



“Green propellants” as a hydrazine substitute: experimental investigations of ethane/ethene-nitrous oxide mixtures and validation of detailed reaction mechanism

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Abstract

Mixtures of hydrocarbons and nitrous oxide are known as green propellants and could replace the highly toxic hydrazine and hydrazine derivatives as rocket fuel, since they are non-toxic and easier to handle, but still have a high specific impulse. Possible hydrocarbon candidates are ethane or ethene. To check the applicability of the two reaction systems, C_2H_6/N_2O and C_2H_4/N_2O , experiments are a prerequisite for accurate predictions under various conditions that are of great importance for the design of safe and reliable thrusters. Therefore, experimental literature data obtained from ignition delay times and laminar burning velocities were used to validate and optimize a new reaction mechanism, which is designed for C_0 – C_3 and nitrogen oxides formation. To achieve a better predictive power of the detailed mechanism, the Arrhenius parameters of three reactions were adjusted: $N_2O + H \rightleftharpoons N_2 + OH$, $N_2O (+M) \rightleftharpoons N_2 + O (+M)$, and $NH + NO \rightleftharpoons N_2O + H$. A good agreement was achieved between simulation and experiment for ignition delay times at various pressures and equivalence ratios in a broad temperature range before and after the mechanism optimization. However, the laminar burning velocities in the whole measured range of the equivalence ratio for all pressures and dilutions showed a significant improvement after the optimization.

Keywords Chemical kinetics · Mechanism optimization · Laminar burning velocity · Ignition delay time · Nitrous oxide · Green propellants

1 Introduction

With its long-term stability and high specific impulse, hydrazine is an ideal storable rocket fuel for occasionally required propulsion applications, like attitude control systems for satellites. Hydrazine derivatives like monomethyl hydrazine (MMH) and unsymmetrical dimethyl hydrazine (UDMH) are used for rocket propulsion applications in various technological contexts. All of these fuels have the same disadvantages in handling: they are highly toxic and carcinogenic [1]. In 2011, hydrazine was included in the list of “substances of very high concern” by the framework

legislation of the European Commission for the Registration, Evaluation, Authorization and Restriction of Chemicals (REACH) [2]. Due to possible restrictions, the use of hydrazine will become expensive and impractical on short to medium notice. At given moment, several tons of hydrazine are still consumed annually in European space activities. The DLR Future Fuels initiative is investigating so-called green propellants as hydrazine alternatives [3, 4]. High potential candidates are hydrocarbon-nitrous oxide mixtures, since they are less or non-toxic, have a high specific impulse, and are less expensive. However, higher flame temperatures and the increased risk of flashbacks in premixed propulsion systems lead to specific design requirements for new satellite in-space propulsion thrusters [5, 6]. Numerical CFD approaches are commonly used to find the ideal geometry. For this, a precise knowledge of combustion chemistry is required.

Mixtures of hydrocarbons and nitrous oxide get into the focus of science in the latest years. Besides the DLR, research programs in the US initiated by the Defense Advanced Research Projects Agency (DARPA) [7] are

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investigating such mixtures, especially C_2H_2/N_2O [8] and C_3H_8/N_2O [9]. In 2009, Mungas et al. [10, 11] started testing mixtures in thrusters with ethane, ethene, or ethyne with nitrous oxides. Various studies on the detailed chemical kinetics have been conducted in the past. Powell et al. used laminar burning velocities for optimizing the chemical kinetic mechanism [12], as well as flame structure measurements, flow reactor data, and shock tube ignition delay data [13]. Mathieu et al. [14] developed a detailed C_1/NO_x model which predicts the influence of N_2O on the ignition of methane. In 2019, Wang and Zhang [15] published a mechanism for predicting laminar burning velocities of hydrocarbon/ N_2O flames, especially for C_2H_4 , but also tested for experimental data from Powell et al. [12] (CH_4 , C_2H_2 , C_3H_8) and Naumann et al. [16] (C_2H_4).

This contribution reports on the validation and optimization of a detailed reaction mechanism for ethane- or ethene-nitrous oxide reaction systems (C_2H_6/N_2O or C_2H_4/N_2O). Experimental data from literature of two global combustion parameters, laminar burning velocity and ignition delay time, were used for the validation and optimization [17–20]. Furthermore, sensitivity analyses and the resulting implications to reaction kinetics of nitrogen-containing species are investigated to evaluate the predictive potential of the mechanism. In future work, this detailed optimized mechanism serves as the basis for a reduced mechanism, which should be used in CFD simulations.

2 Experimental data

All experiments shown here were carried out at the DLR Institute of Combustion Technology in Stuttgart, Germany. Ignition delay times have been measured behind reflected shock waves at the shock tube facility for both reaction systems, C_2H_4/N_2O and C_2H_6/N_2O . The results and details about the experiments and the construction of the devices were published in 2017 [17], 2019 [18], and 2020 [19]. The shock tube used is divided by aluminum diaphragms into the high-pressure driver section and the low-pressure driven section. The driven section was filled with small quantities of the homogenized mixtures at equivalence ratios $\varphi = 1.0$ and 2.0, diluted 1:5 with nitrogen; the driver section was loaded with mixtures of helium and argon. After diaphragm rupture, a shock wave propagates through the reaction mixture and eventually becomes reflected at the end plate. The temperature and pressure directly behind the reflected shock wave were computed from the incident shock velocity measured by piezoelectric pressure gages. The temperature range examined was approximately 1100–2000 K, at initial pressures of $p = 1, 4, \text{ and } 16$ bar, respectively. Ignition was observed by the detection of photon emission from excited CH(A) at 431 nm with photomultipliers. Ignition delay time

values shown in this paper were determined by the occurrence of the first CH(A) maximum after the initiation of the reactive system by the reflected shock wave.

Laminar burning velocities have been measured with a high-pressure burner system using the cone angle method. The experimental setup consists of the burner housing with the pressure control system, the exhaust gas heat exchanger, the ignition system, and the flame holder. For all experiments, the flame holder is heated up to 473 K and the dilution with nitrogen was 50%. The reaction system C_2H_4/N_2O has been measured between equivalence ratios $\varphi = 0.6$ and 1.8 at pressures $p = 1$ and 3 bar by Kick et al. [17] and at $p = 6$ bar by Richter et al. [20]. The reaction system C_2H_6/N_2O was examined under the same conditions as C_2H_4/N_2O [20]. Also, the influence of heat transfer to the flame holder was tested at $p = 1$ bar varying the dilution (40% and 60%). For the evaluation, digital images of the conical flames were captured by a CCD camera in combination with a telecentric zoom lens to determine the cone angle of the flame (α). Based on the cone angle and the gas velocity (v_u) known from the experiment, the laminar burning velocity (S_u) is calculated by the equation $S_u = v_u \cdot \sin(\alpha)$.

3 Chemical kinetic mechanism

The chemical kinetic mechanism used for the simulation of the experiments is based on the in-house developed model DLR SynNG for the combustion of fuel mixtures of syngas and natural gas [21]. This C_0 – C_3 model has already been optimized with experimental data including ignition delay times, species profiles, and laminar burning velocities. Since nitrous oxide was also present as a reactant in the experiments considered here, the mechanism was expanded with a sub-mechanism for the combustion of nitrogen oxides. In doing so, the reactions with nitrogen-containing species from the Glarborg et al. model from 2018 [22] were sub-joined. The entire mechanism includes 165 species and 1410 reactions and is denoted by DLR SynNG + NO v0.0. All chemical kinetic simulations were performed with the open source software Cantera [23].

4 Mechanism optimization

The modified and optimized versions of the model were generated with help of the linear transformation model (linTM) [24]. The linTM very efficiently analyses the relations between reaction rates of chemical kinetic mechanisms and experimental data. Thus, the global sensitivity analysis of the linTM was applied to identify the reactions with the highest impact on the simulation results at the investigated experimental conditions. The reaction sensitivities from the

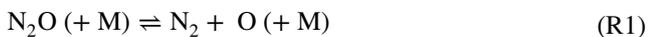
linTM are combining the three Arrhenius coefficients or rates $k(T)$ at three temperatures (k3 method of the linTM), respectively. Therefore, the sensitivities of each rate $k(T)$ span a vector in a three-dimensional space. The length of this vector is defined as the reaction sensitivity of the linTM, and is therefore positive:

$$S_r = \sqrt{\left(\frac{\partial \ln Q}{\partial \ln k(T_1)} \Delta \ln k(T_1)_{\max}\right)^2 + \left(\frac{\partial \ln Q}{\partial \ln k(T_2)} \Delta \ln k(T_2)_{\max}\right)^2 + \left(\frac{\partial \ln Q}{\partial \ln k(T_3)} \Delta \ln k(T_3)_{\max}\right)^2}, \quad (1)$$

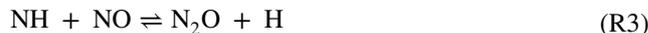
for which Q is the quantity of interest (e.g. ignition delay time or laminar flame speed). The sensitivities of each rate are normalized with their 2σ uncertainty $\Delta \ln k(T)_{\max}$.

Figures 1 and 2 show rate sensitivity coefficients for exemplarily selected simulation conditions for both reaction systems and both types of investigated experiments with the aforementioned mechanism DLR SynNG + NO v0.0. The results for the remaining experimental conditions are comparable.

It can be seen that for both burning velocity and ignition delay time, the two reactions R1 and R2 have major impact on the predictive power of the model:



Also important for burning velocity prediction is reaction R3:



These observations are consistent with the results of Powell et al. [12] from 2009. Powell et al. only optimized reaction R2 and described the reaction rate as the sum of two Arrhenius expressions. Reaction rate of R1 left untouched by Powell et al. based on consistent literature data; Reaction R3 was not changed by Powell et al., since it only plays a minor role.

In the first optimization step within this work, only the Arrhenius parameters of reaction R2 from Klippenstein et al. [25] of the Glarborg et al. model [22] were replaced in the DLR SynNG + NO v0.0 mechanism by the values from Powell et al. [12], to create the model DLR SynNG + NO v0.1.

In a second step, a parameter optimization was performed with the k3 method of linTM [24] and the model DLR SynNG + NO v0.2 was created. Therefore, the Arrhenius parameters of the selected reactions R1, R2, and R3 are changed under the boundary condition that at three

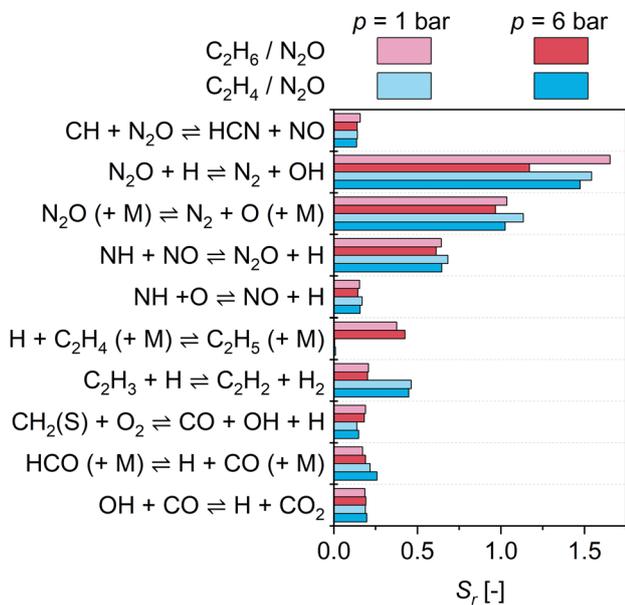


Fig. 1 Global sensitivity coefficients (Eq. 1) of the 10 most sensitive reactions for the measured laminar burning velocity maximum at $T=473$ K, and $p=1$ bar (bright) or $p=6$ bar (dark), each for $\text{C}_2\text{H}_6/\text{N}_2\text{O}$ (red) and $\text{C}_2\text{H}_4/\text{N}_2\text{O}$ (blue) mixtures. Sensitivity coefficients normalized to uncertainty of rate constant of the respective reaction

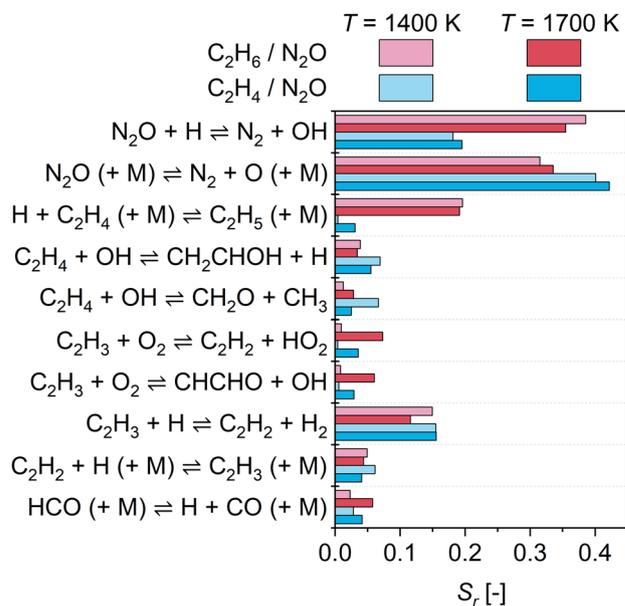


Fig. 2 Global sensitivity coefficients (Eq. 1) of the 10 most sensitive reactions for the ignition delay time at $T=1400$ K (bright) or $T=1700$ K (dark), and $p=1$ bar, each for stoichiometric $\text{C}_2\text{H}_6/\text{N}_2\text{O}$ (red) and $\text{C}_2\text{H}_4/\text{N}_2\text{O}$ (blue) mixtures. Sensitivity coefficients normalized to uncertainty of rate constant of the respective reaction

Table 1 Used uncertainty values for optimization process in linTM at three selected temperatures (k3 method) [24]. Values in brackets corresponds to the 2σ uncertainty

| Reactions | Temperatures (K) | | | Uncertainties (-) | | | References |
|--|------------------|-------|-------|-------------------|-----------------|-----------------|------------|
| | T_1 | T_2 | T_3 | $d \log k(T_1)$ | $d \log k(T_2)$ | $d \log k(T_3)$ | |
| $N_2O (+M) \rightleftharpoons N_2 + O (+M) (k_\infty)$ | 1000 | 1648 | 3000 | 0.172 (0.5) | - 0.027 (0.5) | - 0.445 (0.5) | [26] |
| $N_2O (+M) \rightleftharpoons N_2 + O (+M) (k_0)$ | 1000 | 1648 | 3000 | 0.230 (0.3) | 0.128 (0.3) | - 0.134 (0.3) | [26] |
| $N_2O + H \rightleftharpoons N_2 + OH$ | 298 | 667 | 2000 | - 0.708 (0.5) | 0.671 (0.5) | - 0.176 (0.5) | est |
| | | | | - 0.619 (0.5) | - 0.747 (0.5) | 0.097 (0.5) | |
| $NH + NO \rightleftharpoons N_2O + H$ | 298 | 1200 | 2000 | - 0.213 (0.3) | 0.113 (0.3) | - 0.676 (0.5) | [26] |

Table 2 Overview of original and modified Arrhenius parameters of adapted reactions R1, R2, and R3

| Reaction | A | n | E_a | References |
|--|----------|---------|-----------|------------|
| $N_2O (+M) \rightleftharpoons N_2 + O (+M) (k_\infty)$ | | | | |
| DLR SynNG + NO v0.0 | 9.90E+10 | 0.00 | 5.790E+04 | [22] |
| DLR SynNG + NO v0.1 | 9.90E+10 | 0.00 | 5.790E+04 | [22] |
| DLR SynNG + NO v0.2 | 1.42E+24 | - 3.86 | 6.055E+04 | See text |
| $N_2O (+M) \rightleftharpoons N_2 + O (+M) (k_0)$ | | | | |
| DLR SynNG + NO v0.0 | 6.00E+14 | 0.00 | 5.744E+04 | [22] |
| DLR SynNG + NO v0.1 | 6.00E+14 | 0.00 | 5.744E+04 | [22] |
| DLR SynNG + NO v0.2 | 5.83E+30 | - 4.26 | 7.068E+04 | see text |
| $N_2O + H \rightleftharpoons N_2 + OH$ | | | | |
| DLR SynNG + NO v0.0 | 6.40E+07 | 1.84 | 1.349E+04 | [22, 25] |
| DLR SynNG + NO v0.1 | 2.93E+10 | 0.00 | 4.750E+03 | [12] |
| | 5.82E+14 | 0.00 | 1.788E+04 | |
| DLR SynNG + NO v0.2 | 8.79E+43 | - 9.81 | 1.845E+04 | See text |
| | 9.06E-07 | 5.81 | 8.977E+03 | |
| $NH + NO \rightleftharpoons N_2O + H$ | | | | |
| DLR SynNG + NO v0.0 | 2.70E+15 | - 0.78 | 2.000E+01 | [22] |
| DLR SynNG + NO v0.1 | 2.70E+15 | - 0.78 | 2.000E+01 | [22] |
| DLR SynNG + NO v0.2 | 5.78E+58 | - 13.80 | 1.605E+04 | See text |

Specific reaction rate constants have form $k = A \cdot T^n \cdot \exp(-E_a/RT)$

Units: A : in combinations of cm, mol, s; E_a in cal/mol

selected temperatures the resulting rate constant lies within a previously defined uncertainty range of 3σ (see Tab. 1). The Arrhenius parameters of all modified reactions from the three different models are shown in Tab. 2. The values are fitted parameters for a better agreement between experiment and simulation. To make the changes more visible and to be able to better compare the original with the modified reaction rate constants, the temperature dependence of the reaction rates is shown in Fig. 3.

All other most sensitive reactions usually do not contain any N -containing species (see Figs. 1 and 2). These have not been changed because the C_0 - C_3 model has already been optimized [21].

5 Results and discussion

5.1 Ignition delay time

Experimental ignition delay time results as a function of the inverse temperature are shown in Figs. 4, 5, 6, 7 for both reaction systems, C_2H_4/N_2O and C_2H_6/N_2O , for stoichiometric ($\varphi = 1.0$) and fuel-rich ($\varphi = 2.0$) conditions respectively. At the C_2H_4/N_2O reaction system (Figs. 4 and 5), the original mechanism already showed a satisfactory match for ignition delay times. Nevertheless, an improvement could be achieved by the adaptation of the model (DLR SynNG + NO v0.1). The optimized model (DLR SynNG + NO v0.2) shows an outstanding agreement with the experimental data over the entire temperature range at all pressures, both at $\varphi = 1$ and $\varphi = 2$.

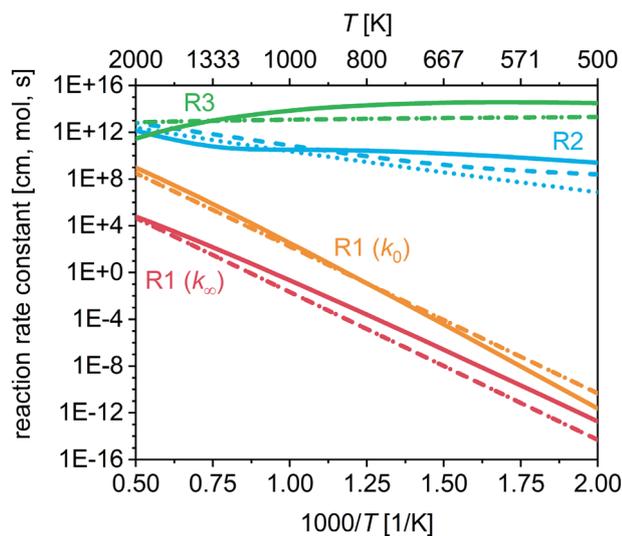


Fig. 3 Comparison of original and modified reaction rates for R1 ($\text{N}_2\text{O} (+\text{M}) \rightleftharpoons \text{N}_2 + \text{O} (+\text{M})$; red and orange), R2 ($\text{N}_2\text{O} + \text{H} \rightleftharpoons \text{N}_2 + \text{OH}$; blue), and R3 ($\text{N}_2\text{O} + \text{H} \rightleftharpoons \text{N}_2 + \text{OH}$; green). Dotted lines: DLR SynNG+NO v0.0; dashed lines: DLR SynNG+NO v0.1; solid lines: DLR SynNG+NO v0.2

Figures 6 and 7 show the results for the reaction system $\text{C}_2\text{H}_6/\text{N}_2\text{O}$. It can be seen here that the simulation results of mechanisms DLR SynNG+NO v0.0 and DLR SynNG+NO v0.2 hardly differ and both provide very good agreement with experimental data. The strong increase of the ignition delay time at atmospheric pressure for temperatures below about 1450 K for the stoichiometric and about 1600 K for the fuel-rich mixture indicates an apparent increase in the global activation energy [18]. This is not reproduced by any of the models used.

The mechanism, in which only the rate constant of R2 was changed (DLR SynNG+NO v0.1), predicts ignition delay times that are too fast compared to the experimental results, especially for low temperatures. This can be explained with help of the sensitivity analysis in Fig. 2. There it can be seen that in the $\text{C}_2\text{H}_6/\text{N}_2\text{O}$ system the reactions $\text{N}_2\text{O} + \text{H} \rightleftharpoons \text{N}_2 + \text{OH}$ (R2) and $\text{N}_2\text{O} (+\text{M}) \rightleftharpoons \text{N}_2 + \text{O} (+\text{M})$ (R1) are both highly sensitive, whereas in the $\text{C}_2\text{H}_4/\text{N}_2\text{O}$ system the sensitivity is mostly dominated by R1. When the Arrhenius parameters are only changed for R2, the effects on the ignition delay times of mixtures with C_2H_4 are significantly smaller. Therefore, there is no big change in Figs. 4 and 5 for model DLR SynNG+NO v0.1 compared to the original mechanism. However, if only reaction R2 is accelerated in reaction system $\text{C}_2\text{H}_6/\text{N}_2\text{O}$ (see Fig. 3), the branching ratio between R1 and R2 is severely impaired. This consequently leads to a change in the formation of radicals at starting reactions of N_2O and thus leading to faster ignition.

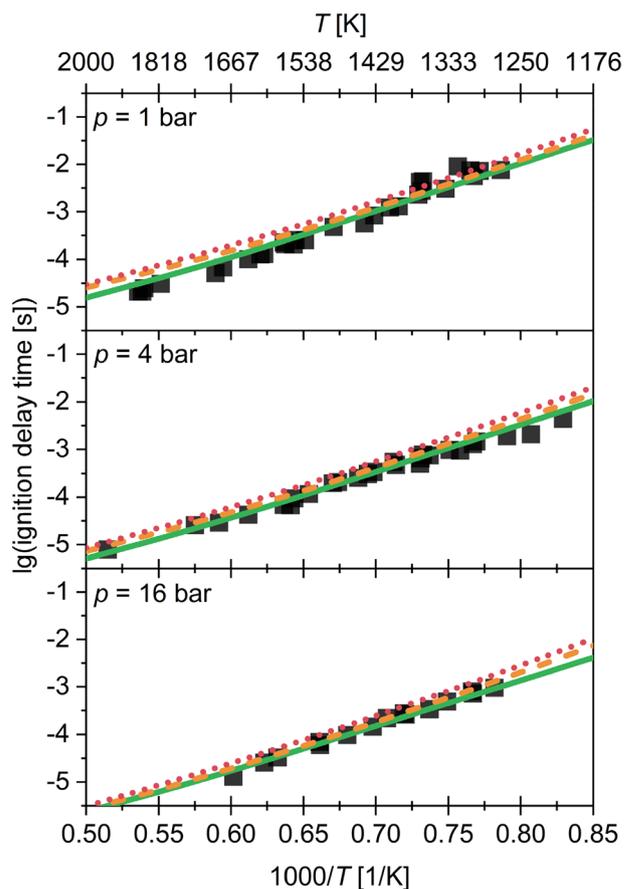


Fig. 4 Comparison between experimental and modeling ignition delay time results for $\text{C}_2\text{H}_4/\text{N}_2\text{O}$ ($\varphi=1.0$) at $p=1, 4,$ and 16 bar. Lines: Simulations (red dotted: DLR SynNG+NO v0.0; orange dashed: DLR SynNG+NO v0.1; green solid: DLR SynNG+NO v0.2). Squares: experimental data from Naumann et al. [18, 19]

5.2 Laminar burning velocity

Laminar burning velocities results for ethane/nitrous oxide and ethane/nitrous oxide are depicted in Figs. 8, 9, 10. Experimental (squares) and simulation results (lines) are shown as a function of equivalence ratio at an initial temperature of 473 K for different pressures ($p=1, 3,$ and 6 bar) and dilution with nitrogen $d(\text{N}_2)=50\%$; for reaction system $\text{C}_2\text{H}_6/\text{N}_2\text{O}$ also for different dilutions ($d(\text{N}_2)=40, 50,$ and 60%) at $p=1$ bar.

Figure 8 depicts the effect of the changes in the Arrhenius parameters in the mechanism optimization affecting the prediction quality of the model, especially at $p=1$ bar. With the original model (DLR SynNG+NO v0.0, red dotted line), there are large differences of up to 0.22 m/s between model and experiment. With every optimization step (from red dotted to orange dashed line, and from orange dashed to green solid line), the correspondence improves; even the changes in rate constants of R2 ($\text{N}_2\text{O} + \text{H} \rightleftharpoons \text{N}_2 + \text{OH}$) in DLR

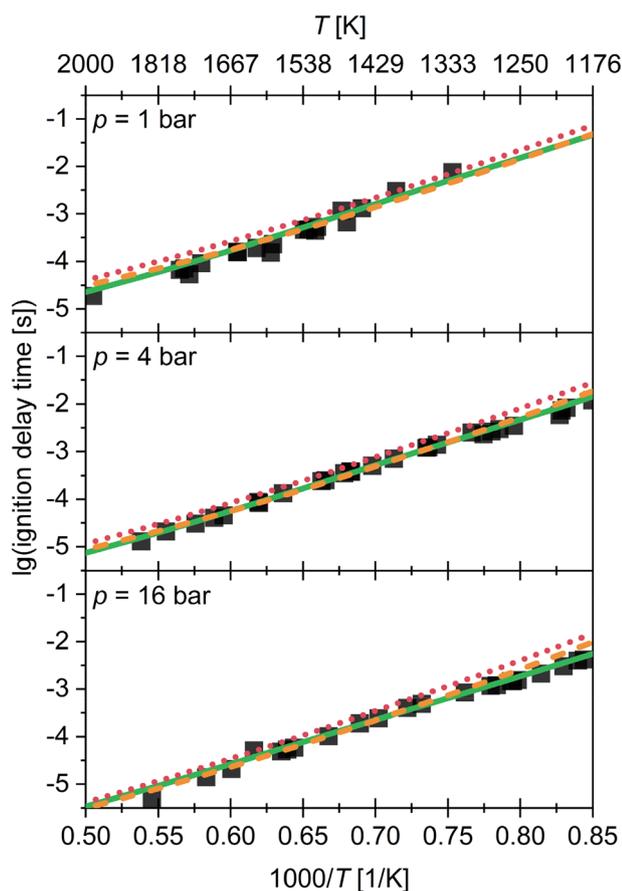


Fig. 5 Comparison between experimental and modeling ignition delay time results for $\text{C}_2\text{H}_4/\text{N}_2\text{O}$ ($\varphi=2.0$) at $p=1, 4,$ and 16 bar. Lines: Simulations (red dotted: DLR SynNG+NO v0.0; orange dashed: DLR SynNG+NO v0.1; green solid: DLR SynNG+NO v0.2). Squares: experimental data from Naumann et al. [18, 19]

SynNG+NO v0.1 (orange dashed line) have an immense influence. This is due to the change from the single-term Arrhenius rate expression from Klippenstein et al. [25] to the double-term Arrhenius rate expression from Powell et al. [12]. While the expression from Klippenstein stems from a theoretical work with focus on a good prediction of NNH and the products from the $\text{N}_2\text{O} + \text{H}$ reaction in total, Powell et al. chose the double-term expression to refit experimental data from Marshall et al. [27], Hidaka et al. [28], and Dean et al. [29] from low to high temperature. This results finally in an improvement of the prediction of the experimental flame speed data from Powell et al.

The smallest differences between experiment and model are obtained at the maximum laminar burning velocity with the mechanism from the second optimization step (DLR SynNG+NO v0.2, green solid line), while the mechanism from the first optimization step (DLR SynNG+NO v0.1, orange dashed line) also delivers good results for fuel-rich mixtures at $p=1$ bar and especially at $p=6$ bar.

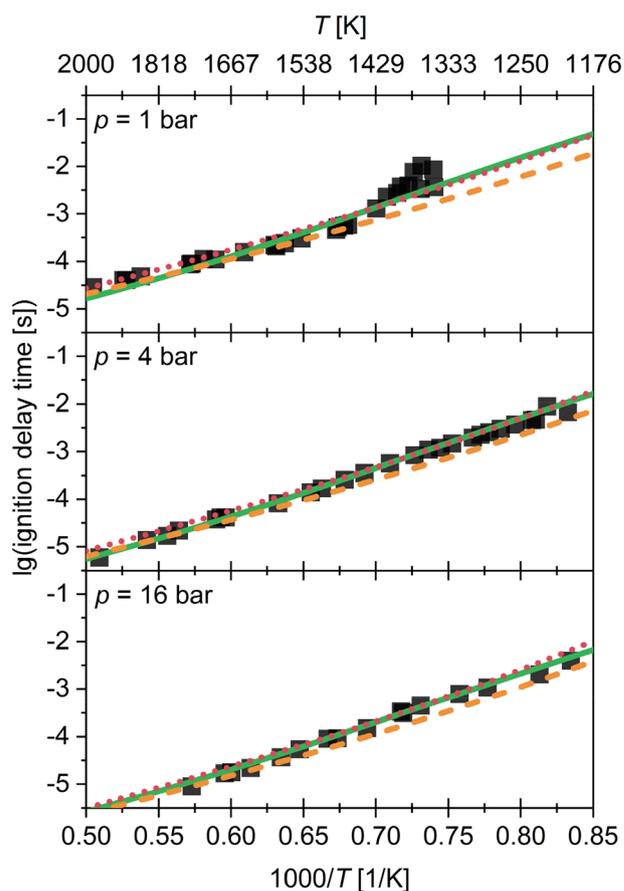


Fig. 6 Comparison between experimental and modeling ignition delay time results for $\text{C}_2\text{H}_6/\text{N}_2\text{O}$ ($\varphi=1.0$) at $p=1, 4,$ and 16 bar. Lines: Simulations (red dotted: DLR SynNG+NO v0.0; orange dashed: DLR SynNG+NO v0.1; green solid: DLR SynNG+NO v0.2). Squares: experimental data from Naumann et al. [18]

The same applies to the results of ethane/nitrous oxide mixtures, see Fig. 9. At pressures of $p=1$ and 6 bar, the model with the three optimized reactions (solid line) is even able to reproduce the measurement data over the entire range of the equivalence ratio exactly. A small difference can only be seen at $p=3$ bar, but the qualitative trend is correct (same in Fig. 8 for $\text{C}_2\text{H}_4/\text{N}_2\text{O}$ mixtures). All models predict an influence of the pressure on the laminar burning velocity.

Furthermore, the influence of the dilution with nitrogen on the laminar burning velocity was simulated (see Fig. 10). Here too, the DLR SynNG+NO v0.2 mechanism (green solid line) provides the best results and, in all cases examined experimentally, a very good agreement for all equivalence ratios. Therefore, this mechanism can also be used to predict laminar burning velocities without nitrogen dilution.

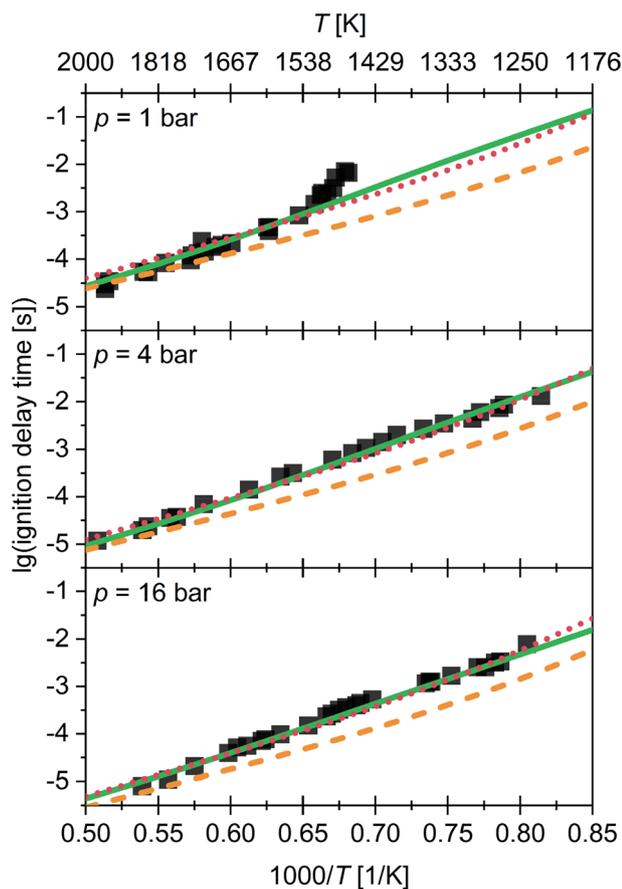


Fig. 7 Comparison between experimental and modeling ignition delay time results for C_2H_6/N_2O ($\phi=1.0$) at $p=1, 4,$ and 16 bar. Lines: Simulations (red dotted: DLR SynNG+NO v0.0; orange dashed: DLR SynNG+NO v0.1; green solid: DLR SynNG+NO v0.2). Squares: experimental data from Naumann et al. [18]

6 Conclusion

Ethane/nitrous oxide and ethene/nitrous oxide mixtures are possible candidates as green propellants, which could replace hydrazine and its derivatives as rocket fuel. Chemical kinetic mechanisms that predict the combustion behavior of these mixtures are necessary for the design of safe and reliable thrusters. As in this work, experimental literature data of global combustion parameters such as ignition delay times and laminar burning velocities are used to optimize detailed kinetic mechanisms. The starting point for the optimization was a mechanism for syngas and natural gas (DLR SynNG) by Methling et al. [21], coupled with the nitrogen oxide model by Glarborg et al. from 2018 [22]. With the help of sensitivity analyses, three reactions were identified that are of great importance for optimizing the mechanism:

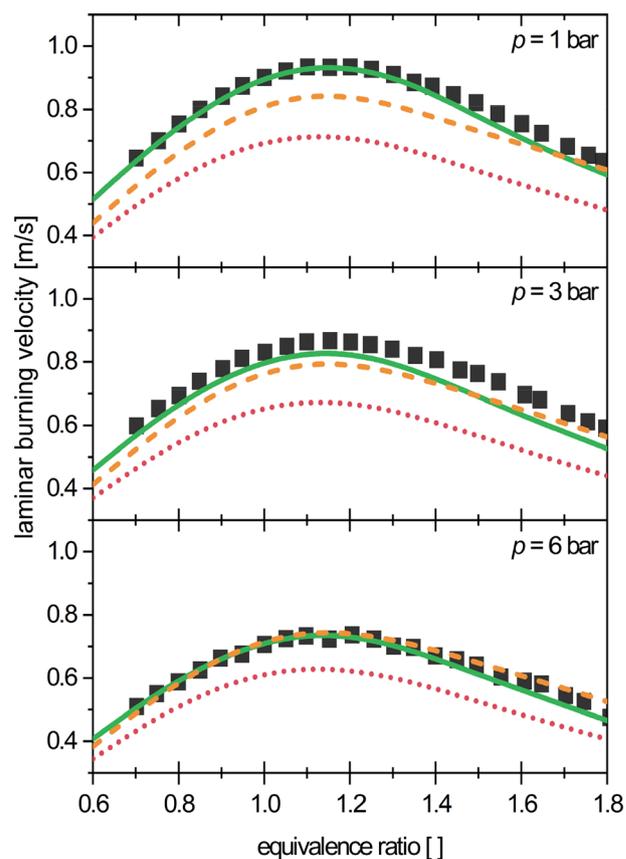
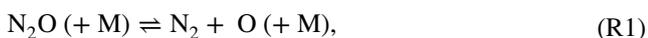


Fig. 8 Experimental laminar burning velocity results and model predictions for C_2H_4/N_2O mixtures ($d(N_2)=50\%$, $T=473$ K) at $p=1, 3,$ and 6 bar. Lines: simulations (red dotted: DLR SynNG+NO v0.0; orange dashed: DLR SynNG+NO v0.1; green solid: DLR SynNG+NO v0.2). Squares: experimental data from Kick et al. [17] and Richter et al. [20]



The best agreement between model and experiment could be achieved for ignition delay times if the Arrhenius parameters were adjusted of all three reactions (mechanism DLR SynNG+NO v0.2). The same applies to the laminar burning velocities over entire range of equivalence ratio considered. With the changed Arrhenius parameters, the mechanism DLR SynNG+NO v0.2 is therefore able to predict laminar burning velocities and ignition delay times in the examined range correctly. In future work, this detailed optimized mechanism serves as the basis for a reduced mechanism, which should be used in CFD simulations.

Supplementary Information The online version contains supplementary material available at <https://doi.org/10.1007/s12567-021-00370-8>.

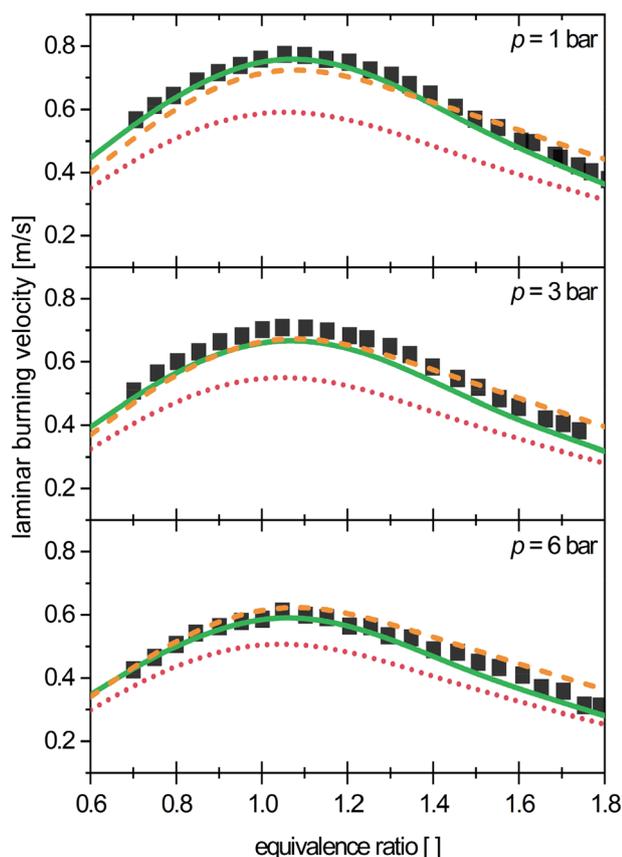


Fig. 9 Experimental laminar burning velocity results and model predictions for C_2H_6/N_2O mixtures ($d(N_2)=50\%$, $T=473$ K) at $p=1$, 3, and 6 bar. Lines: simulations (red dotted: DLR SynNG+NO v0.0; orange dashed: DLR SynNG+NO v0.1; green solid: DLR SynNG+NO v0.2). Squares: experimental data from Richter et al. [20]

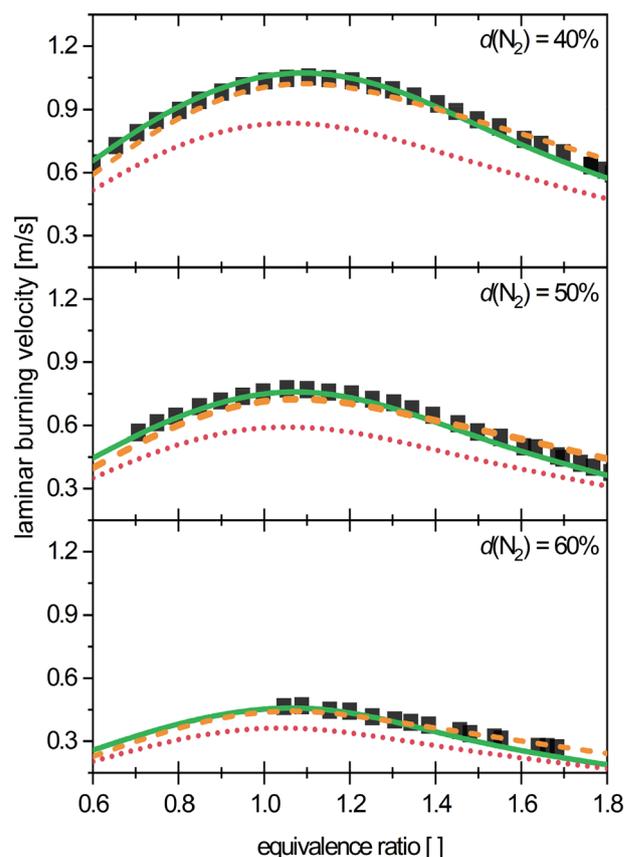


Fig. 10 Experimental laminar burning velocity results and model predictions for C_2H_6/N_2O mixtures ($p=1$ bar, $T=473$ K) for different dilutions with N_2 ($d(N_2)=40, 50, 60\%$). Lines: simulations (red dotted: DLR SynNG+NO v0.0; orange dashed: DLR SynNG+NO v0.1; green solid: DLR SynNG+NO v0.2). Squares: experimental data from this work

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Availability of data and material All data and information being necessary to understand the study are given in the manuscript.

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