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# The cybermatrix protocol: a link between classical aircraft design and formal multidisciplinary optimization

Knowledge for Tomorrow

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# A merger of two approaches

#### Classic aircraft design

- ✓ Focus on process automation, many disciplines, data modeling
- ➤ No specific focus on high-performance computing (HPC)
- $\checkmark$  No formal optimality criteria, suboptimal designs by construction

#### ✓ Formal multidisciplinary optimization

- ✓ Focus on analysis fidelity, modeling constraints, and adding disciplines
- Explicit consideration of optimality criteria and often high HPC use
- ✓ Simplifed tools, poorly scalable in number of disciplines/experts
- ✓ The proposed solution establishes a link between the two approaches
  - Developed within the DLR project VicToria
  - Optimality criteria explicit, but applied in a heuristic manner
  - ✓ Parallelism from ground up, both in expert participation and in use of HPC
  - ✓ Implementation (human) and execution (computer) phases with analogous communication and control in a matrix-like structure → cybermatrix



# The design equation

Any design process can be viewed as an **approximate** optimization process:

$$\frac{\widehat{df(p)}}{dp} - \frac{\widehat{dc(p)}}{dp}^{T}q = 0, \quad c(p) = 0$$

where **f** goal ( $\mathbb{R}^1$ ), **c** constraints ( $\mathbb{R}^m$ ), **p** design parameters ( $\mathbb{R}^n$ ), **q** goal-to-constraint sensitivities (Lagrange multipliers,  $\mathbb{R}^m$ )  $\rightarrow$  approximate first KKT optimality condition

**\checkmark** Expanded for three disciplines **A**, **B**, **C** and global goal function *F* ( $\mathbb{R}^1$ ):

$$\begin{aligned} & \frac{\widehat{\partial F}}{\partial f_A} \frac{\widehat{df_A}}{dp_A} + \frac{\widehat{\partial F}}{\partial f_B} \frac{\widehat{df_B}}{dp_A} + \frac{\widehat{\partial F}}{\partial f_C} \frac{\widehat{df_C}}{dp_A} - \frac{\widehat{dc_A}^T}{dp_A^T} q_A - \frac{\widehat{dc_B}^T}{dp_A^T} q_B - \frac{\widehat{dc_C}^T}{dp_A} q_C = 0, \quad \underline{c_A} = 0 \\ & \frac{\widehat{\partial F}}{\partial f_A} \frac{\widehat{df_A}}{dp_B} + \frac{\widehat{\partial F}}{\partial f_B} \frac{\widehat{df_B}}{dp_B} + \frac{\widehat{\partial F}}{\partial f_C} \frac{\widehat{df_C}}{dp_B} - \frac{\widehat{dc_A}^T}{dp_B^T} q_A - \frac{\widehat{dc_B}^T}{dp_B^T} q_B - \frac{\widehat{dc_C}^T}{dp_B^T} q_C = 0, \quad \underline{c_B} = 0 \\ & \frac{\widehat{\partial F}}{\partial f_A} \frac{\widehat{df_A}}{dp_C} + \frac{\widehat{\partial F}}{\partial f_B} \frac{\widehat{df_B}}{dp_C} + \frac{\widehat{\partial F}}{\partial f_C} \frac{\widehat{df_C}}{dp_C} - \frac{\widehat{dc_A}^T}{dp_C^T} q_A - \frac{\widehat{dc_B}^T}{dp_C^T} q_B - \frac{\widehat{dc_C}^T}{dp_C^T} q_C = 0, \quad \underline{c_B} = 0 \end{aligned}$$



#### Sidenote: An interpretation of Lagrange multiplier

✓ Example: Find p, q for an aircraft that minimize mission fuel expenditure  $(m_f)$ under max. take-off field length  $(s_{TO})$ and other constraints

$$m_f^* = \min_{p,q} m_f$$
$$s_{TO} \le s_{TO}^* (\to q_{s_{TO}})$$
$$etc.$$



- ✓ The measure of how much the goal would change per unit constraint change
  - $\checkmark$  An information highly sought for by designers

Why are we never reporting it?



#### The representation protocol

- ✓ Since the design equation is usually implied, use a schematic representation
- ✓ Let each row belong to one discipline (all related to its design parameters)



### The communication protocol

- ✓ Each disciplinary design process can have any form, only iteration assumed
- ✓ Add to it data exchange points and initial data estimators



#### Sidenote: An iteration with gradient based processes

- Assume all disciplinary processes A, B, C are gradient-based processes, using (different) off-the-shelf gradient-based optimization algorithms
- Step k of A (analogous for B, C) could be a single gradient computation plus the associated line/trust-region search

$$\frac{\widehat{\partial F}}{\partial f_A} \frac{\widehat{df_A}}{\underline{dp_A}} \bigg|_{p_A^{k+1}, p_{B,C}^k} + \left( \frac{\widehat{\partial F}}{\partial f_B} \frac{\widehat{df_B}}{dp_A} + \frac{\widehat{\partial F}}{\partial f_C} \frac{\widehat{df_C}}{dp_A} - \frac{\widehat{dc_B}}{dp_A}^T q_B - \frac{\widehat{dc_C}}{dp_A}^T q_C \right)_{p_{A,B,C}^k} - \frac{\widehat{dc_A}^T}{\underline{dp_A}} q_A \bigg|_{p_A^{k+1}, p_{B,C}^k} = 0$$

which an off-the-shelf optimizer can be tricked to perform by modifying the original disciplinary goal function in the step k as

$$\widetilde{f_A}\Big|_{p_A^{k+1}, p_{B,C}^k} = \frac{\widehat{\partial F}}{\partial f_A}\Big|_{f_A^k} \underbrace{\underline{f_A}}_{p_A^{k+1}, p_{B,C}^k} + \left(\frac{\widehat{\partial F}}{\partial f_B} \frac{\widehat{df_B}}{dp_A} + \frac{\widehat{\partial F}}{\partial f_C} \frac{\widehat{df_C}}{dp_A} - \frac{\widehat{dc_B}^T}{dp_A}^T q_B - \frac{\widehat{dc_C}^T}{dp_A}^T q_C\right)_{p_{A,B,C}^k} (p_A^{k+1} - p_A^k)$$

linearized "penalty" – how much to "give up" for other disciplines

- $\checkmark$  The same idea and rationale as e.g. for coupled-adjoint gradient evaluation
  - Jacobi/Gauss-Seidel fixed-point block-iteration to couple processes, each using the best method for its internal iteration, with "rhs modification"



#### A realization on HPC clusters

- $\checkmark$  A cybermatrix HPC process integration framework in development
  - Starts disciplinary processes, assigns resources, monitors progress
  - Triggers data exchanges and determines global convergence
- Disciplinary experts do not work with the framework directly
  - ✓ No need to learn yet another integration framework
  - Only provide input collector scripts to copy data from other disciplines
  - ➤ The whole MDO process implementation: a directory of input collectors
- ✓ Maintainable by standard software engineering tools and practices
  - ✓ Set of input collectors under source version control
  - Integration framework is an interpreter of the set of collectors and some meta-data (data exchange periods, etc)
- ✓ Currently data exchange performed over parallel on-disk file system
  - ✓ Parallel in-memory or area-network file system possible in principle
  - $\checkmark$  No changes to disciplinary processes in any case



#### **On-machine appearance**





#### **Example: MDO of a long-range transport aircraft**

- ✓ Large twin-engine wide-body long-range transport aircraft
  - Wing-body-tail-pylonflow through nacelle
  - 250 t max. take-off mass class
- Global goal function:
  minimize fuel consumption
- ✓ Involved disciplinary processes:
  - Overall aircraft wing planform design (oad)
  - Aerodynamic design of wing airfoils (aero)
  - ✓ Structural member sizing of wing and tail (struct)
  - Determination and evaluation of design loads (loads)







#### **Example: Problem setup** aero Adjoint aeroelastic optimization RANS flow, mesh 5,900,000 pts oad 🐭 CAD+ROM airfoil shapes, Rolling trade study total mass 126 design parameters (tuned trust reg. SQP) Minimize drag at trimmed flight CAD+ROM wing shape, total drag Step: one gradient and line search < 10 design parameters Minimize mission fuel wing planform Step: one QP approx. V oad oad and trust req. step aero global FEM, CoG airfoil shapes aero aero aero oad struct wing planform wing planform struct struct design loads oad aero dynamic FEM, MCs struct loads loads loads load oad struct Fully-stressed design Dynamic gust, turbulence Global FEM, 42,000 els Dynamic FEM, 1,060 DoF Model region thicknesses, Panel aero, 1,160 boxes oad 364 design parameters 1,200 LCs / 2 MCs aero Minimize mass for limit No goal/cons./design par. strength, buckling per LC struct \* Step: one full evaluation Step: one full sizing loads



# **Example: Optimization results**

- ✓ Still robustness problems on planform variations, so planform fixed → oad only for evaluation
- Total run time:98 hours on 192 cores
  - → Base period duration: 13.9 h avg
- Drag reduction (-7.2%) more significant than mass increase (1.6% wing, 0.16% total), resulting in mission fuel reduction (-6.9%)
  - Wing sections slightly retwisted and reshaped to reduce shock waves
  - Somewhat less favorable spanwise load distribution results in higher design loads
  - Variation in number of design load cases not large, but not negligible
  - What is the baseline for comparison?
    - $\checkmark$  Time 0 on wall-time axis has no meaning
    - Intention-dependent: here result of an optimization with fixed **aero** design param.

#### Sidenote: Jacobi, Gauss-Seidel, mixed iteration



#### Sidenote: Which process "must" run before which?





- Just a difference in time to convergence
- Though if multiple optima, could fall into a different one



#### **Conclusions and outlook**

- ✓ A core of a cybermatrix-based MDO process demonstrated
  - Aero-structural approximate overall aircraft optimization with configuration-dependent variable number of design load cases
  - ✓ Maneuver and gust loads process following certification regulations
  - ✓ CAD-based shape parametrization through reduced order modeling
- ✓ Improvement to the core process
  - $\checkmark$  More robustness in local design on planform variations
  - ✓ More flight points and powered engine for aerodynamic design
  - Control laws and high-fidelity corrections for loads
  - ✓ More design dependencies (Jacobian-like information)
- $\checkmark$  Beyond the core process
  - ✓ Higher fidelity structural modeling (separate wing/fuselage disciplines)
  - ✓ Tighter geometry and mass synthesis (aircraft synthesis discipline)
  - ✓ Configuration-dependent engine conceptual design (engine discipline)
  - Flutter analysis (to eliminate planforms exhibiting inherent flutter)

Thank you for your attention!



...plans of penguins and people...

