### WASI Training V: Spectral field data – measurements

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### Illumination

Light source is the upper hemisphere

 $\theta$ : Zenith angle

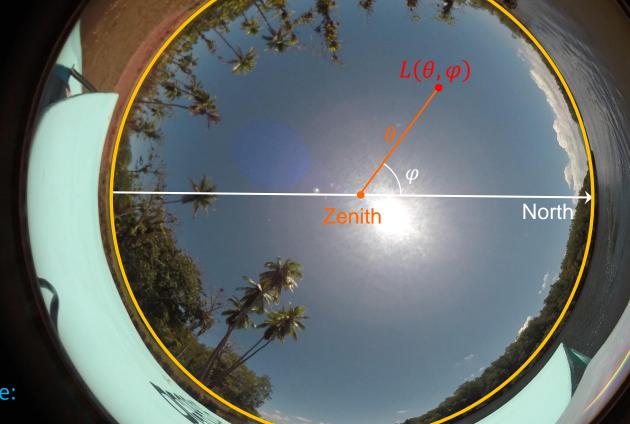
 $\varphi$ : Azimuth angle

#### Upper hemisphere:

$$\theta = 0..90^{\circ} = 0.. \pi/2$$
  
 $\varphi = 0..360^{\circ} = 0.. 2\pi$ 

#### Downwelling irradiance:

$$E_d = \int_{0}^{2\pi} \int_{0}^{\pi/2} L(\theta, \varphi) |\cos \theta| \sin \theta \, d\theta \, d\varphi$$

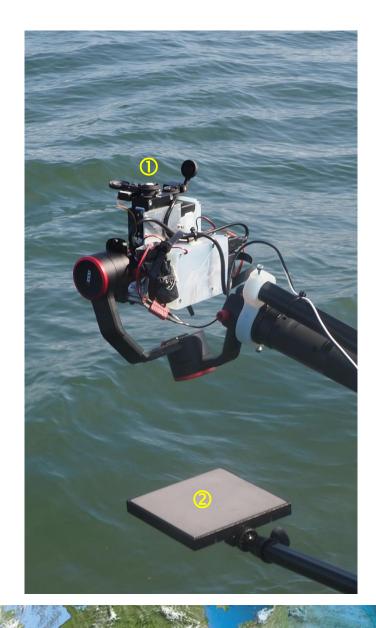


# Irradiance Measurement DLR's Ocean-Optics Sensor System (OOSS)

#### Two measurement methods

• Direct: Cosine collector ①

• Indirect: Diffusor plate ("Spectralon") ②





$$E_{d}(\lambda) = R_{E}(\lambda) \cdot (S_{E}(\lambda) - D_{E}(\lambda))$$

 $R_E(\lambda)$ : Irradiance response (from laboratory)

 $S_E(\lambda)$ : Signal of irradiance sensor [DN]

 $D_E(\lambda)$ : Dark current of irradiance sensor [DN]

#### Comments

- The angular response of  $R_E(\lambda)$  must be proportional to  $\cos\theta$  to measure  $E_d=\int_0^{2\pi}\int_0^{\pi/2}L(\theta,\varphi)\left|\cos\theta\right|\sin\theta\,\mathrm{d}\theta\,\mathrm{d}\varphi$
- It is very difficult to produce a cosine collector with a  $good cos\theta$  response
- The manufacturer Ocean Optics doesn't specify the uncertainty of its cosine collector, hence we do not trust these types of collectors to have an accurate cos characteristics
- We do not believe that our cosine collector is of "good quality" w.r.t. the cosine law





We use the cosine collector to measure the *changes*  $\Delta_E(\lambda, t)$  of the downwelling irradiance

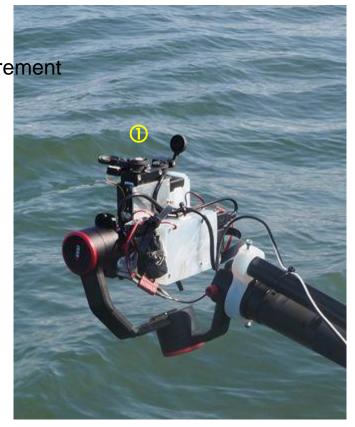
$$E_d(\lambda, t) = E_d(\lambda, t_0) \cdot (1 + \Delta_E(\lambda, t))$$

 $E_d(\lambda, t_0)$ : Irradiance at the time  $t_0$  of the reference measurement

 $E_d(\lambda, t)$ : Irradiance at a later time t

 $\Delta_E(\lambda, t)$ : Relative change of irradiance

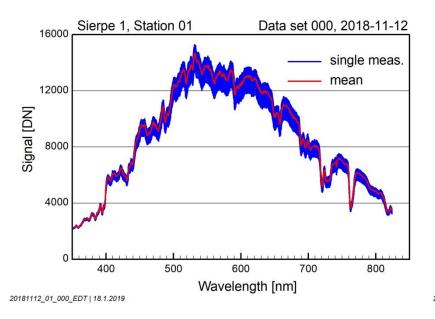
These relative measurements are not very much affected by imperfect cos charactics of the sensor head

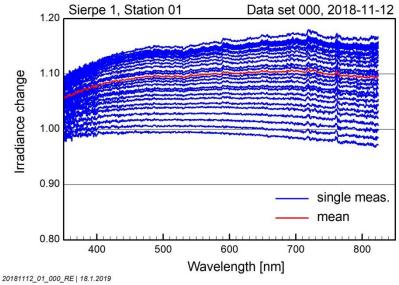




Example of irradiance change under unfavourable illumination conditions (broken clouds)

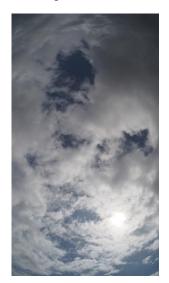


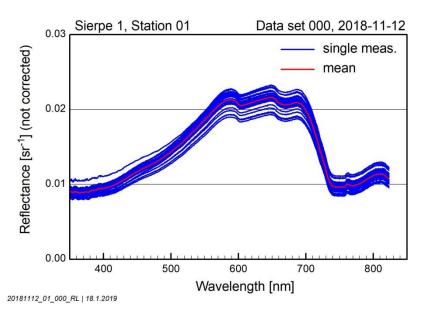


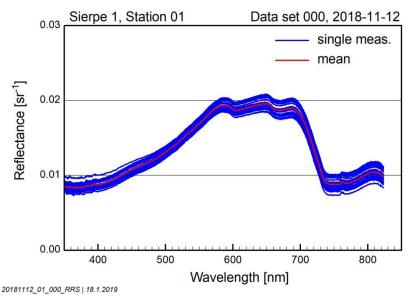




Example of reflectance measurements and their correction under unfavourable illumination conditions (broken clouds)







uncorrected reflectance

reflectance corrected using cosine collector



# Irradiance Measurement Diffusor plate method

$$L_r(\lambda) = \rho_{plate} \cdot R_{Lr}(\lambda) \cdot (S_{Lr}(\lambda) - D_{Lr}(\lambda))$$
  
$$E_d(\lambda) = \pi \cdot L_r(\lambda)$$

 $L_r(\lambda)$ : Radiance of diffusor plate

 $\rho_{plate}$ : Reflectance of plate (from laboratory)

 $R_{Lr}(\lambda)$ : Response of L sensor (from laboratory)

 $S_{Lr}(\lambda)$ : Signal of L sensor during reference meas. [DN]

 $D_E(\lambda)$ : Dark current of L sensor during ref. meas. [DN]

#### Comment

Spectralon plates are known to have good cosine characteristics





# Irradiance Measurement Diffusor plate method

#### Main advantage of this method:

 $E_d(\lambda)$  is measured with the same instrument as  $L_u(\lambda)$  of the target

- ➤ No spectral artifacts from instrument differences
- Sensor response must not be known for deriving reflectance





## Irradiance Measurement Diffusor plate method

#### Recommendations

Following Castagna et al. (2019)

- ➤ Chose viewing angle close to 0° for gray plate
- ➤ Chose sensor distance > 20 cm
- > Ensure level orientation: trained operator or gimble mount
- > Ensure that sensor field of view is inside plate
- ➤ Minimize impact of operator: dark clothing or plate at sufficient distance
- ➤ Select position on the boat which minimizes impact of surrounding structures
- ➤ Record at least 10 sequential measurements
- ➤ Flag stations with a coefficient of variation > 6 %

Best results are obtained for sun zenith angles between 20° and 60°, stable illumination and up to moderate sea-state

