT VOM



Bundesministerium
für Bildung
und Forschung

Background



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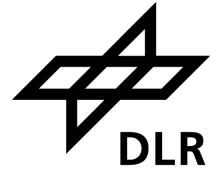


Fig.1: Global CO₂ emissions 1970–2023 ^[1]

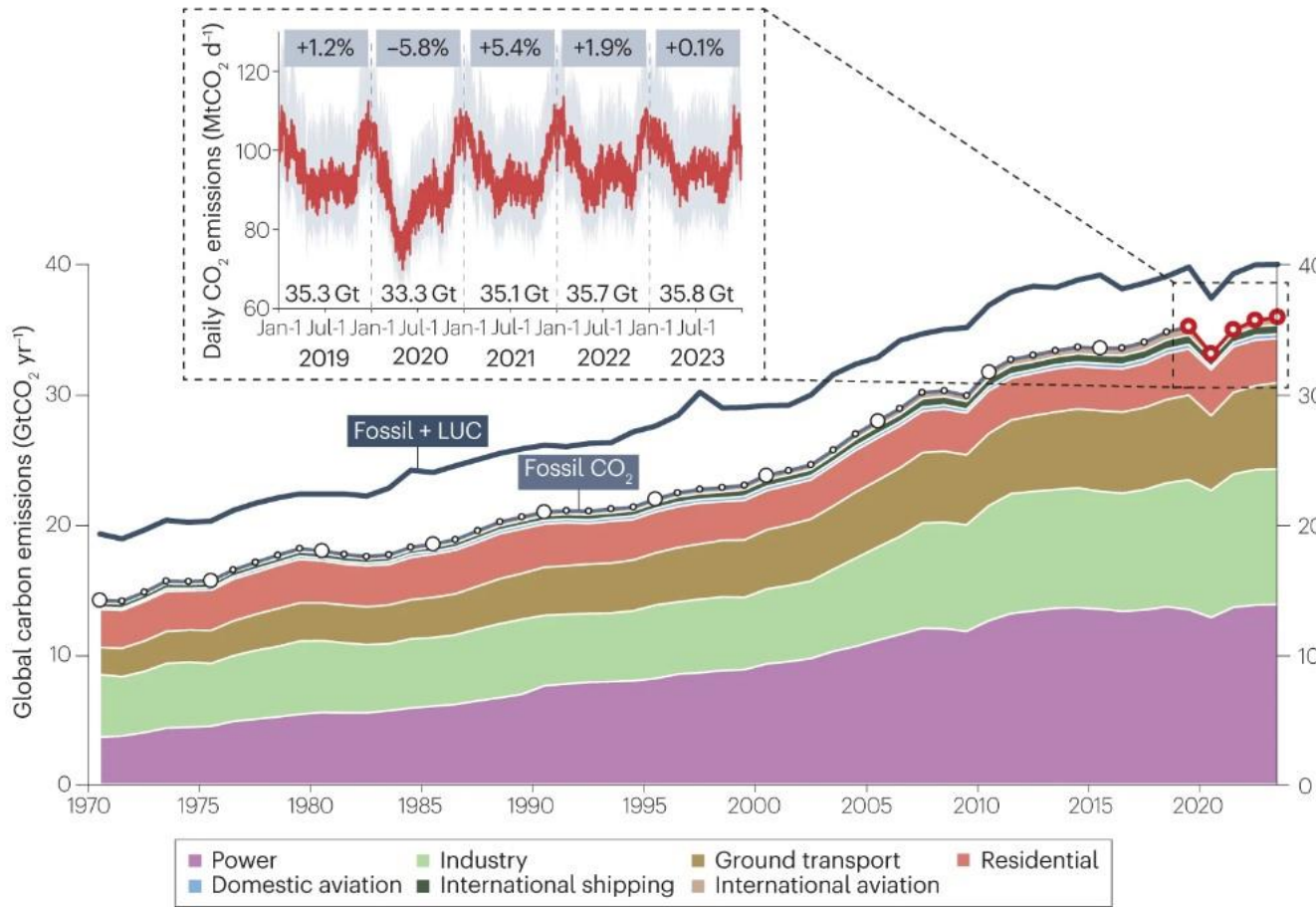


Fig.2: German climate neutrality goal ^[2]

Germany to achieve climate neutrality earlier

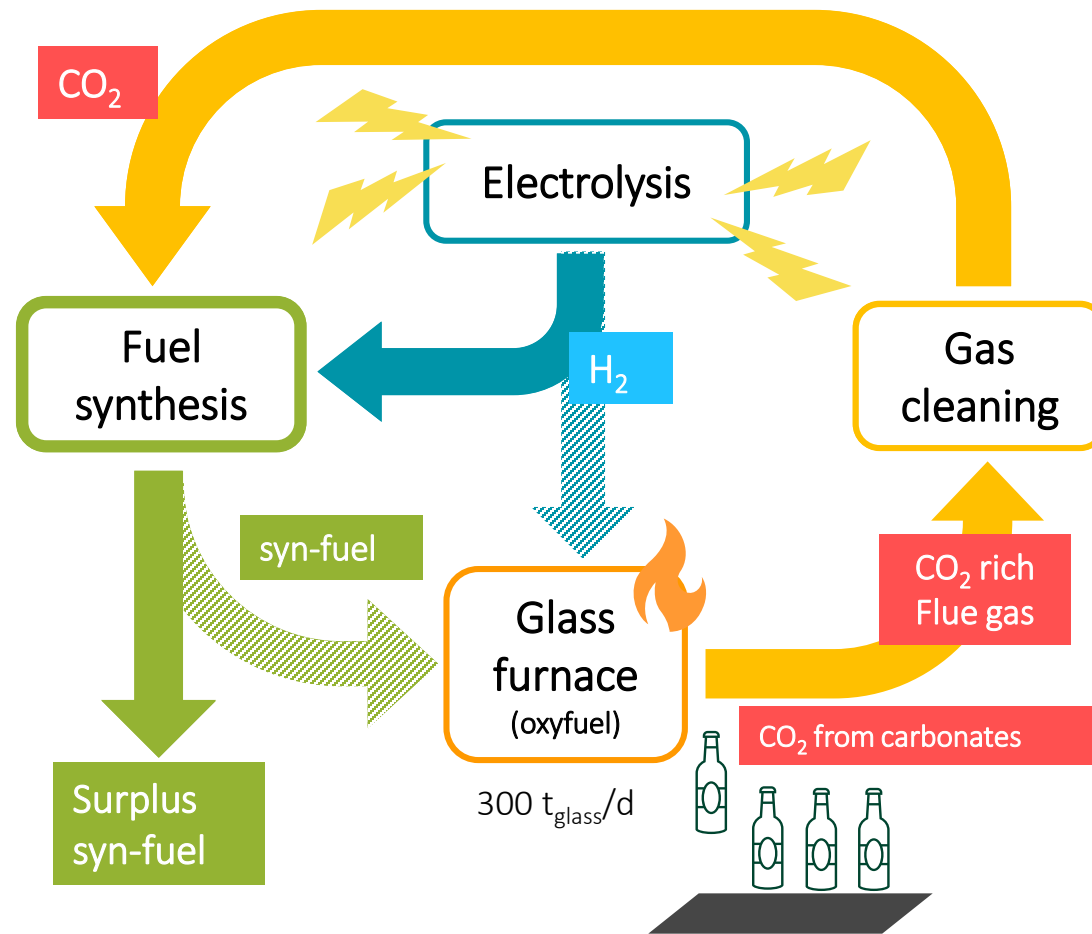
- Greenhouse gas emissions
 - By 2030: 65% less CO₂ (current target 55%)
 - By 2040: 88% less CO₂
 - 2045: Climate neutrality (current target 2050)
- Permissible annual CO₂ emissions for individual sectors such as energy, industry, transport and buildings to be reduced.

[1] <https://www.nature.com/articles/s43017-024-00532-2>

[2] [Climate Change Act - climate neutrality by 2045 \(bundesregierung.de\)](https://www.bundesregierung.de/breg-de/themen/klimaschutz/klimaschutzgesetz)

Background

Challenge: Glass furnace journey (campaign)
15 years with 24/7 operation



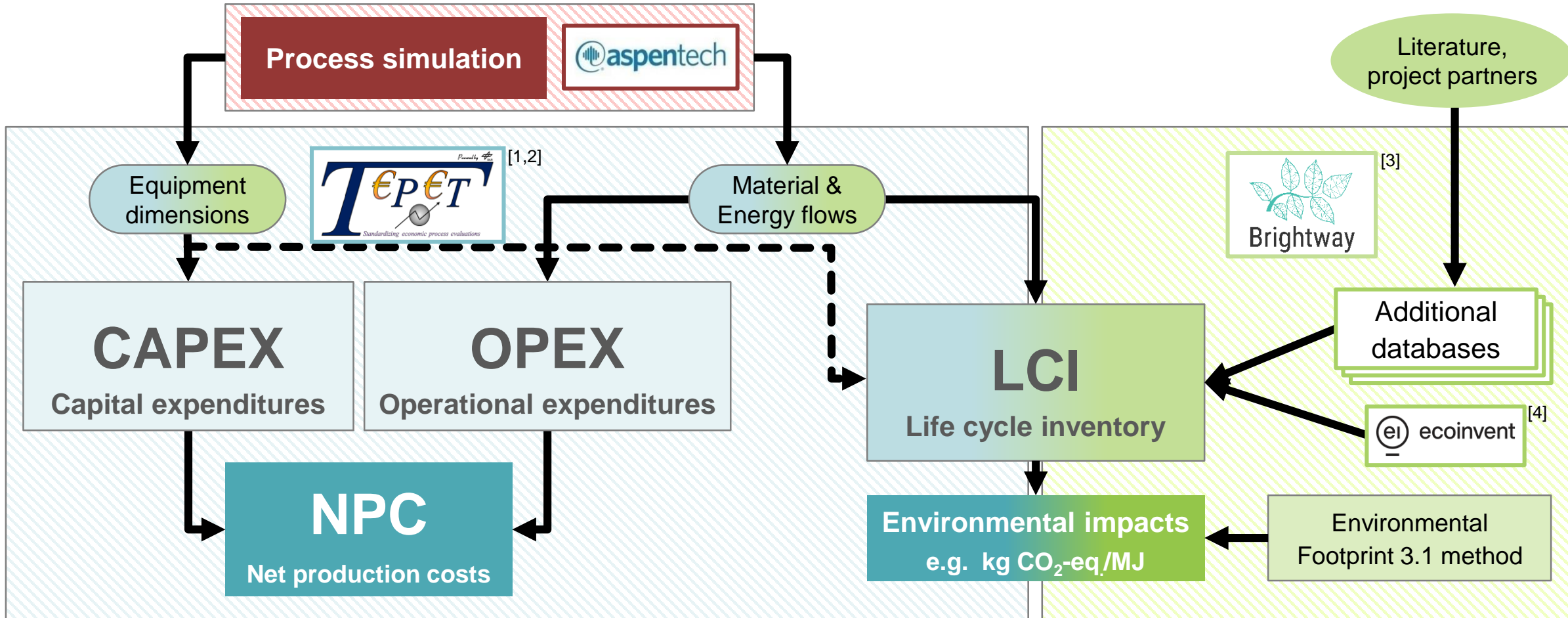
- Power-to-X: alternative to full electrification
 - only 60-80 % electrification possible (hybrid)
- Valorization difficult-to-avoid CO₂ from carbonates

 4.2 Mt CO₂ → 1 Mt CO₂

Case	Gas cleaning	Heating fuel	Surplus
SNG/SNG	✓	SNG	SNG
MeOH/MeOH	✓	Syn-MeOH	Syn-MeOH
H ₂ /SNG	✓	H ₂	SNG
H ₂ /MeOH	✓	H ₂	Syn-MeOH
H ₂ /CO ₂	N/A	H ₂	CO ₂

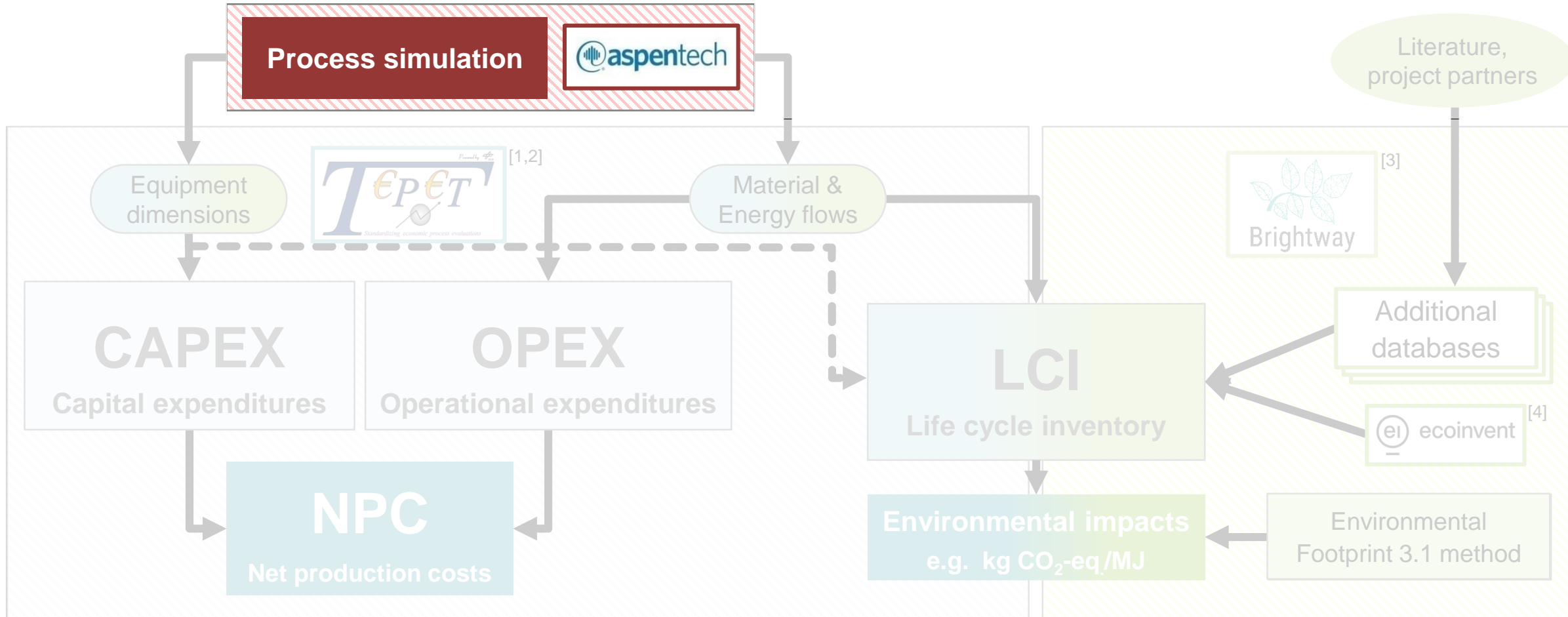
Methodology

Techno-economic (TEA) and life cycle assessment (LCA)



[1] Albrecht et al. (2016): <https://doi.org/10.1016/j.fuel.2016.12.003>
[2] Maier et al. (2021): <https://doi.org/10.1016/j.enconman.2021.114651>
[3] Mutel (2017): <https://doi.org/10.21105/joss.00236>
[4] Wernet et al. (2016): <https://doi.org/10.1007/s11367-016-1087-8>

Process description



[1] Albrecht et al. (2016): <https://doi.org/10.1016/j.fuel.2016.12.003>
[2] Maier et al. (2021): <https://doi.org/10.1016/j.enconman.2021.114651>
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Process description

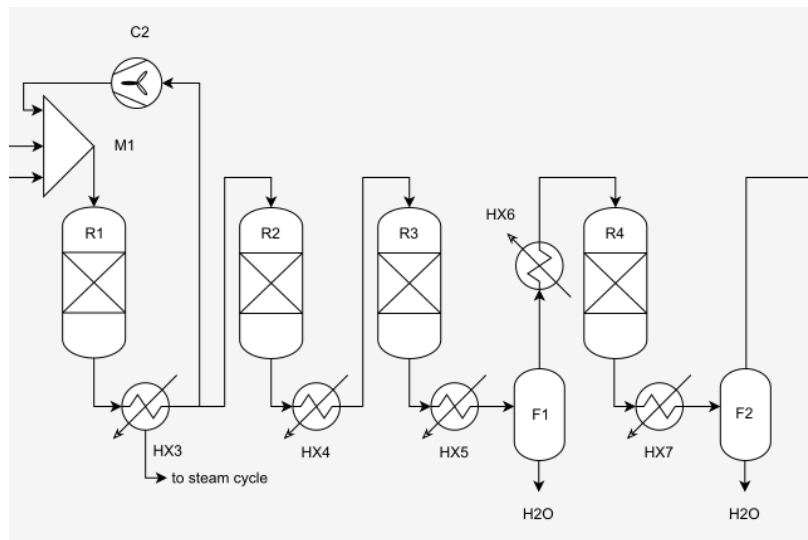
Reactor design and parameters: SNG



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TREMP™ reactor design^[1]: high energetic efficiency & steam cycle applicable



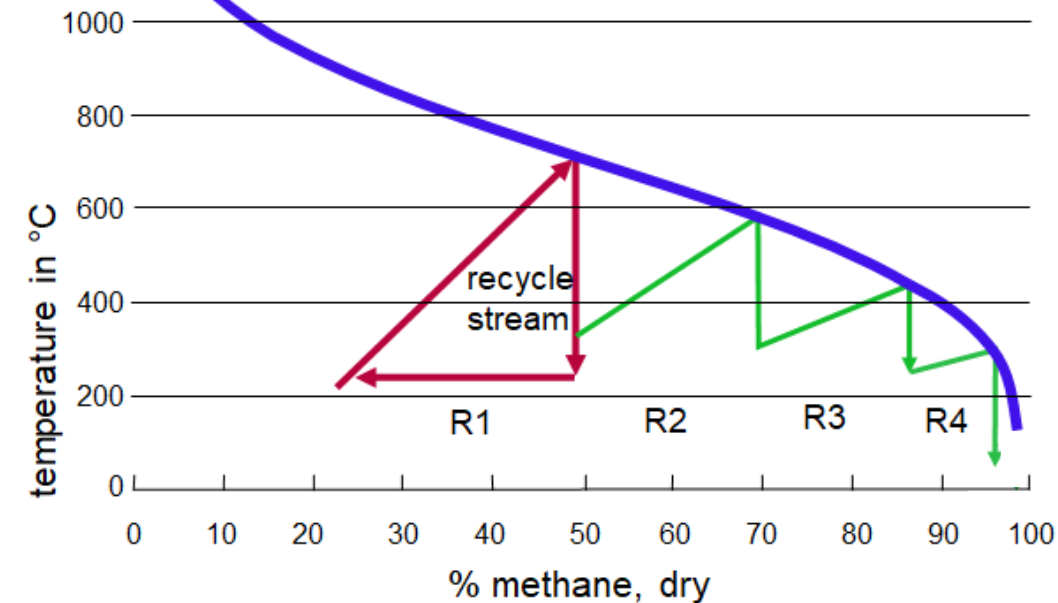
AspenPlus® model: RPlug

$T_{\max,R1}^{[3]} = 700 \text{ °C}$

$T_{\text{in},R1} = 250 \text{ °C}$

$p^{[2]} = 20\text{-}30 \text{ bar}$

$GHSV^{[2]} = 4200\text{-}8900$



Kinetic model: Rönsch et al.^[3-5]

Combination of WGS and CO-Methanation

Catalyst^[2] MCR-2X (Ni-based)

→ Gas cleaning required

[1] Topsøe, H., From coal to clean energy. 2011

[2] in range of: Harms, H., B. Höhle, and A. Skov, 1980, Methanisierung kohlenmonoxidreicher Gase beim Energie-Transport.

[3] Röscher et al., 2016, Review on methanation – From fundamentals to current projects.

[4] Klose, J., 1984, Kinetics of the methanation of carbon monoxide on an alumina-supported nickel catalyst. Journal of Catalysis

[5] Zhang, J., et al., 2013, Kinetic investigation of carbon monoxide hydrogenation under realistic conditions of methanation of biomass derived syngas

[6] Meylan et al., 2016, Material constraints related to storage of future European renewable electricity surpluses with CO2 methanation

Process description

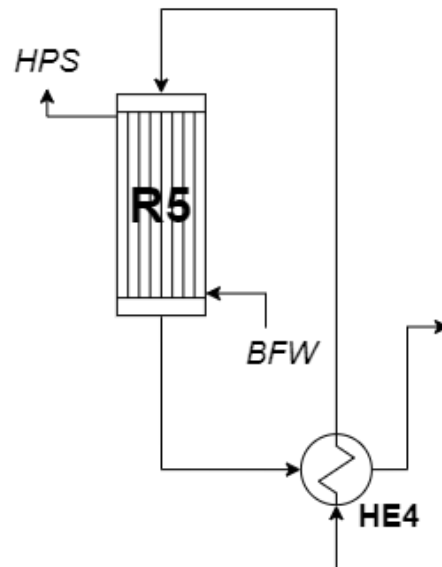
Reactor design and parameters: Syn-MeOH



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Lurgi reactor design^[2]: high energetic efficiency & steam generation applicable



AspenPlus® model^[1]: RPlug

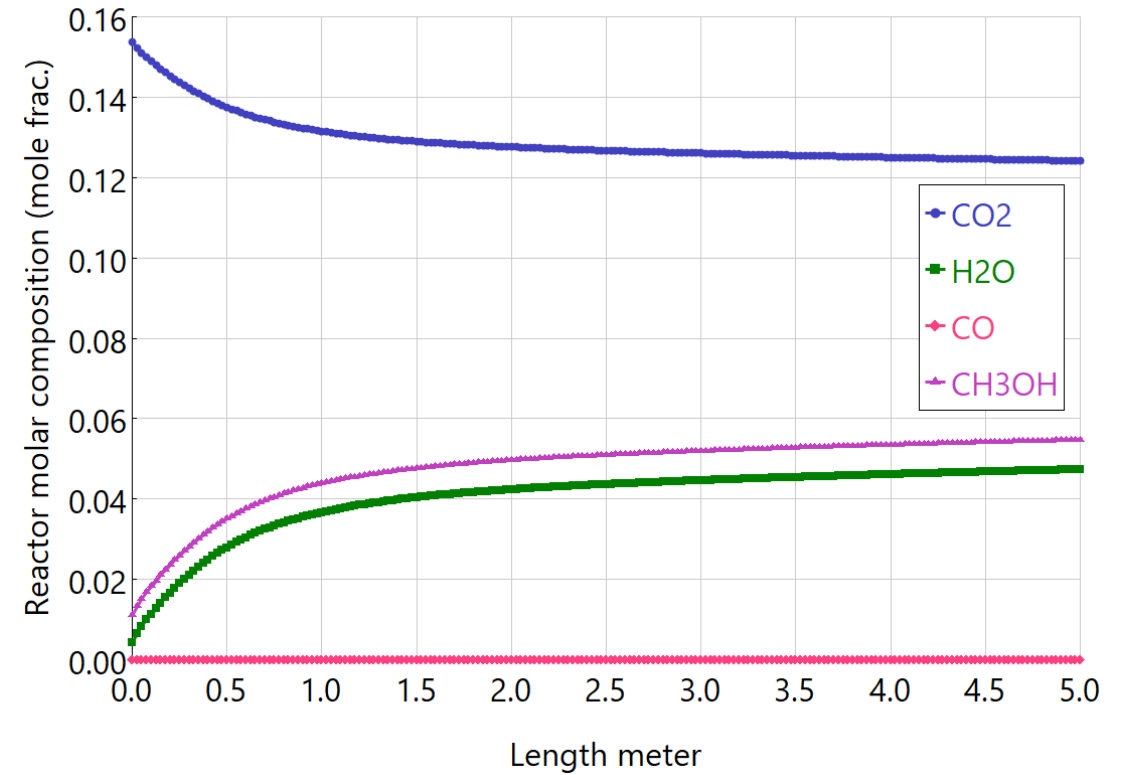
$T_{\max,R1}^{[2,5]} = 280-300\text{ °C}$

$T_{\text{in},R1}^{[1]} = 230\text{ °C}$

$p^{[1,2]} = 80\text{ bar}$

Catalyst^[3] Cu/ZnO/Al₂O₃

→ Gas cleaning required



Kinetic model: Vanden Bussche and Froment^[1,3]

MeOH synthesis from CO/CO₂/H₂ represented as CO₂ hydrogenation & RWGS reactions

[1] Rahmat et al. (2023) Techno-economic and exergy analysis of e-MeOH production <https://doi.org/10.1016/j.apenergy.2023.121738>

[2] Metallgesellschaft AG (1996) – EP 0 790 226 B1

[3] Van-Dal and Bouallou (2013) Design and simulation of a methanol plant from CO₂ hydrogenation

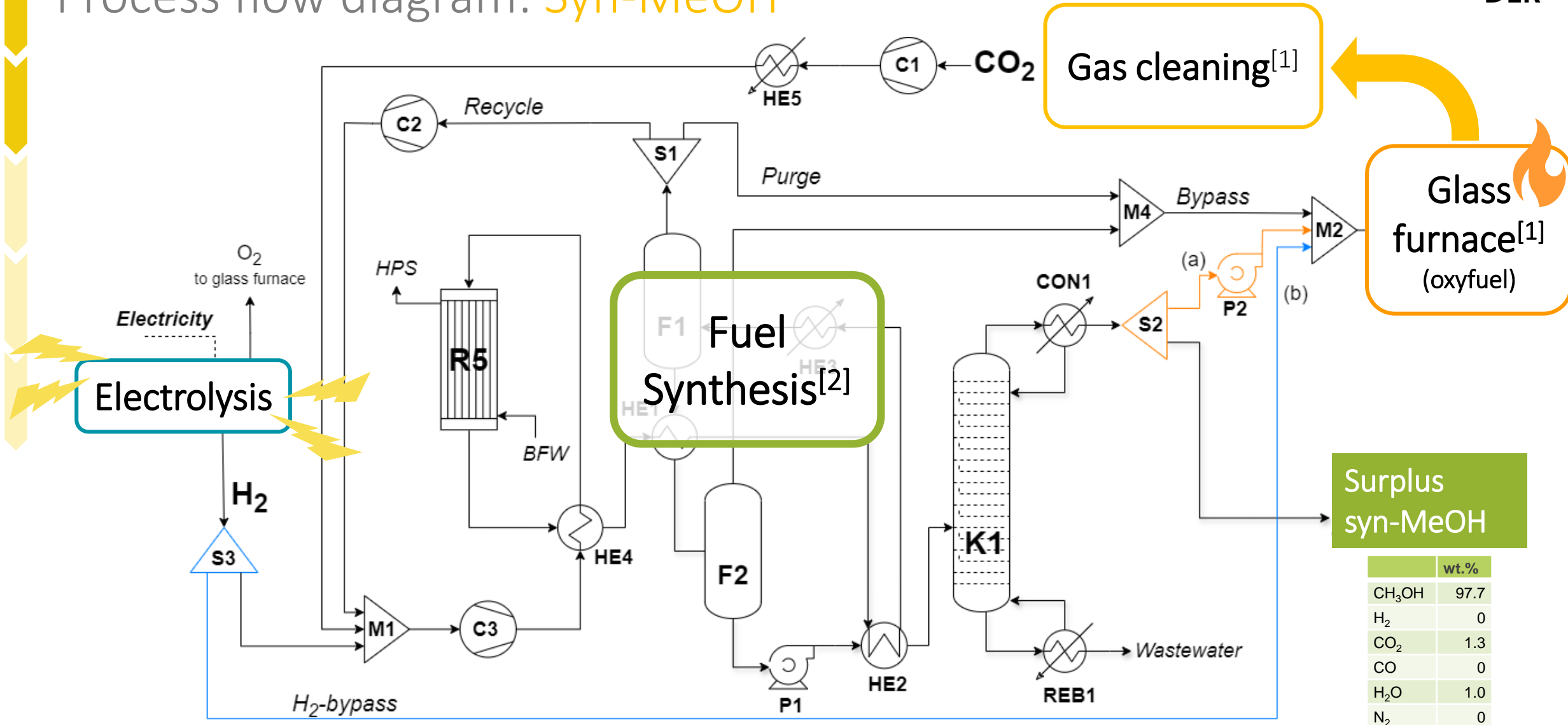
[4] Bartholomew and Farrauto (2006) Fundamentals of Industrial Catalytic Processes, 2. Ed.

Process description

Process flow diagram: Syn-MeOH



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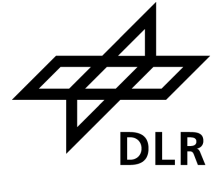


Process description

Equipment design and parameters



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Equipment ^[1-3]	AspenPlus® model	Parameters	Remarks
Heat exchangers	HeatX/Heater	$\Delta p = 0.2 \text{ bar}^{[4]}$, $\Delta T_{\text{approach}} = 10 \text{ K}^{[4]}$	U-values ^[5] method
Compressors	Compr/MCompr	Max. CR = 3 ^[4] $\eta_{\text{isentropic}} = 80 \%^{[4]}$, $\eta_{\text{mech.}} = 95 \%$	range CR = 2.5-4 ^[4]
Pumps	Pump	$\eta_{\text{pump}} = 95 \%$, $\eta_{\text{driver}} = 95 \%$	
Flash drums	Flash2	$Q = 0 \text{ kW}$, $\Delta p = 0.2 \text{ bar}^{[4]}$	adiabatic
Distillation columns	RadFrac	$p_{\text{cond.}} = 1.36 \text{ bar}^{[1]}$, $\Delta p_{\text{col.}} = 0.34 \text{ bar}^{[1]}$ $n_{\text{stage}} = 55$, reflux ratio = 1	$d_{\text{col.}} = f(\dot{V}_{\text{gas,col.}})^{[6]}$
Electrolyzer AEL	RStoic (Stack) Flash2, Sep, Pump (BoP)	$\eta_{\text{energetic}} = 53.3 \% \text{ (LHV)}^{[2]}$	simplified model
Wet scrubber (limestone)	Flash2, Sep	100 % separation of SO ₂ , SO ₃ , HCl, HF	black-box
Membrane PMP	Sep	N ₂ separation = 92.75 % ^[8]	black-box

[1] Rahmat et al. (2023) Techno-economic and exergy analysis of e-MeOH production <https://doi.org/10.1016/j.apenergy.2023.121738>

[2] Sánchez et al. (2020) Aspen Plus model of an alkaline electrolysis system for hydrogen production. <https://doi.org/10.1016/j.ijhydene.2019.12.027>

[3] Heimann, N. et al (2023), Standardized tea of sCNG and HCNG, to be submitted

[4] Woods (2007) Rules of Thumb in Engineering Practices

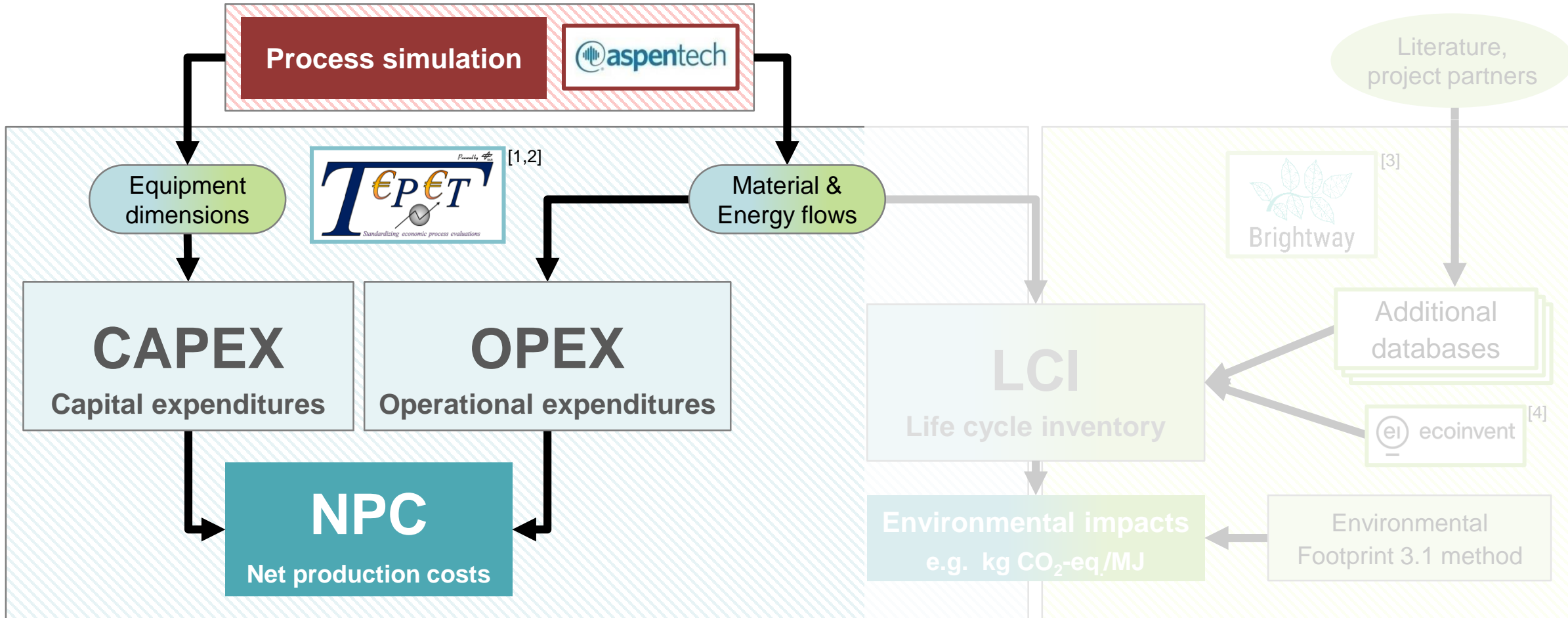
[5] VDI-Gesellschaft (2006) VDI-Wärmeatlas. [978-3-540-32218-4_13.pdf \(springer.com\)](https://doi.org/10.1002/vdi13)

[6] Towler (2008) Chemical Engineering Design

[7] Sorrels (2021) Chapter 1 – Wet and Dry Scrubbers for Acid Gas Control. www.epa.gov

[8] Samei and Raisi (2022) Separation of nitrogen from methane by multi-stage membrane

Techno-economic assessment (TEA)



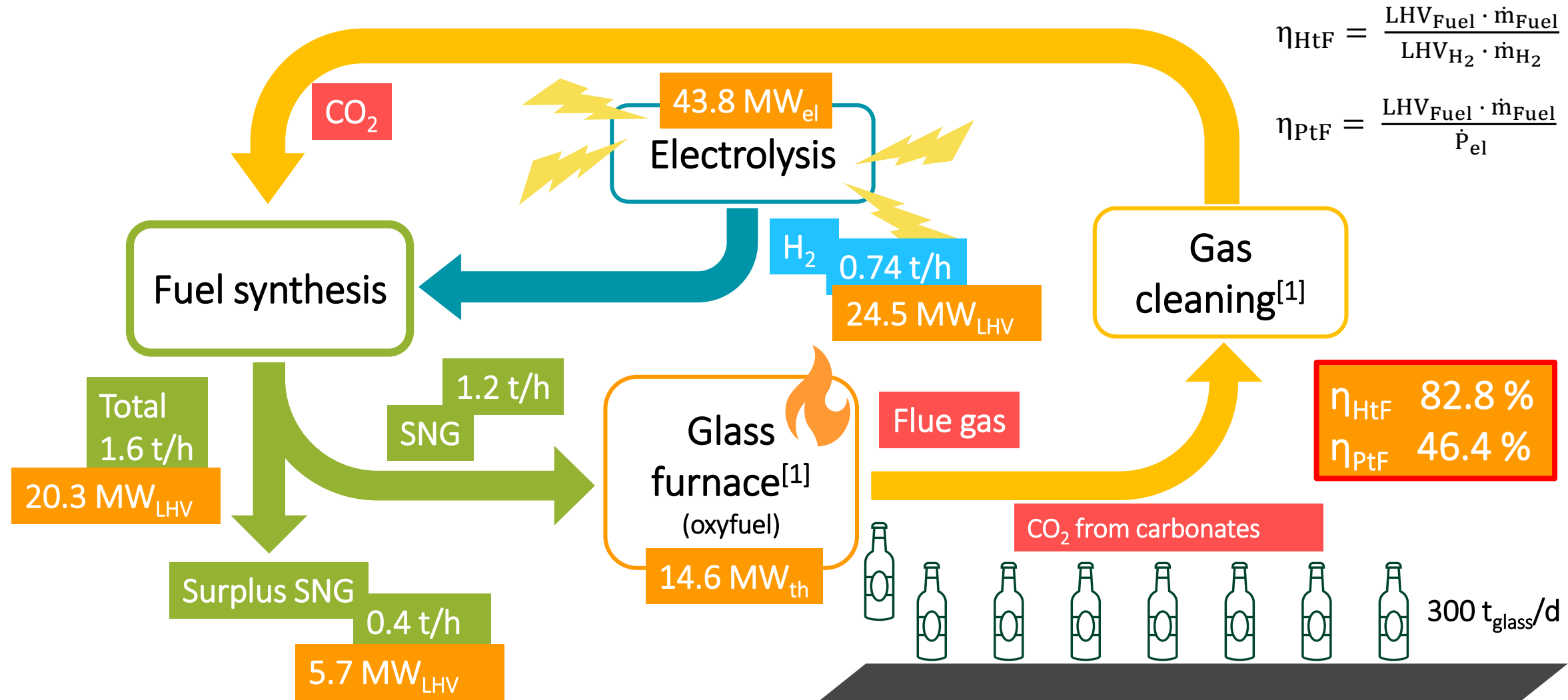
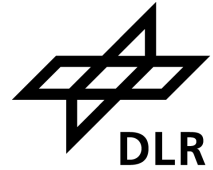
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 [3] Mutel (2017): <https://doi.org/10.21105/joss.00236>
 [4] Wernet et al. (2016): <https://doi.org/10.1007/s11367-016-1087-8>

Techno-economic assessment (TEA)

Efficiencies: SNG/SNG



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$$\eta_{HtF} = \frac{LHV_{Fuel} \cdot \dot{m}_{Fuel}}{LHV_{H_2} \cdot \dot{m}_{H_2}}$$

$$\eta_{PtF} = \frac{LHV_{Fuel} \cdot \dot{m}_{Fuel}}{\dot{P}_{el}}$$

$$\eta_{HtF} = 82.8\%$$

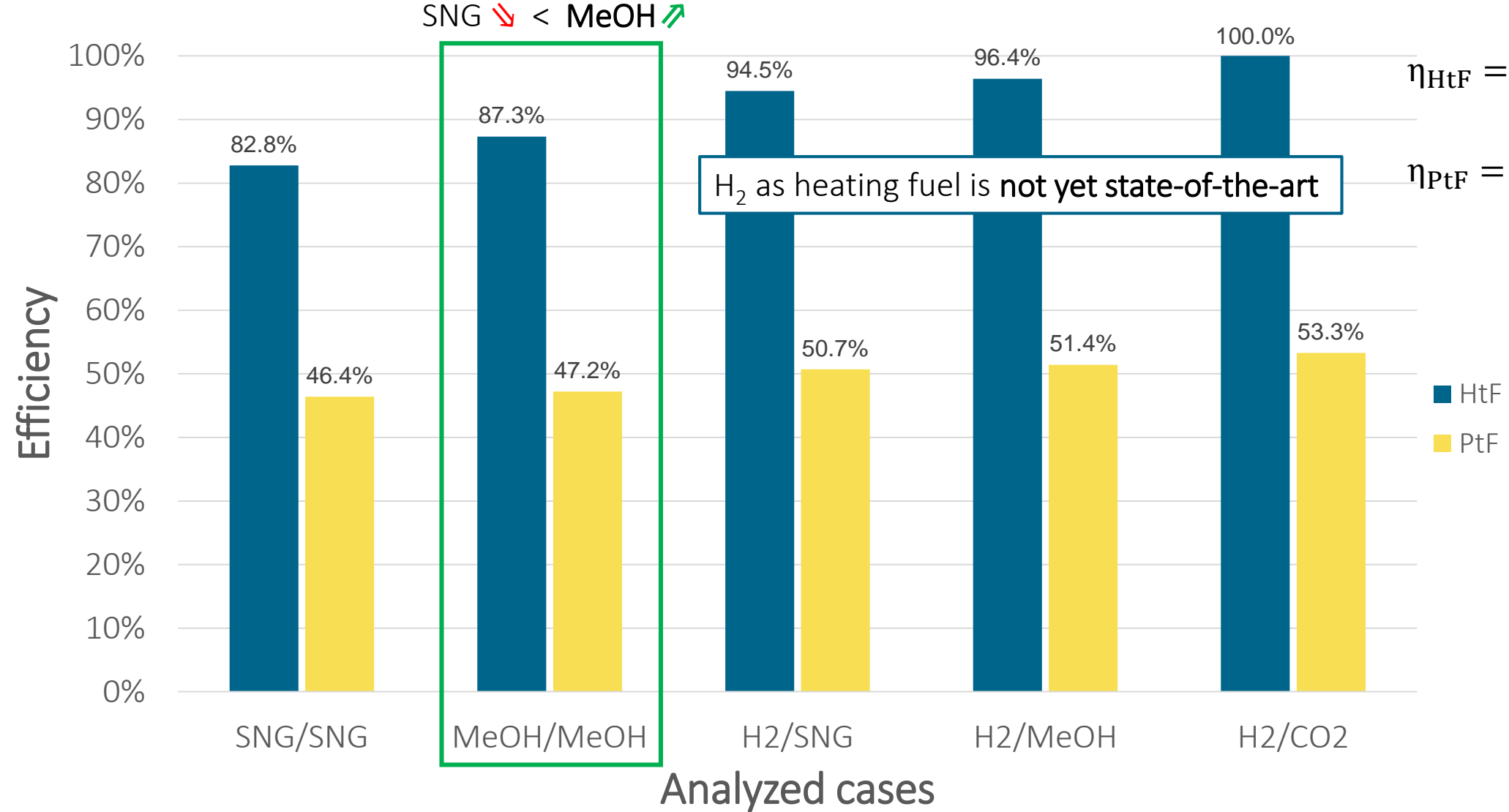
$$\eta_{PtF} = 46.4\%$$

Techno-economic assessment (TEA)

Efficiencies



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$$\eta_{HtF} = \frac{LHV_{Fuel} \cdot \dot{m}_{Fuel}}{LHV_{H_2} \cdot \dot{m}_{H_2}}$$

$$\eta_{PtF} = \frac{LHV_{Fuel} \cdot \dot{m}_{Fuel}}{\dot{P}_{el}}$$

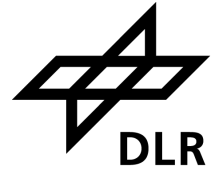
■ HtF
■ PtF

Techno-economic assessment (TEA)

Input – basis conditions & OPEX



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Basis conditions	
Plant location	Germany
Base year	2022
Basis currency	€
Full-load hours	8000 h/a
Plant lifetime (y)	15 a
Interest rate (IR)	7 %
Labor costs	41 €/h

Raw materials	
CO ₂	Flue gas & carbonates
H ₂	AEL electrolysis
Electricity ^[1]	60-250 €/MWh _{el}
Utilities	taken from [2]

$$NPC \left[\frac{\text{€}}{\text{MWh}_{LHV}} \right] = \frac{ACC + \sum OPEX + \text{labor costs}^{[2,3]}}{\dot{m}_{synfuel} * LHV_{synfuel}}$$

$$ACC = FCI * \text{Annuity factor}$$

$$FCI_i = EC_i * \sum CAPEX \text{ cost factors}$$

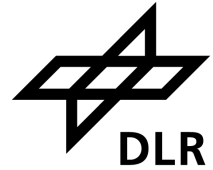
See next slide!

Techno-economic assessment (TEA)

Input – CAPEX cost functions



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$$EC_{i,ref} = EC_{ref} \times \left(\frac{sizing_i}{sizing_{ref}} \right)^n \times \left(\frac{CEPCI_i}{CEPCI_{ref}} \right)$$

$$EC_{i,poly} = \left[e \cdot (sizing_i)^2 + f \cdot sizing_i + g \right] \times \left(\frac{CEPCI_i}{CEPCI_{ref}} \right)$$

Reference function ($EC_{i,ref}$)	EC_{ref}	Currency	$sizing_{ref}$	Unit	n	Year _{ref}	Source
Compressor	3 035	\$	1	kW _{el}	0.68	2002	[1]
Centrifugal pump	16 809	\$	1	m ³ s ⁻¹	0.36	2002	[1]
Distillation column	286 343	\$	100	size factor = HxD ^{1.5} [m ^{2.5}]	0.53	2007	[2,3]
AEL stack	800	k€	0.005	kg/s	1	2019	[4]
AEL balance of plant	1	m€	0.025	kg/s	0.8	2019	[4]
Wet scrubber (limestone)	13 061	k\$	14	MW _{th}	0.72	2012	[5]
Membrane PMP	9.76	m\$	525.6	kmol/h	0.6	2020	[6]**
Methanation fixed-bed reactor	57 794	\$	14 000	m ³ /h	0.52	2007	[2]
Polynomial function ($EC_{i,poly}$)	e	f	g	Sizing unit	Currency	Year _{ref}	Source
MeOH Lurgi reactor, D _{tube} 2 in.*	0	156.03	11 910	Number of tubes [-]	\$	2002	[1]**
Shell & tube heat exchanger*	0	201.29	3853.3	Heat transfer area [m ²]	\$	2002	[1]
Flash drum	-2.21	369.75	805.42	Length & diameter [m]	\$	2002	[1]

*stainless steel as the material construction

**with own reformulation

[1] Peters et al. (2002) *Design and Economics for Chemical Engineers*. Europe: McGraw-Hill Education.

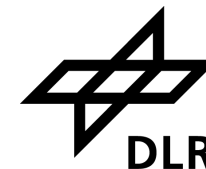
[2] Woods (2007) *Rules of Thumb in Engineering Practices*

[3] Towler (2008) *Chemical Engineering Design*

[4] Habermayer et al. (2023) Sustainable aviation fuel from forestry residue and hydrogen. <https://doi.org/10.1039/d3se00358b>

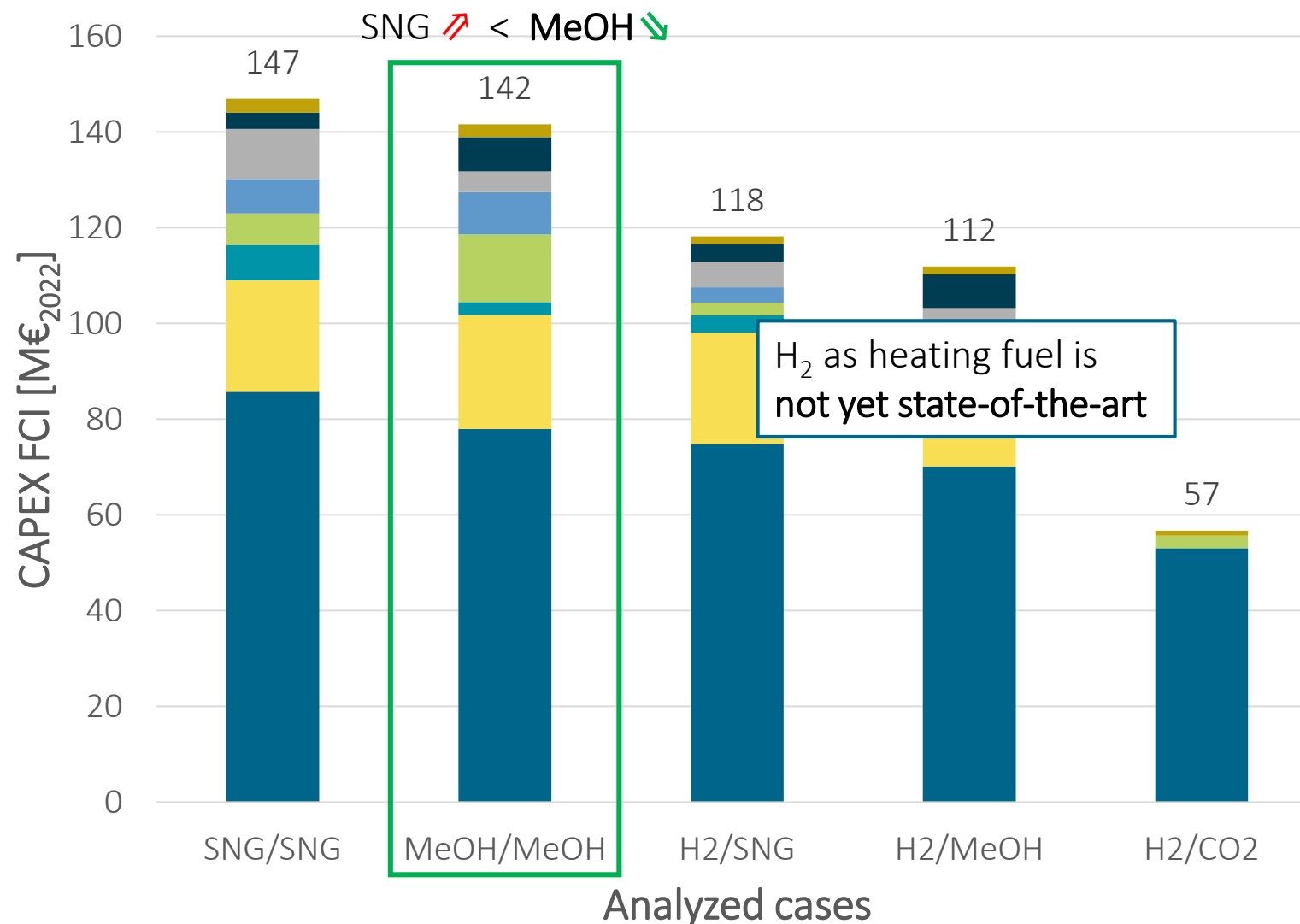
[5] Sorrels (2021) Chapter 1 – Wet and Dry Scrubbers for Acid Gas Control. www.epa.gov

[6] Samei and Raisi (2022) Separation of nitrogen from methane by multi-stage membrane

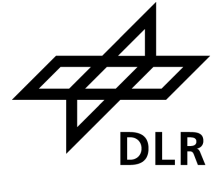


TEA for 12.2 MW_{th} Glass Furnace

Results – CAPEX Fixed Capital Investment (FCI)

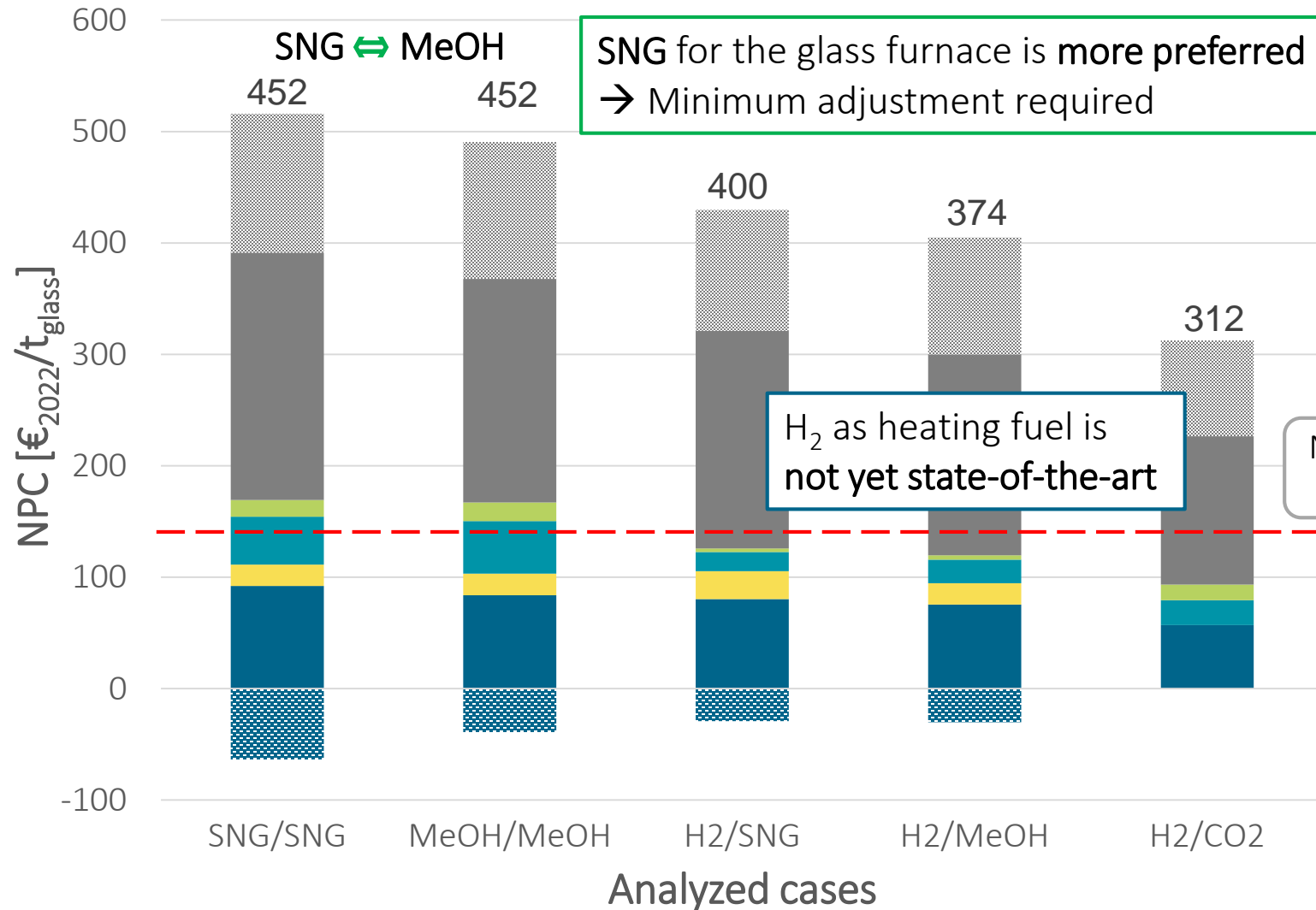


- **AEL:** SNG ↗ requires more H₂ feedstock than MeOH ↘
- **Reactors:**
SNG fixed-bed **multi-stage** ↗
MeOH multi-tube **single-stage** ↘
- **Compressors:**
p_{reactor} SNG **30 bar** ↘
p_{reactor} MeOH **80 bar** ↗
- **Steam cycle:**
SNG in recuperator & reactor
MeOH in recuperator only



TEA for 12.2 MW_{th} Glass Furnace

Results – NPC with electricity price 60 €₂₀₂₂/MWh_{el}



- Sales of surplus syngas as fossil fuels
- Cost driver is H₂ generation
60-67 % NPC

Eco-friendly beer bottle
ca. 26 ct. €₂₀₂₂/bottle

Natural gas costs^[1]
130 €₂₀₂₂/t_{glass}

Beer bottle (330 g) price
up to 15 ct. €₂₀₂₂/bottle^[2]

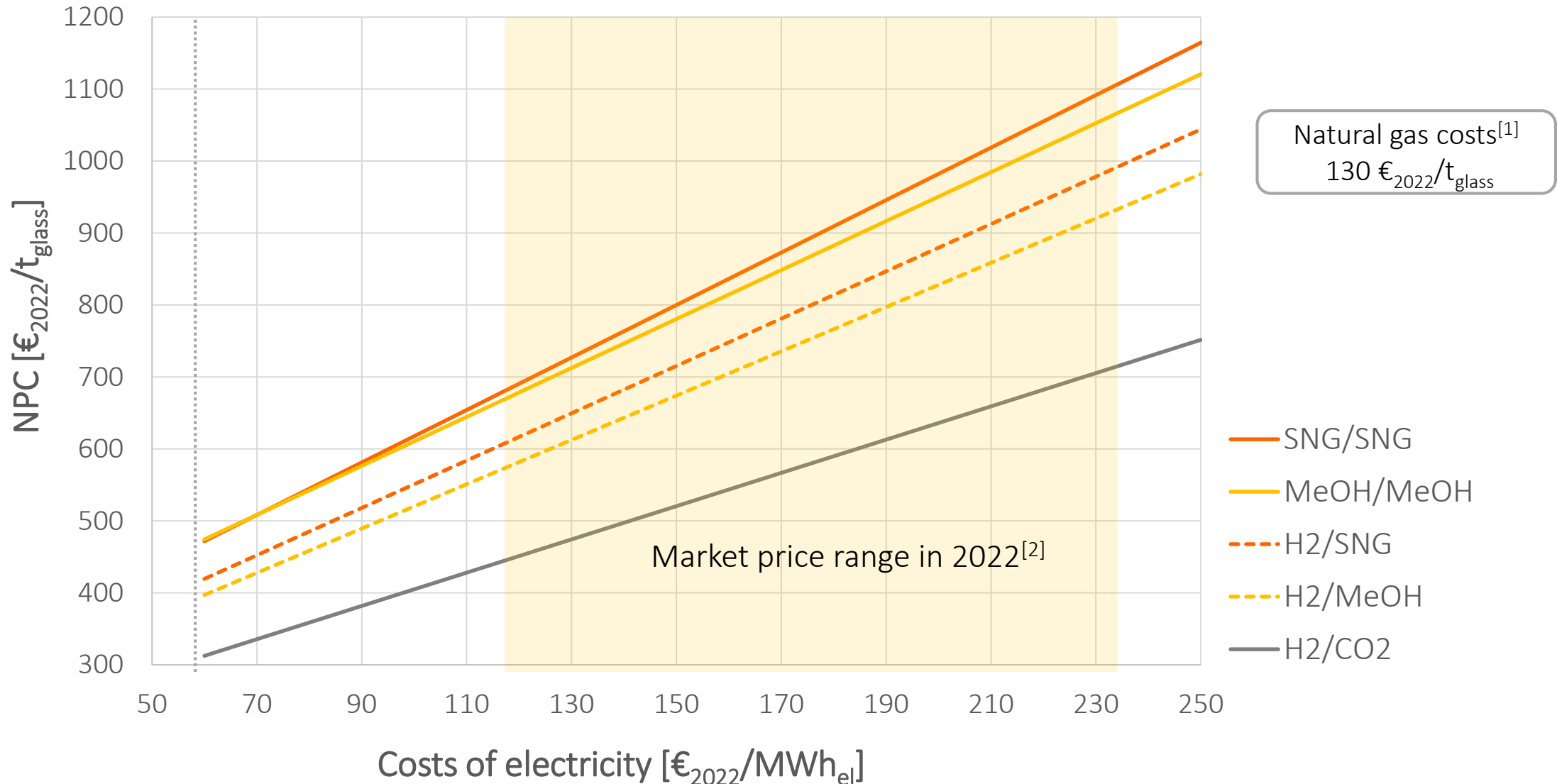
- By-products (sold)
- Indirect costs
- Electricity
- Remaining OPEX
- Remaining FCI
- Wet scrubber & membrane
- AEL electrolyzer

Techno-economic assessment (TEA)

Results – NPC sensitivity analysis

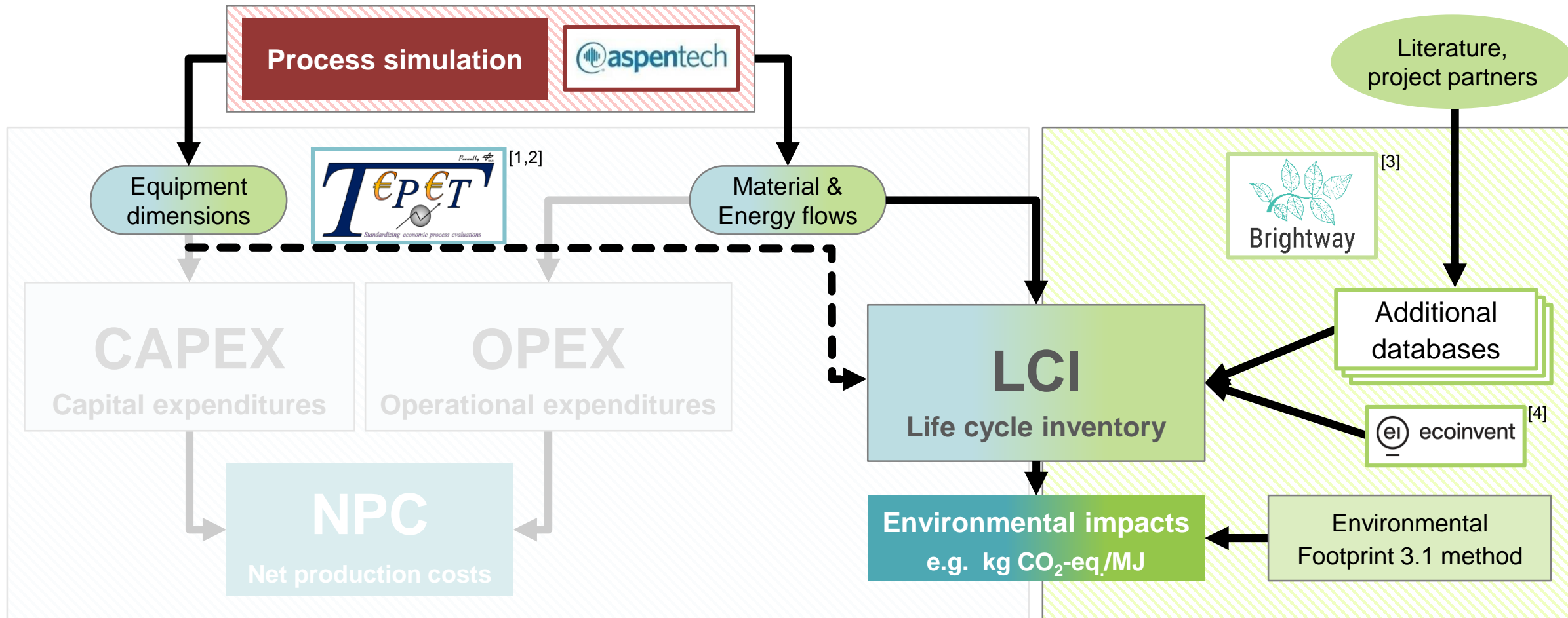


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Life cycle assessment (LCA)

Functional unit: 1 tonne glass produced



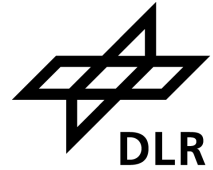
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LCA results (preliminary)

SNG/SNG vs MeOH/MeOH vs H₂/CO₂

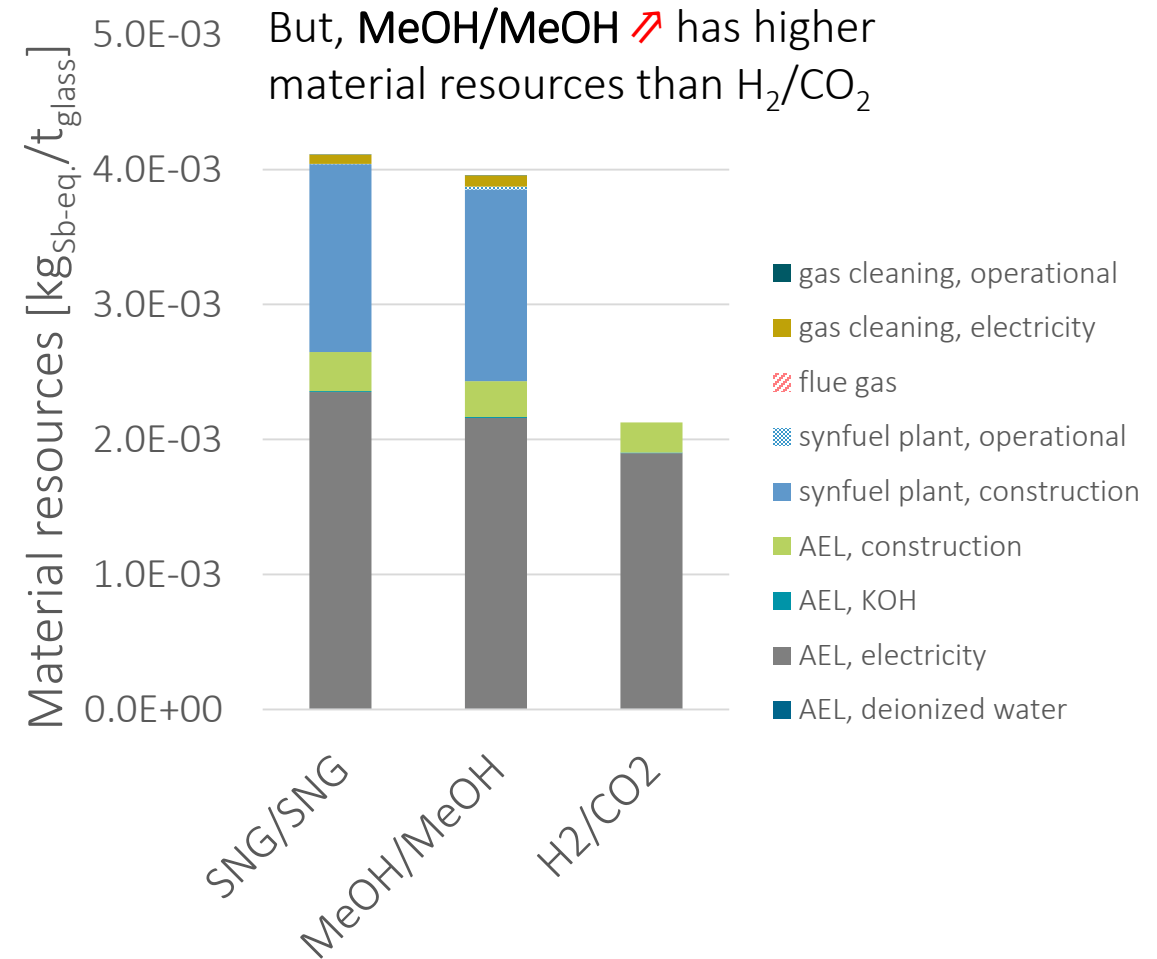
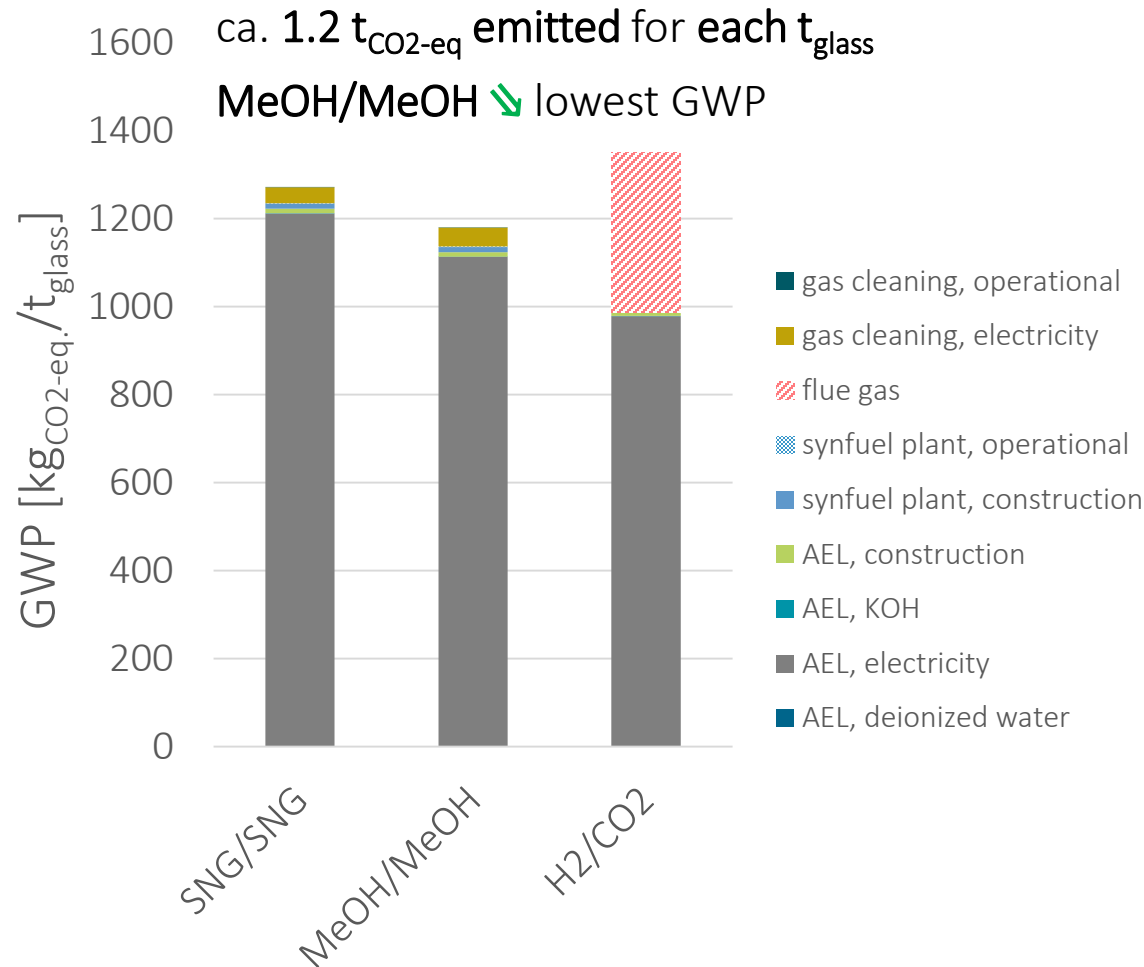


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Functional unit: 1 tonne glass produced

German grid electricity as the el. source



Conclusion



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- Implementation of Power-to-X concepts for a sustainable industrial glass production
→ Example for industry decarbonization
- Glass industry can be **sustainable**, depending on the electricity source
→ **Case SNG/SNG** is the most suitable as direct substitution for natural gas
- Glass furnace requires adjustments for direct H₂ combustion
- CCU is **theoretically applicable**
→ Practical tests must be conducted
- **Eco-friendly container glass** (beer bottle) would cost **almost twice** of the current price
→ depending on the electricity costs
- **Preliminary LCA** shows good potential of the PtX concepts, however a trade-off is expected, e.g. material resources impact

Realization = f(user-acceptance)
Industry? Market?



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THANK YOU FOR YOUR ATTENTION!

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