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## Signal analysis of the first GPS III satellite

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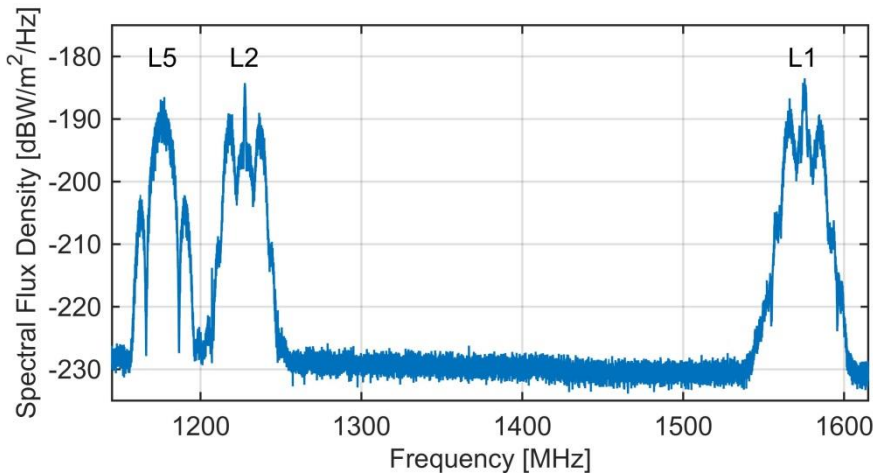
### Abstract

The signal-in-space of the first GPS Block III spacecraft is analyzed based on radio-frequency measurements collected with a 30 m high-gain dish antenna as well as data from geodetic GPS receivers. The spectral properties and modulation characteristics are discussed with focus on the L1 band, which employs a novel interlaced majority voting technique for combination of the C/A, P(Y), and L1C data+pilot signal components. Compared to the preceding generation of Block IIF satellites, a modified shaping of the L1 transmit antenna gain pattern is found, which results in lower carrier-to-noise density ratios at mid to high elevations. Along with this, use of a separate transmission chain for the military M-code signal is evidenced through the analysis of in-phase/quadrature signal components and the derived transmit antenna gain variations. A high level of signal purity is demonstrated on all frequencies, which can be attributed to the use of a new, mostly digital, signal generation unit. Maps of code bias variations for selected signals are presented to quantify the achievable user tracking performance as a function of user receiver parameters. For the L5 signal, a notable reduction of digital distortions is obtained with respect to the Block IIF satellites, whereas analog distortions are found to be of similar magnitude. Thermally induced L5 phase variations found in the Block IIF satellites are no longer observed in GPS III. Using triple-frequency phase observations, a sub-centimeter consistency of the L1, L2, and L5 carriers is demonstrated.

## Introduction

Space Vehicle Number (SVN) 74 is the first of a new generation of GPS satellites built by Lockheed Martin. The GPS III satellites offer an increased 15-years life time and a wide series of technological improvements over their predecessors, while maintaining compatibility with other satellites in the constellation for navigation users. Among others, the satellites make use of a new, mostly digital, signal generation unit, support up to 64 different ranging codes, host three enhanced rubidium atomic frequency standards, support continuous monitoring of a redundant clock in hot standby, and are equipped with an enhanced cross-link transponder (Marquis and Shaw 2011).

The SVN 74 spacecraft with a wet mass of about 3.7 tons and a dry mass of 2.2 tons was launched with a Falcon 9 rocket from Cape Canaveral, Florida, on December 23, 2018. Following injection into a transfer orbit and performance of several orbit raising maneuvers, the spacecraft arrived near slot “3” of orbital plane “F” and started transmission in the L1, L2, and L5 frequency bands in early 2019 (Fig. 1). First signals using the pseudorandom noise (PRN) number 4 ranging codes were tracked by worldwide GPS receivers starting on January 9.



**Fig. 1** SVN 74 spectrum recorded with the Weilheim 30 m antenna on January 9, 2019 at 12:40 UTC.

Among the most notable features of the new GPS III satellites is the transmission of a new civil navigation signal, named L1C, on the L1 frequency (IS-GPS-800E, 2018). Compared to the legacy L1 coarse/acquisition (C/A) code, the L1C signal uses the same chipping rate of 1.023 MHz but makes use of 10-times longer ranging codes, provides distinct data and pilot channels, and carries the new CNAV-2 navigation message with forward error correction (Betz et al. 2006). The use of a binary offset carrier (BOC(1,1)) modulation with a square sub-carrier of the same rate as the ranging code results in a split power spectrum and enables good compatibility with other L1 signals. Improved multipath performance is, furthermore, achieved through time multiplexed binary offset carrier (TMBOC(6,1,4/33)) modulation of the pilot channel, which replaces the BOC(1,1) subcarrier by a BOC(6,1) subcarrier for 4/33th of the time (Chen et al. 2014). Distinct families of Weil codes were selected to achieve optimum cross-correlation properties for both pilot and data channel modulation (Rushanan 2007). Overall, L1C offers more robust navigation under adverse signal conditions such as low power or multipath as well as reduced

time-to-first fix. It is, furthermore, designed to be fully interoperable with the Galileo E1 Open Service signal (Hein et al. 2006) and the BeiDou B1C signal on the same center frequency.

An early characterization and quality assessment of signals transmitted by the new GPS III satellite within the first month after activation are presented in this work. The results are based on high-gain antenna measurements obtained at the Weilheim signal monitoring facility (Thoele et al. 2009). With a diameter of 30 m, the antenna offers a total gain of about 50 dB and enables detailed performance studies in the spectral and temporal domain for all GNSS signals in the lower and upper L-band. Furthermore, absolute power level measurements are supported through regular calibration of the entire measurement system against external standards. Complementary to the signal monitoring facility, observations with geodetic-grade multi-frequency receivers are conducted to assess the SVN 74 tracking performance from a user perspective.

Following the introduction, the article first provides an overview of GPS III signals in the L1, L2, and L5 frequency bands. Specific modulation schemes and differences with respect to previous generations are outlined and illustrated through signal spectra and in-phase and quadrature constellation diagrams. A quantitative performance assessment based on high-gain antenna measurements and receiver tracking data is provided in the subsequent section. It provides an S-curve analysis for evaluation of chip-shape induced code tracking biases, a signal strength characterization, and a comparison of receiver tracking noise and multipath for different signals. Furthermore, the consistency of the L1, L2, and L5 carriers is evaluated using a triple-carrier phase combination.

## **GPS III signals**

Within this section the GPS III signals are briefly introduced, and basic signal analyses are performed based on spectral and in-phase and quadrature (IQ) measurements.

### **L1 signal components**

The L1 signal transmitted by the GPS III satellites comprises a notably larger number of individual components than that of past generations. As documented in the US Federal Radionavigation Plan, the US government is committed to continue transmission of the C/A-code and the encrypted P(Y)-code with their current characteristics for up to a minimum of two years after the deployment of a 24-satellites GPS constellation with L5 capability (FRNP 2017). Along with the military M-code signal and the addition of a new civil L1C signal comprising a data (L1C-D) and pilot (L1C-P) component, a total of five navigation signals are now transmitted on the L1 carrier to maintain the desired level of full backwards compatibility (Table 1; Betz 2016).

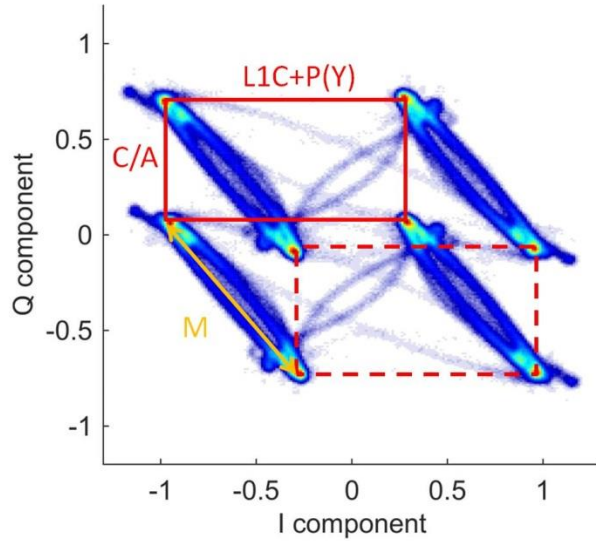
**Table 1** GPS III L1 signal components

Component	Modulation	Chipping rate [MHz]	Minimum received power [dBW]	Reference
C/A	BPSK(1)	1.023	−158.5	IS-GPS-200J (2018)
L1C data	BOC(1,1)	1.023	−163.0	IS-GPS-800E (2018)
L1C pilot	TMBOC(6,1,4/33)	1.023	−158.25	IS-GPS-800E (2018)
P(Y)	BPSK(10)	10.23	−161.5	IS-GPS-200J (2018)
M	BOC(10,5)	10.23	−158.0	Marquis and Reigh (2015)

BPSK: Binary Phase Shift Keying; BOC: Binary Offset Carrier; TMBOC: Time-Multiplexed BOC

Compared to the coherent adaptive subcarrier modulation (CASM; Dafesh et al. 1999, Partridge and Dafesh 2001) that is used in the Block IIR-M and IIF satellites for combining the C/A-, P(Y)- and M-codes with adjustable power levels, a notably different approach is taken in GPS III. First, a distinct amplifier and antenna chain are used for the M-code transmission, which can thus be controlled independently from the four other signal components transmitted via the main L-band antenna. For the remaining four signals, a quadrature phase shift keying (QPSK) modulation is employed with one signal (C/A-code) in the quadrature (Q) channel and an interlaced majority voting combination (Spilker and Orr 1998) of the P(Y) signal along with the L1C data and pilot components in the in-phase (I) channel. Overall, the employed multiplexing scheme offers an efficient constant-envelope modulation of four user signals.

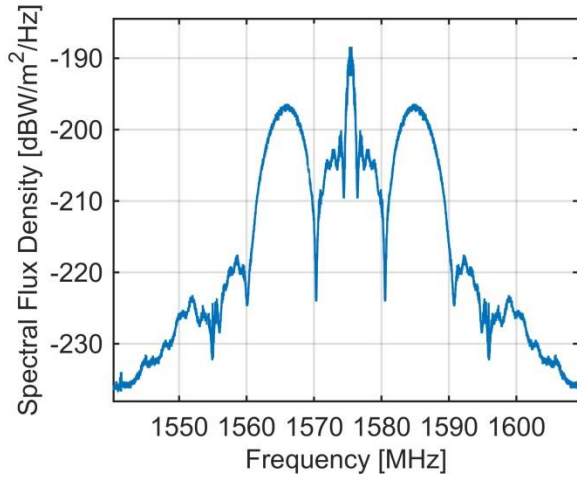
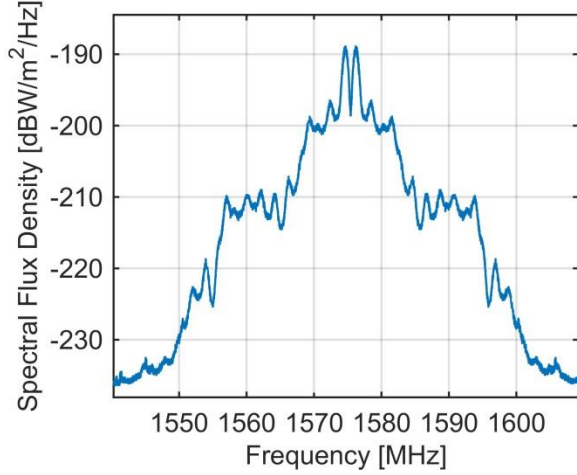
The L1 signal composition is illustrated by the IQ constellation diagram in Fig. 2, which shows the color-coded amplitude of in-phase and quadrature signal components obtained after down-conversion and Doppler-removal of the SVN 74 L1 signal collected with the 30 m high-gain antenna. The QPSK modulation of C/A-, P(Y)- and L1C-codes results in a rectangular set of stationary points, which alternates between two positions in the IQ plane depending on the instantaneous M-code chip and data bit. While the M-code is generated phase-coherently with the other signals, the transmission via a different antenna chain with different phase center results in a phase shift with respect to transitions of the other signals. This phase shift depends on the projection of the relative phase center vector on the line of sight and therefore varies over time along with the varying boresight angle. Different alignments of the M-code transitions with respect to those of the other signals may thus be observed at different measurement epochs. In addition, the relative amplitude of M-code chip transitions varies with the viewing direction due to the different antenna gain patterns.



**Fig. 2** IQ constellation plot of GPS III L1 signals showing the in-phase contribution of the L1C + P(Y) signal components and the C/A code quadrature component as well as the M-code signal transmitted by a separate antenna chain.

Properties of the individual L1 signal components can best be studied, whenever the M-code transition is closely aligned with the quadrature component of the main L-band antenna signal and can readily be separated from the L1C and P(Y) contribution. This is illustrated in Fig. 3, which shows distinct spectra obtained from the I- and Q-channels in such a condition. For the in-phase component (top), two narrow peaks can be recognized next to the center frequency, which are caused by the BOC(1,1) modulation of the 1.023 MHz L1C signal. They are superimposed on a ten times wider lobe of reduced amplitude, which originates from the BPSK(10) binary phase shift keying modulation of the 10.23 MHz P(Y) signal. A completely different pattern is obtained for the quadrature-phase components (Fig. 3, bottom), which reflects the contribution of the 1.023 MHz C/A-code. At the same time, the BOC(10,5) binary offset carrier modulation of the 5.115 MHz M-code with a 10.23 MHz subcarrier is clearly discernible from two broad lobes shifted by about  $\pm 10$  MHz from the center frequency.

The combination of three components, i.e., L1C data, L1C pilot, and P(Y), into a single binary signal sequence for the I-channel is accomplished through “interlaced majority voting”, also known as “weighted voting”. This technique extends the concept of majority voting for multiplexing of signals with time multiplexed interlacing of chips from the two strongest signals (Spilker and Orr 1998; Dafesh and Kahn 2009, Frye 2017). While majority voting alone yields an equal-power combination, the weighted voting scheme can be used to combine the three signals with different effective power level. This is achieved by controlling the fractions of time during which an individual signal is transmitted instead of the combination obtained by a traditional majority voting.



**Fig. 3** Spectral contributions of selected GPS III L1C + P(Y) signal components (top) and M + C/A (bottom).

In case of GPS III, the interface specifications (IS-GPS-200J, IS-GPS-800E) define the minimum received power levels summarized in Table 1. From these, relative power levels of 1.41 and 2.98 can be derived for the L1 P(Y) and L1C-P signals relative to the weakest signal component L1C-D. Using majority voting, a combined signal

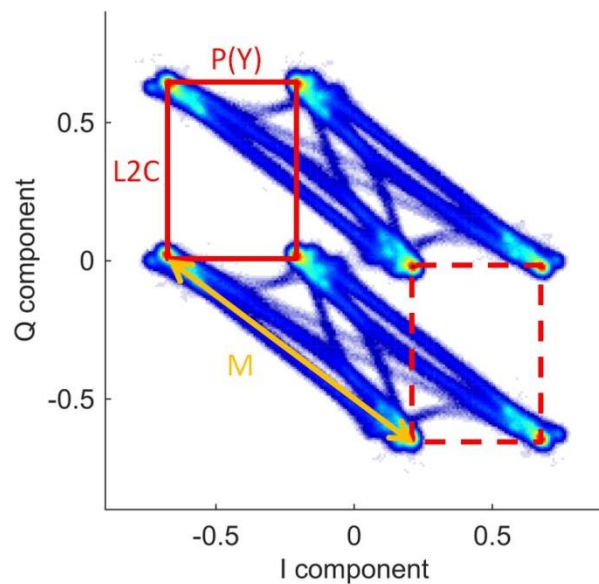
$$s_{MV} = s_{L1C-D} + s_{L1C-P} + s_{P(Y)} - s_{L1C-D} \cdot s_{L1C-P} \cdot s_{P(Y)}$$

with 25% power sharing for each of the three user signal components and the intermodulation product is obtained. Based on a pseudorandom sequence, the signal generator then toggles between transmission of the  $s_{MV}$  combination and transmission of uncombined  $s_{L1C-P}$  and  $s_{P(Y)}$  signals for the specified fractions of time. As discussed in Dafesh and Kahn (2009) and Allen et al. (2019), the specified power ratios are achieved by transmitting the majority voting combination for only 68.5% of the time, while transmitting pure L1C-P or P(Y) signals for averages of 25% and 6.5%, respectively.

Due to the unknown P(Y)-code chip sequence and the associated intermodulation product, the interlacing rate and pseudorandom sequence could not be unambiguously identified within the present study. Likewise, it was not possible to independently verify the published power ratios of the L1C-D/P and P(Y)-code components from the collected IQ measurements.

## L2 signal components

On the L2 frequency, the legacy P(Y)-code and the civil L2C signal are transmitted that had been introduced with the modernized GPS IIR-M satellites along with the military M-code. A simple QPSK modulation is used for the P(Y) and L2C signal, while the M-code is transmitted via a separate antenna chain like on L1. The resulting IQ constellation is illustrated in Fig. 4. In accordance with the 3 dB difference of the minimum power level specifications in IS-GPS-200J (2018), the L2C transitions have a roughly  $\sqrt{2}$  times higher amplitude than the P(Y) code chips, which corresponds to a 3 dB difference in power level. The phase orthogonal modulation of the two signals in SVN 74 with L2C lagging L2 P(Y) by  $90^\circ$  represents the current default for all L2C capable GPS satellites. It is also indicated through a corresponding status bit of the CNAV navigation message to alert users of a possible transmission of phase aligned L2C and L2 P(Y) signals (IS-GPS-200J 2018).

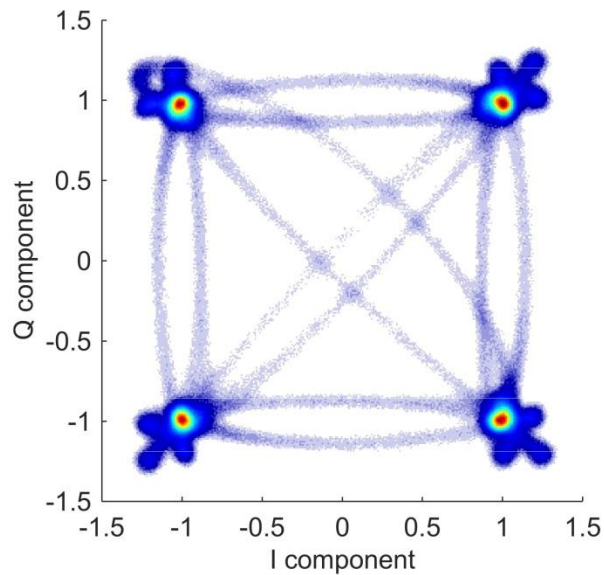
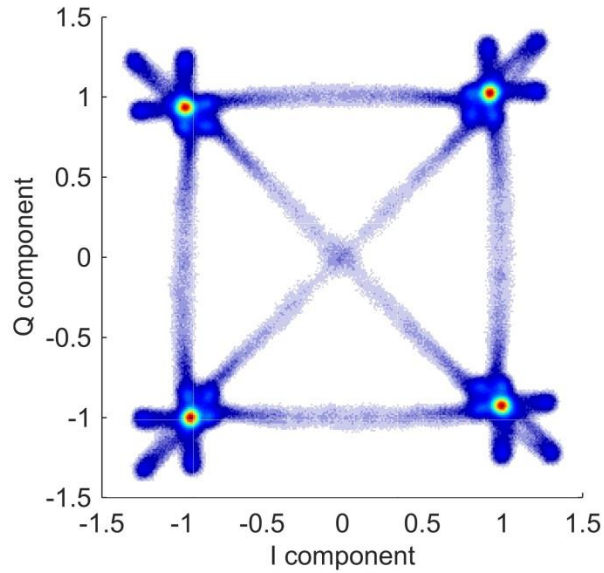


**Fig. 4** IQ constellation plot of GPS III L2 signals showing the QPSK modulated L2C and P(Y) signal components as well as the M-code transmitted by a separate antenna chain.

## L5 signal components

The QPSK modulation of the GPS III L5 data and pilot signals with their 10.23 MHz ranging codes matches that of the Block IIF satellites. The IQ constellation diagram shows an extreme purity of the SVN 74 L5 signal compared to previous satellites (Fig. 5), which can be attributed to the use of a mostly digital navigation signal generation unit.

Based on the superior chip transition quality an associated reduction of correlator-dependent ranging biases maybe expected which would benefit the overall error budget for aviation users (Phelts et al. 2010, Hegarty and Ross 2010). This is further investigated and quantified in the following section.



**Fig. 5** IQ constellation plot of the GPS III L5 signal (SVN 74, top) measured on January 9, 09:34 UTC as compared to the GPS IIF-1 satellite (SVN 62, bottom; after Thaelert et al. 2010).

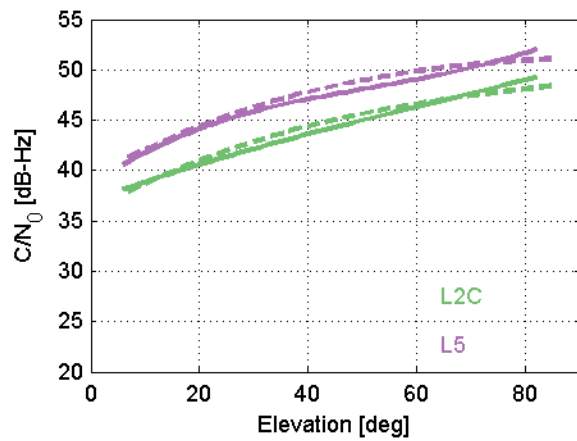
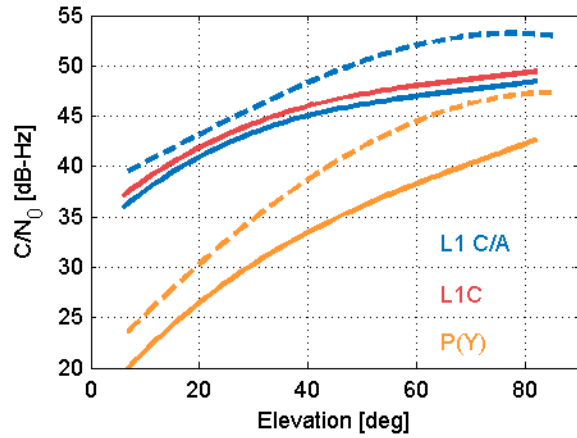


## Signal and measurement quality

Within this section, further analyses of the GPS III signals and the achievable quality of user measurements are presented.

### Antenna pattern and signal strength

Using carrier-to-noise density ratio ( $C/N_0$ ) measurements of a GNSS receiver, the received signal strength of GPS III signals can be compared against other satellites in the GPS constellation. For illustration, Fig. 6 shows the variation of  $C/N_0$  with elevation, or, equivalently, transmit boresight angle, as recorded by a reference station near the satellite ground track for SVN 74 and a Block IIF satellite (PRN 9, SVN 68) in the same orbital plane. A third-order polynomial has been fitted to the original  $C/N_0$  values of one satellite pass on February 15, 2019. For the L1 C/A-code, the Block IIF  $C/N_0$  values are stronger by 2-3 dB for elevations up to about  $35^\circ$ . Above this elevation, the  $C/N_0$  difference between Block IIF and Block III increases to almost 5 dB. This behavior is also visible in the P(Y)  $C/N_0$  curve representing the semi-codeless tracking on L1 and L2. The  $C/N_0$  values for L1C pilot tracking show the same elevation dependence as those for L1 C/A, but are stronger by about 1 dB. Differences of  $C/N_0$  for the L2C and L5 signals of the GPS III and GPS IIF satellites are below 0.8 and 1.0 dB, respectively. A notably different shaping of the L1 transmit antenna pattern for the two types of satellites can be inferred from the  $C/N_0$  of L1 C/A and L1C tracking at mid to high elevations. While an M-shaped far-field antenna pattern has been implemented on all GPS satellites starting with Block I to achieve a more uniform received signal power across the entire surface of the Earth (Czopek and Shollenberger 1993), the  $C/N_0$  measurements suggest a notably flatter gain variation of the GPS III L1 antenna pattern in the vicinity of the boresight direction as compared to the IIF satellite.

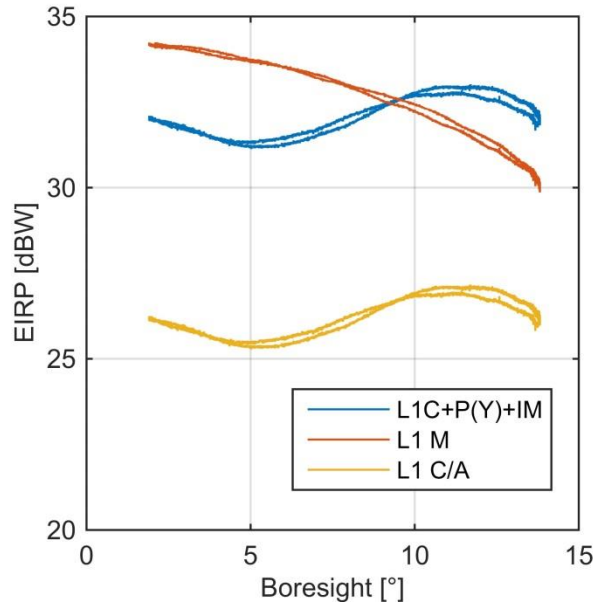


**Fig. 6** Carrier-to-noise density ratio of GPS signals tracked by a Septentrio PolaRx5 receiver with a Leica AR1203+GNSS antenna in Oberpfaffenhofen, Germany for the first GPS III satellite (solid line) and a Block IIF satellite (SVN 68, dashed line).

Even though the antenna shaping results in mostly smaller  $C/N_0$  values for GPS III-1 than for other GPS satellites, the received power is in full accord with its specification. Based on the calibrated IQ measurements obtained with the high-gain antenna, a ground-received C/A-code power of -157.9 dBW can be derived for a user observing the SVN 74 satellite at 5° elevation with an isotropic, circularly-polarized antenna. Within the inherent measurement uncertainty, this value closely matches the minimum received power specified in the GPS signal ICD (see Table 1).

More detailed information on the antenna gain pattern can be obtained from the IQ amplitude of individual L1 signal components (cf. Fig. 2) and their variation with boresight angle as obtained with the Weilheim signal monitoring facility. Results are given in Fig. 7, which shows the equivalent isotropic radiated power (EIRP) for (a) the C/A-code component, (b) the combination of L1C data, L1C pilot, P(Y)-code and their intermodulation product, and (c)

the M-code. The figure clearly shows the distinct shaping of the two antenna patterns and provides independent evidence that the M-code signal originates from a separate antenna chain. Based on the measured M-code transmit power variation over boresight a 3 dB beamwidth of approximately  $\pm 12^\circ$  can be obtained.



**Fig. 7** Variation of the L1 equivalent isotropic radiated power with boresight angle for the C/A-code (yellow), the combination of L1C, P(Y), and their intermodulation product (blue), and the M-code signal (red).

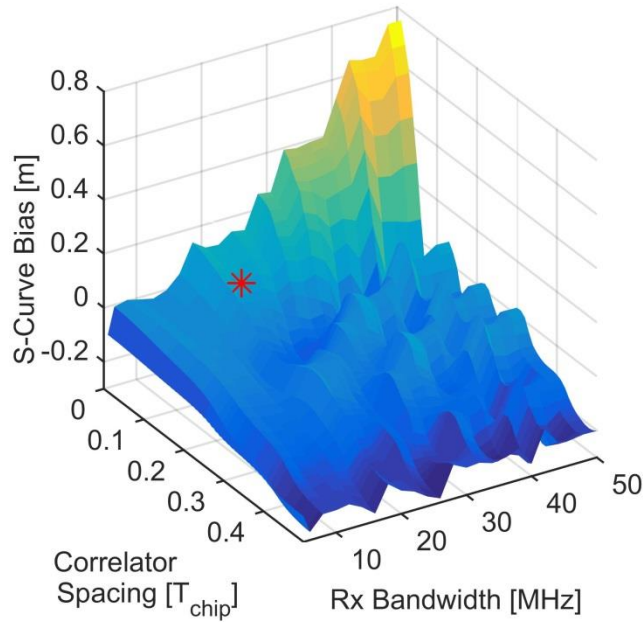
## Signal distortions and biases

Depending on the characteristics of the satellite's signal generation and transmission payload, GNSS signals are subject to distortions that show up as alterations or imperfections of an ideal chip shape. These affect the correlation process and may cause receiver dependent ranging biases. The impact of nominal signal deformations, i.e. distortions related to the design of the signal generation and transmission chain, rather than specific anomalies, is discussed in Phelts and Akos (2004) as well as Thoelet et.al. (2014) for different GNSSs.

Based on the calibrated IQ data obtained with the 30 m high-gain antenna, the signal deformations of SVN 74 can be monitored and the impact on the user range estimation can be quantified. To this end, the digitized IQ samples are correlated with an ideal replica of the respective signal using a non-coherent early-minus-late correlator for a pre-selected grid of correlator spacings and filtering bandwidths. The resulting S-curve bias (Soellner et al.

2008) describes the variation of the resulting tracking point relative to a reference configuration and is a measure of the scatter in ranging measurements obtained with different types of receivers.

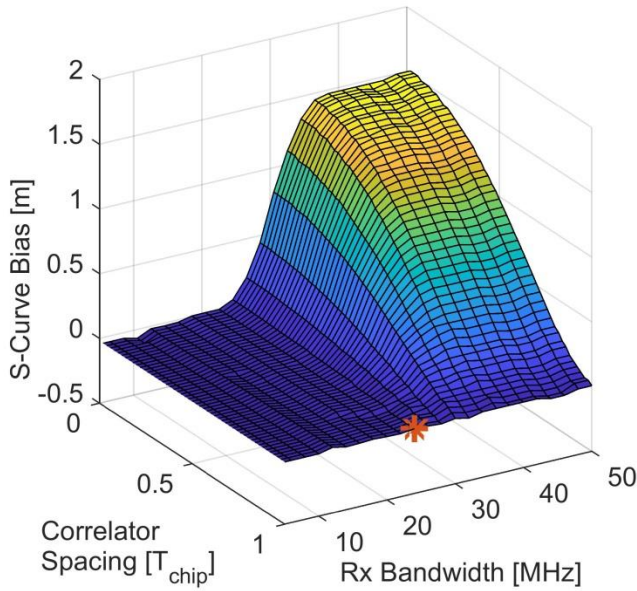
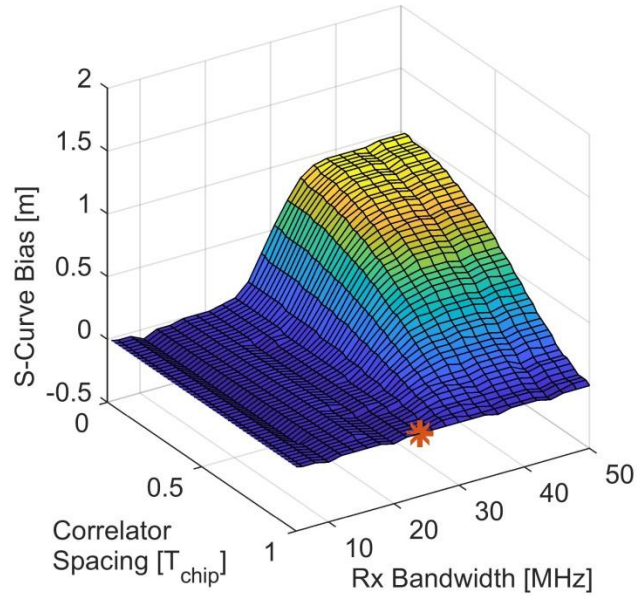
In Fig. 8 the S-curve bias for the L1C pilot signal is depicted relative to a reference receiver using a narrow correlator spacing of  $d=0.1$  chips and a two-sided band limitation of 20 MHz in accordance with recommendations in EUROCAE (2019). The result shows a maximum bias of 1 m that may arise in differential GPS applications using different receiver configurations. For settings which avoid a bandwidth higher than 25 MHz and correlator spacings of less than 0.1 chips, the resulting bias is smaller than 30 cm.



**Fig. 8** L1C code tracking bias as a function of the receiver bandwidth and correlator spacing relative to a two-sided reference bandwidth  $B=20$  MHz and correlator spacing  $d=0.1$  chips marked by a red asterisk.

Aside from the new L1C signal, S-curve biases were also derived for the L5 signal. This signal is already transmitted by the GPS IIF satellites and specifically intended for safety critical aviation applications, such as ground based augmentations systems (GBAS) and advanced receiver autonomous integrity monitoring (ARAIM). The textbook-like shape of the L5 IQ constellation diagram of SVN 74 shown in Fig. 5 gives the impression that GPS III users would benefit from lower signal distortions and consequently higher range accuracy. However, this initial impression is not supported by the comparison of S-curve biases for the GPS IIF-1 (SVN 62) and GPS III-1 (SVN74) satellites as shown in Fig. 9. The results are again based on a non-coherent discriminator and cover early-minus-late correlator spacings of  $d=0\dots1$  chip as well as receiver bandwidths of 5 to 50 MHz. For both satellites, range biases relative to a reference receiver with  $d=1$  chip and  $B=24$  MHz amount to less than a decimeter for two-sided bandwidths below 20 MHz. However, peak biases of up to 1.5 m are attained for SVN 74, which even exceed

those of the older IIF satellite. This slightly degraded performance can best be related to the overshooting during chip transitions. This shows up in small tails near the stationary points of the IQ diagram (see Fig. 5) that are more pronounced for the new GPS III-1 spacecraft than the IIF-1 satellite.



**Fig. 9** L5 code tracking bias of a non-coherent discriminator as a function of the two-sided receiver bandwidth and correlator spacing relative to  $B=24$  MHz and correlator spacing  $d=1$  chip (red star); example GPS IIF-1 (top), example GPS III-1 (bottom)

Complementary to the S-curve biases, digital distortions were investigated for the L5 signal based on the measured IQ data. Digital distortions represent systematic deviations of the chip durations from their nominal values that show up as a lead or lag of the falling or raising edge of the chip. This phenomenon and the associated tracking errors have been widely analyzed for GPS satellites and other GNSSs in view of their relevance for safety critical aviation navigation systems (Phelts and Akos 2006, Thoelet et al. 2014; Vergara et al. 2016).

**Table 2** Estimated digital distortions for GPS IIF-1 and GPS III-1.

Signal	Digital distortions [ns]	
	GPS IIF-1	GPS III-1
L5 data	5.1	0.2
L5 pilot	3.6	0.4

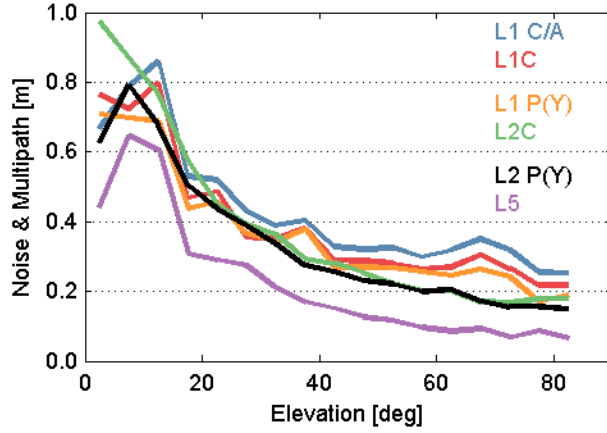
Following Vergara et al. (2016), the transfer function of the transmitter chain was determined from high-resolution IQ measurements of the L5 signal to remove all analog distortions and to recover the actual digital chip shapes. The resulting digital distortions of the data and pilot components are presented in Table 2 for SVN 74 and a GPS IIF satellite. The comparison shows that the amount of digital distortions within the L5 signal is significantly smaller for the new GPS generation and essentially negligible.

## Noise and multipath

The BOC modulation of the new L1C signal promises reduced thermal measurement noise and multipath sensitivity compared to the legacy L1 C/A code signal. Using the multipath combination (Kee and Parkinson 1994)

$$MP(p_i, \varphi_i, \varphi_j) = p_i - \varphi_i - 2 \frac{f_j^2}{f_i^2 - f_j^2} (\varphi_i - \varphi_j)$$

of pseudorange ( $p_i$ ) and carrier observations ( $\varphi_i, \varphi_j$ ) on two signal frequencies  $f_{i \neq j}$  ( $i, j = 1, 2, 5$ ), the combined noise and multipath of code measurements has been assessed for different signals at the WTZ300DEU reference station of the International GNSS Service (IGS; Johnston et al. 2017, IGS 2019). As shown in Fig. 10, a small error reduction may indeed be noted for the L1C signal in comparison to L1 C/A for a wide elevation range, even though L1C is clearly outperformed by the L5 signal with its much higher chipping rate. For the given station, L1C tracking exhibits a slightly lower thermal noise than L1 C/A tracking at identical loop bandwidths which can be related to the increased steepness of the BOC(1,1) correlator function. Further tests in diverse multipath conditions will, however, be required to assess the practical impact of the additional BOC(6,1) component in the TMBOC modulated pilot signal.



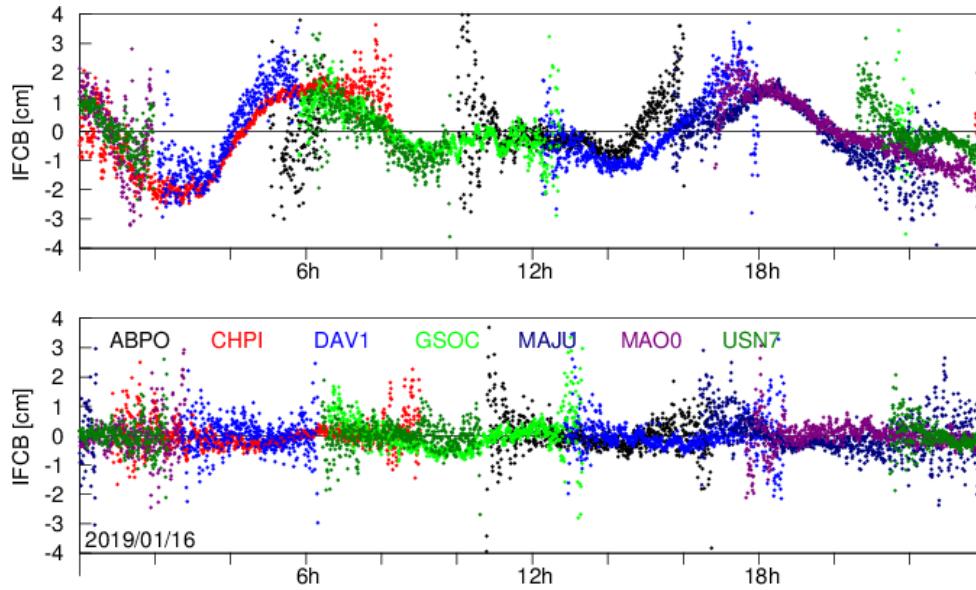
**Fig. 10** RMS pseudorange noise and multipath of SVN 74 in 5° elevation bins obtained from a Javad TRE\_G3TH receiver at the Geodetic Observatory Wettzell (WTZ300DEU, February 14-16, 2019).

### Triple carrier phase combination

Based on triple-frequency carrier phase observations  $\varphi_1$ ,  $\varphi_2$ , and  $\varphi_5$  the ionosphere- and geometry-free linear combination

$$\text{DIF}(\varphi_1, \varphi_2, \varphi_5) = \left( \frac{f_1^2}{f_1^2 - f_2^2} - \frac{f_1^2}{f_1^2 - f_5^2} \right) \varphi_1 - \left( \frac{f_2^2}{f_1^2 - f_2^2} \right) \varphi_2 + \left( \frac{f_5^2}{f_1^2 - f_5^2} \right) \varphi_5$$

can be formed. This linear combination essentially contains multipath, measurement noise, inter-frequency biases, and biases due to ambiguities. It reflects the difference of satellite clock offsets derived from ionosphere-free L1/L2 and L1/L5 carrier phase combinations and has therefore been designated as inter-frequency clock bias (IFCB) in various studies. Orbit-periodic IFCB variations with amplitudes of up to 20 cm are present for all Block IIF satellites (Montenbruck et al. 2012) and represent a continued challenge for multi-frequency GPS processing and precise point positioning applications (Pan et al. 2018, Guo and Geng 2018). The observed IFCB amplitude of the IIF satellites depends on the elevation of the Sun above the orbital plane and is smallest for high elevations.



**Fig. 11** Inter-frequency clock biases obtained from triple-frequency ionosphere- and geometry-free linear combination for the GPS Block IIF satellite SVN 68 (top) and the Block III satellite SVN 74 (bottom). Orbit-periodic variations can be seen for the Block IIF satellite but not for Block III. Station abbreviations: ABPO: Ambohimpanompo, Madagascar; CHPI: Cachoeira Paulista, Brazil; DAV1: Davis, Antarctica; GSOC: Oberpfaffenhofen, Germany; MAJU: Majuro, Marshall Islands; MAO0: Maui, USA; USN7: Washington, USA.

Fig. 11 shows an ionosphere- and geometry-free carrier phase linear combination for a GPS Block IIF satellite and the new GPS III satellite after removing a bias for each of the seven stations. Carrier phase measurements of the L1 C/A, L2 P(Y), and L5 I/Q tracking have been used (IGS 2019). Both satellites share the same orbital plane F which exhibited a Sun elevation of about  $70^\circ$  in early 2019. Due to this high elevation, the IFCB variations of the Block IIF satellite are comparatively small, but still clearly visible with a peak-to-peak amplitude of about 4 cm. The SVN 74 spacecraft, on the other hand, does not show such variations, and the triple carrier phase combination is dominated by noise and multipath at low elevations. Based on these measurements, orbit periodic IFCB variations, if present at all, are confined to less than sub-centimeter amplitudes. Further observations will be required, though, to monitor the carrier consistency throughout the annual variation of the orbital plane w.r.t. the Sun.

## Summary and conclusions

Following the launch and activation of the first GPS III satellite, the early signals transmitted in January 2019 were investigated using measurements with a high-gain dish antenna and common tracking receivers. Among the novel features of the third generation of GPS satellites is the transmission of the new L1C signal. It includes a



TMBOC(6,1,4/33) pilot signal which is interoperable with other GNSS signals in the L1 band and offers increased robustness and precision for its users. Furthermore, the replenishment of aging GPS satellites by the new GPS III generation will expand the availability of the civil L2C signals as well as the L5 signal for aviation users.

The high-gain antenna measurements clearly reveal the use of an independent transmitter chain for the military M-code signals in the L1 and L2 band. This provides increased operational flexibility and enables M-code power changes without affecting the signal power or phase relation for civil GPS. In the L1 band, a new constant-envelope multiplexing scheme, known as “weighted voting” is employed. It enables the phase coherent transmission of four user signal components, namely the L1 C/A code, the L1C data and pilot codes and the L1 P(Y)-code, on a single carrier. Other than in a traditional majority voting, the power contribution of the individual components can be freely adjusted through randomized interlacing of non-multiplexed signals.

Even though the interlacing scheme and the power ratios of the individual L1 constituents could not be investigated based on the high-gain antenna measurements due to the unknown P(Y)-code chip sequence, an L1C pilot power similar to that of the L1 C/A code signal could be confirmed from  $C/N_0$  measurements with GNSS receivers supporting L1C tracking. The observed strength of the civil L1 signals of GPS III is consistent with the specified minimum received power, but falls behind that of the GPS IIF satellites for medium to high elevations due to a notably different shaping of the transmit antenna gain pattern. However, nearly matching signal powers and antenna diagrams were found for the L2 and L5 signals of the two blocks of GPS satellites.

The use of a new digital signal generation in GPS III results in a high purity of chip transitions and IQ constellation diagrams. However, a notable overshooting can still be recognized. As a result, S-curve biases, which describe receiver-dependent variations of the tracking point and limit the achievable quality of differential code corrections are of similar (or even lightly larger) magnitude as for the past GPS IIF generation. Digital distortions, in contrast, show a remarkable reduction to sub-nanosecond level and are essentially negligible in the first GPS III satellite. Also, an excellent consistency of the L1, L2, L5 carrier can be observed with triple-frequency observations and no evidence of thermally induced biases as observed on GPS IIF satellites has been found.

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