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Title: Cost-effective fabrication of polycrystalline TiO<sub>2</sub> with tunable n/p conductivity for selective hydrogen monitoring

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Abstract: In this report, we demonstrate a simple and cost-effective strategy to prepare polycrystalline rutile TiO<sub>2</sub> based gas sensors with tunable n/p type conductivity inversion depending on gas concentration, operating temperature and applied voltage. The effect of surface modification by Ag and Ni thin film on structural, morphological and gas sensor characteristics is studied in detail. The sensors show excellent sensing performance in terms of sensitivity (~25% for 0.1 vol. % H<sub>2</sub> diluted in technical air), selectivity (selectivity factor for 0.1 vol. % H<sub>2</sub> is about ~24 against NH<sub>3</sub>, CH<sub>4</sub>, NO<sub>2</sub> and ~8 for CO), stability (both long-term and short-term) and reaction times (~0.7 min for 0.1 vol. % H<sub>2</sub>). The aforementioned performance is recorded at 300 °C with applied voltage of 0.1 V. Excluding the power consumption of sensor heater (typically ~5×10<sup>-5</sup> watt), this applied voltage 0.1 V can reduce the power consumption to 3×10<sup>-10</sup> watt. We found a critical point, defined with threshold-concentration (C<sub>Th</sub>), threshold-temperature (T<sub>Th</sub>) and critical-voltage (V<sub>C</sub>), at which the conductivity inverses from one kind to another, something intriguing to novel sensing phenomena that can be exploited to tailor the selectivity of the sensors. A physical-chemical sensing model is presented to understand the aforesaid peculiar occurrence.

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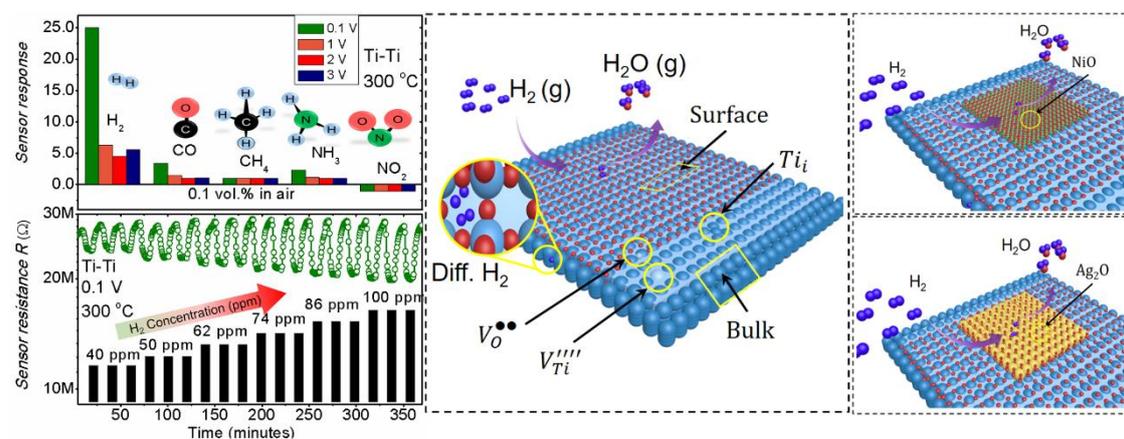
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## ABSTRACT

In this report, we demonstrate a simple and cost-effective strategy to prepare polycrystalline rutile  $\text{TiO}_2$  based gas sensors with tunable n/p type conductivity inversion depending on gas concentration, operating temperature and applied voltage. The effect of surface modification by Ag and Ni thin film on structural, morphological and gas sensor characteristics is studied in detail. The sensors show excellent sensing performance in terms of sensitivity ( $\sim 25\%$  for 0.1 vol. %  $\text{H}_2$  diluted in technical air), selectivity (selectivity factor for 0.1 vol. %  $\text{H}_2$  is about  $\sim 24$  against  $\text{NH}_3$ ,  $\text{CH}_4$ ,  $\text{NO}_2$  and  $\sim 8$  for  $\text{CO}$ ), stability (both long-term and short-term) and reaction times ( $\sim 0.7$  min for 0.1 vol. %  $\text{H}_2$ ). The aforementioned performance is recorded at  $300^\circ\text{C}$  with applied voltage of 0.1 V. Excluding the power consumption of sensor heater (typically  $\sim 5 \times 10^{-5}$  watt), this applied voltage 0.1 V can reduce the power consumption to  $3 \times 10^{-10}$  watt. We found a critical point, defined with threshold-concentration ( $C_{\text{Th}}$ ), threshold-temperature ( $T_{\text{Th}}$ ) and critical-voltage ( $V_C$ ), at which the conductivity inverses from one kind to another, something intriguing to novel sensing phenomena that can be exploited to tailor the selectivity of the sensors. A physical-chemical sensing model is presented to understand the aforesaid peculiar occurrence.



# Cost-effective fabrication of polycrystalline TiO<sub>2</sub> with tunable n/p conductivity for selective hydrogen monitoring

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## 1. Introduction

Unlike the previous decades, in the last few years, there is a rapid rising demand on low-cost, highly sensitive, and selective gas monitoring smart systems to be utilized in various modern industries. Chemical sensors based on nanostructured metal oxide semiconductors (MOX) offer great opportunity to meet this demand as a consequence of their superior sensing properties in detecting and monitoring of various toxic and explosive gases [1-3]. Concomitantly, besides the selectivity and operating temperature issues, the recent discovery of n-p-n type conductivity transition with gas exposure has triggered new matter to be addressed. Recently, many articles have reported on this transition behavior from n- to p-type conductivity or the opposite, for pure MOX, doped MOX and for its composites [4-11]. The explanation of conductivity transition is a matter of debate in recent times since the factors causing this phenomenon are manifold, such as temperature [4-7], gas concentration [4-9] composition [4, 10], and impurity concentration [11, 12]. However, there is no doubt that the conductivity transition is related to the surface charge effect, leading to the transformation of the type of dominant charge carriers [13-14].

Titanium dioxide or titania (TiO<sub>2</sub>) belongs to the MOX group and exhibit not only excellent sensitivity, but stability even in harsh conditions and elevated temperatures [15-18]. It has already been experimentally proved that bulk TiO<sub>2</sub>, in general, exhibits n-type conductivity with electrons being dominant surface charge carriers and having ionized donors at room temperature with the density of electrons  $[e^-]$  equals the density of donors  $N_D$  ( $[e^-] = N_D = 10^{17}-10^{20} \text{ cm}^{-3}$ ), small effective mass  $m^*$  ( $\sim 0.1-0.4 m_e$ ) and mobility in the range  $\mu=1-50 \text{ cm}^2/\text{Vs}$ . Depending on the circumstances, many factors can be considered to influence the charge carrier density ( $[e^-]\sim 10^{16}-10^{18} \text{ cm}^{-3}$ ) and the mobility value ( $\mu\sim 10^2-10^3 \text{ cm}^2/\text{Vs}$ ), including grain boundaries, ionized impurities and electron-phonon interactions. For example, the grain boundaries in polycrystalline TiO<sub>2</sub> contain very high densities of surface states that results in depleted grains and capture (or scatter) free charge carriers to generate a potential barrier ( $\sim eV_s$ ). On the contrary, TiO<sub>2</sub> can also be classified as p-type semiconductor due to dominant counterpart surface charge carriers, the holes. For n-type TiO<sub>2</sub> based gas sensors, the resistance value decreases when the surface is exposed to reducing gases (e.g. H<sub>2</sub>, CO) as conversely occurs for oxidizing gases (e.g. NO<sub>2</sub>, O<sub>2</sub>).

The authors have already published several reports on improved hydrogen gas sensing properties of TiO<sub>2</sub> coatings even at room temperature through the control of electrode

configuration [19-21]. However, there are only limited reports [10-11] in the literature on the conductivity transition behaviour of TiO<sub>2</sub>. Nanostructured TiO<sub>2</sub> was facily fabricated via simple thermal oxidation of Ti-discs. In addition, very thin (~ 30 nm) layer of Ni and Ag was sputtered on the top surface prior to thermal oxidation to achieve differences in morphology and conductivity. To authors' best knowledge, for the first time, in this report the factors that influence the conductivity change of rutile TiO<sub>2</sub> are explored. From a fundamental viewpoint, the dependence of the conductivity on the operational parameters can pose serious limitations to the practical exploitation of the proposed sensor. In addition, the work provides a conceptual advance in the field of semiconductor metal oxide gas sensors, where we demonstrate the inherent n/p type electrical conductivity inversion of TiO<sub>2</sub> with gas exposure by engineering the surface charge carriers. The proposed strategy in this report can make significant impact on the development of future smart gas sensors and should be applicable to other materials in this area.

## 2. Experimental

### 2.1 Fabrication of gas sensors

As a raw material, high purity Ti-discs (99.9% purity) having diameter of  $\varnothing=15$  mm and thickness of 1 mm was purchased from BaoTi Group Co. Ltd. At first, the discs were washed using ultrasonic bath in sequence in acetone, ethanol, and deionized (DI) water for each 15 min, respectively, to remove oil and subsequently dried at 90 °C for 5 min. Thereafter, both sides of Ti-discs were polished for 20 min using the abrasive metallographic paper from type 0# (W40) to 05# (W7) until the surface become highly smooth. After continuous polishing for 10 min on the polishing machine, the Ti-discs were repeatedly washed again using ultrasonic oscillation for 10 min in acetone, ethanol and DI water bath, respectively, in order to remove any available surface impurities. Afterwards, thin films ~ 30 nm of Ti, Ni, and Ag were deposited on the dried Ti-discs using RF magnetron sputtering (MSIB-6000 magnetron sputtering/ion beam sputtering machine from Beijing Chuangweina Tech. Co. Ltd) by means of controlling power and time accurately. Finally, nanostructured TiO<sub>2</sub> films modified with Ti, Ni, and Ag oxides were obtained via thermal oxidation under static air condition. During oxidation process the samples were placed in porcelain combustion boats in tube furnace OTF-1200X tubular furnace (Hefei Kejing Materials Technology Co. Ltd) and the temperature was increased to 1000 °C with heating rate of 10 °C/min. The furnace temperature under the mentioned conditions was kept at 1000 °C for 1 h and subsequently cooled down naturally to room temperature with a slow rate.

The interdigitated electrodes with a spacing of 10  $\mu$ m were fabricated by photolithography method. To start with, the lift-off photoresist (35E and AZ 5214E) was deposited by spin coating on the surface of oxidized TiO<sub>2</sub>, followed by the exposure to 200 W Hg discharge lamp through a mask with comb-like structures. Then platinum layer of 20 nm thickness was deposited by DC magnetron sputtering process. In a typical DC magnetron sputtering of platinum process, a voltage source Swinstek GPR – 60H15D (Cathode voltage –  $U_k = 380$  V with current limit  $I = 80$  mA) was used, the distance between target and substrate was kept at 4 cm, the base pressure was  $\sim 10^{-3}$  Pa. The sputtering process was conducted in a closed vacuum chamber in continuous argon flow mode at working pressure of 0.5 Pa. The growth rate of Pt layer with these parameters was  $\sim 0.5$  nm/s. Eventually, the samples were put in

acetone to remove photoresist. The detailed thermal oxidation process and the sensor fabrication technique have been reported in our previous studies elsewhere [22-24]. The schematic diagram of overall preparation steps is shown in Fig. 1.

## 2.2 Characterization

The crystal structure of the sensing films was confirmed by using Ultima IV X-ray diffraction (XRD) instrument from Japan with Cu K $\alpha$  radiation ( $\lambda = 0.15406$  nm) in the angle range of 10–80° at a scanning rate 5° min<sup>-1</sup>. The MDI JADE 5.0 software was used for XRD pattern processing and determination of crystal phases in each sample by comparing the obtained peaks with reference Joint Committee on Powder Diffraction Standards (JCPDS) cards. The surface morphology was observed by Hitachi S-4700 scanning electron microscopy (SEM) from Japan. The sensing films structural details were further characterized by JEM-2100F transmission electron microscope (TEM, JEOL Ltd. Japan) operating at an accelerating voltage of 200 kV, equipped with Bruker energy dispersive spectrometer (EDS, from Germany).

The hydrogen sensing measurements were carried out using a self-established gas sensing measurement unit (Functional Materials and Chemical Sensor Lab, FuMS). With the aid of precisely controlled gas flow by mass flow controllers (MFC) from Vögtlin Instruments GmbH (GSC-A5SA-BB22), the gases flow to the pre-mixing cylindrical chamber of volume ~200 cm<sup>3</sup> simultaneously. The hydrogen concentrations were varied in the range of 40–1000 ppm by means of adjusting the flow ratio of 1000 ppm hydrogen (background technical air) and technical air. After passing 3 meters long gas pipeline with a diameter of  $\varnothing=6$  mm, the mixing gases reaches the reaction chamber of volume ~350 cm<sup>3</sup> in the OTF-1200X tubular furnace (Hefei Kejing Materials Technology Co. Ltd), which determines the operating temperature of gas sensors. The model 6482 Dual-Channel Picoammeter/Voltage Source (Keithley, Tektronix US) was applied to measure the dynamic changes in the resistance/current of the sensor. The measurement unit enables to perform gas sensing measurement under different operating temperatures (up to ~1200 °C), applied voltages ( $\pm 30$  V) and atmosphere conditions. All the included instruments and experiment processes were accurately controlled by the independent research and development of in-house software based on LabVIEW program (Fig. S1 in ESI). The sensor response  $SR=R_0/R_{H_2}$  ( $R_0$  is the stabilized resistance in dry technical air and  $R_{H_2}$  is the saturated resistance in specific hydrogen concentration), and response (recovery) time, defined as and 90% change in the stable baseline (saturated gas) resistance, were estimated for the response analysis.

## 3. Results and Discussion

### 3.1 Phase and Crystal Structure

Notwithstanding the commercially available metallic titanium (Ti) discs and/or sheets are mainly characterized by the hexagonal closed packed alpha titanium ( $\alpha$ -Ti) and body centered cubic beta titanium ( $\beta$ -Ti) phase, the oxides of titanium (e.g. TiO<sub>2</sub>) are stamped as tetragonal anatase (A) and rutile (R), and orthorhombic brookite (B) phase. The XRD analyses, shown in Fig. 2, were performed to determine the constituent phases in each sample. As indicated by black filled circles in Fig. 2a, all the peaks at the XRD diffractogram

of as received (un-oxidized) Ti-disc (orange curve labelled as T0) were identified by comparing with standard powder diffraction card JCPD-44-1294, which shows the dominance of  $\alpha$ -Ti phase with no other peak from  $\beta$ -Ti (JCPDS 44-1288) phase. The XRD diffractogram of the sample oxidized at relatively low temperature 600 °C (blue curve labelled as T6) still shows the dominant presence of  $\alpha$ -Ti phase due to the exceeding penetration of X-rays through un-oxidized bulk of the disc. Very weak peak of rutile R (110) phase is appeared, which indicates very small fraction of initial rutile crystal phase formation in the mostly  $\alpha$ -Ti phase disc. Upon oxidation, most probably due to the rise of surface titanium oxides the lattice parameters also increase yielding slight shift of  $\alpha$ -Ti peaks to the right. The splitting of peaks at 38.45° and 70.69° is due to the formation of other titanium oxide (such as  $\text{TiO}_x$ ) phases on the surface.

It appears that the degree of rutile crystallinity increases with oxidizing temperature as the intensity of  $\alpha$ -Ti phase decreases. At higher oxidation temperatures 1000 °C (black curve labelled as T10), the  $\alpha$ -Ti phase nearly disappears and transforms to rutile phase. However, the rutile phase is anisotropic (polycrystalline tetragonal) in nature, with  $P42/mnm$  space group and lattice constants  $a=b=4.593$  Å and  $c = 2.959$  Å, as its strong diffraction peaks at  $2\theta$  [°] = 27.44, 36.11, 54.39 and 56.71 are indexed to rutile  $\text{TiO}_2$  phases (110), (101), (211) and (220) (JCPDS file No. 21-1276). There are low intensity peaks at 41.36° (111) and 44.19° (210), while the strongest one is (110) followed by (211).

The Fig. 2b demonstrates the XRD diffractograms of oxidized (at 1000 °C)  $\text{TiO}_2$  modified with 30 nm Ti (black curve labelled as TO), Ni (red curve labelled as TNi) and Ag (olive green curve labelled as TAg) layers. The results exhibit peak intensity reduction and shift (towards right) of each rutile crystal; see the inset of R (110) peak in each curve of Fig. 2b. The peak intensity of R (110) crystal for un-modified  $\text{TiO}_2$  is higher followed by  $\text{TiO}_2$  modified with Ni and Ag respectively. On the other hand, the right shift of the peaks increases with Ni and Ag modifications. A slight increase in the peak intensity of TNi was found for R (211). After careful consideration of instrumental broadening, the grain size  $D_g$  of the rutile crystal for each sample was calculated by using standard Scherer formula  $D_g = 0.9\lambda/B\cos\theta$ , where  $\lambda = 0.15406$  nm, B is described by the width of relevant diffraction peak profile at maximum height FWHM (in radians) and  $\theta$  is the Bragg angle (in radians). For the most intense peak R (110), the grain size of TO was nearly same as that of TNi ~ 60 nm, while for TAg the grain size was small  $D_g = \sim 49$  nm. In addition, for the samples TO, TNi and TAg, the grain size decreases for other rutile R (101)/(211) crystals, i.e.  $D_g = \sim 78/55$ ,  $\sim 57/48$  and  $\sim 53/39$  nm.

To sum up, the un-annealed Ti-discs were metallic with only  $\alpha$ -Ti phase. Under oxidizing conditions (in the present case static air) and high temperature treatment (in the present case at 1000 °C) the Ti-discs oxidize completely to  $\text{TiO}_2$ . The oxidized  $\text{TiO}_2$  discs (TO, TNi and TAg) are polycrystalline in nature with a grain size in the range of ~ 39–78 nm. From the above analysis, it is inferred that the oxidized discs contains randomly oriented nano-grains of polycrystalline film. These findings, the reduced peak intensity as well as right shift, indicate the successful surface modification with oxides of Ni and Ag (i.e. NiO and  $\text{Ag}_2\text{O}$ ). Due to anisotropic (polycrystalline) nature of the oxidized discs it is reasonable to assume that the peak shift (or mismatch  $2\theta$  values from reference database PDF cards) and intensity reduction are mainly caused by strain produced by defects in rutile crystals due to surface modification by Ti, Ni, and Ag thin coating and thus serve only for qualitative comparison

[25]. Moreover, it is remarkable to note that the  $\alpha$ -Ti phase transforms into rutile phase without even going through anatase phase, the reason for which is unknown to the authors.

### 3.2 Microstructure and compositional analyses

On contrary, from the SEM micrographs in Fig. 3, it is evident that relatively large polycrystalline  $\text{TiO}_2$  crystals in the submicron size ranging from  $\sim 0.2$  to  $2 \mu\text{m}$  are formed randomly after oxidizing Ti-dics at  $1000^\circ\text{C}$  in oxygen rich environment (i.e. static air). The contrasting values of  $\text{TiO}_2$  grains from XRD means the volume where the crystalline structure is intact and hence shows size of coherent domain. This happens when the grains contain defects such as dislocations. Thus one would say that the values obtained from SEM/TEM micrographs are more authentic. The surface of  $\text{TiO}_2@/\text{TiO}_2$  exhibits a periodically repeating (connected through their grain boundaries) submicron grains chain having an average size of  $\sim 600 \text{ nm}$ , Fig. 3a. The surface of these well-organized submicron grains contains several  $\text{TiO}_2$  nano-crystals (average size well below  $100 \text{ nm}$ ) which grew courtesy of oxidized  $\sim 30 \text{ nm}$  thin Ti coating, see the inset Fig. 3a-bottom. In addition, the EDX analysis and elemental mapping show a  $\text{TiO}_2$  elemental composition near to stoichiometric order.

In comparison with  $\text{TiO}_2@/\text{TiO}_2$  surface, the  $\text{TiO}_2@/\text{NiO}$  grains in Fig. 3b show extensive transformation in morphology and form steps-like terraces which grow along prismatic  $\text{TiO}_2$  (100) rutile ledges. Albeit no NiO peaks were observed from above XRD analysis, the authors believe that such transformation is caused by  $\sim 30 \text{ nm}$  Ni coating on Ti-disc surface. Interestingly to note that the effective ionic radius of  $\text{Ag}^+$  ( $r_{\text{ion}} \sim 1.21 \text{ \AA}$ ) is twice of that  $\text{Ti}^{4+}$  ( $r_{\text{ion}} \sim 0.60 \text{ \AA}$ ), so the substitution of  $\text{Ti}^{4+}$  by  $\text{Ag}^+$  is improbable as it would result in the expansion of  $\text{TiO}_2$  lattice constants due to large ionic radii difference, which is not attested by our XRD data. On the other hand, the ionic radii of  $\text{Ni}^{2+}$  ( $r_{\text{ion}} \sim 0.69 \text{ \AA}$ ) does not differ strikingly, so  $\text{Ni}^{2+}$  incorporation into  $\text{TiO}_2$  lattice is highly possible, as lattice constants slightly changed for this case. In addition, due to the above mentioned fact, Ni modifies the surface significantly to give prominent step-like structure. By averaging the heights and widths of ten steps, the cumulative steps height and width is found to be  $\sim 10$  and  $\sim 160 \text{ nm}$  respectively. The values of steps heights ( $\sim 10 \text{ nm}$ ) differ from the previously reported mono-steps heights values ( $\sim 0.23 \text{ nm}$ ) [26], while the values of heights do not vary significantly. The reason for such differences may be related to the selection of single crystal  $\text{TiO}_2$  wafer, wet chemical treatment and high-temperature oxidation under continuous oxygen flow [27]. Apparently no oxide nano-particles (either  $\text{TiO}_2$  or NiO) on the surface was observed; however, the EDS mapping in the Fig. 3b-bottom shows the presence of Ni element ( $\sim 0.86 \text{ at. \%}$ ).

There appears to be only a few places on  $\text{TiO}_2@/\text{AgO}$  surfaces where such steps-like terraces are formed. This suggests that the bulk-terminated rutile  $\text{TiO}_2$  surface consists of polycrystalline submicron grains as shown in Fig. 3c. The micro-facets are also cleaved by occasional appearance of submicron rod like structures between the adjacent grains. The surface of the micro-facets also contain nanoparticles, to authors these refer to the oxides of silver yields during oxidation of  $\sim 30 \text{ nm}$  Ag coating on Ti-disc, as suggested by the elemental mapping by EDS analysis, which confirms the presence of  $0.95 \text{ at. \% Ag}$ , see Fig. 3c-bottom. The SEM results are in agreement with XRD results, and are further discussed and confirmed via TEM analysis below.

As observed in TEM images Fig. 4a-c, the average size of  $\text{TiO}_2@\text{TiO}_2$  (~ 600 nm) is observed to be smaller than  $\text{TiO}_2@\text{NiO}$  (~2  $\mu\text{m}$ ), and  $\text{TiO}_2@\text{AgO}$  (~1.8  $\mu\text{m}$ ). Since,  $\text{Ni}^{2+}$  may replace  $\text{Ti}^{4+}$ , so its oxides were not fully seen in TEM micrographs, on the other hand, the traces of  $\text{Ag}_2\text{O}$  deposited on  $\text{TiO}_2$  are already evident from TEM micrographs shown in Fig. S2 (ESI) as due to difference in contrast the black granular spots are superimposed in the background of large  $\text{TiO}_2$  grains. In all samples, the bulk of the  $\text{TiO}_2$  grains is characterized by R (110), R (101) and R (210) planes that correspond to d-values  $d$  [ $\text{\AA}$ ] ~3.25, 2.45 and 2.05  $\text{\AA}$  respectively, see middle Fig 4a-c. Despite being highly stable, R (110) phase can undergo reconstruction depending on the degree of oxidizing temperature and environment [28]. In current case, nevertheless, the authors found the side faces of the rutile grains are mainly R (200) and R (111) corresponding to the d-values  $d$  [ $\text{\AA}$ ] ~2.28 and 2.19 respectively, see middle Fig 4a-c. The XRD peak intensity of R (111) of  $\text{TiO}_2@\text{NiO}$  has become sharper than that of un-modified sample, which suggests that the lattice fringes parallel to the side surface should be assigned to R (111) planes. Since these phases are not stable at higher temperature, so it is reasonable to assume hereinafter that the step-like structure appears on these faces. Despite that, as expected the selected area electron diffraction (SAED) pattern of  $\text{TiO}_2@\text{TiO}_2$  sample shows relatively similar size rutile facets surface distribution. The SAED patterns of  $\text{TiO}_2@\text{NiO}$  and  $\text{TiO}_2@\text{AgO}$  indicate the formation some occasional large rutile crystal embedded in overall polycrystalline material, Fig. 4a-c on the right. The SAED pattern of  $\text{TiO}_2@\text{TiO}_2$  is characterized by rings with occasional bright spots, where rings for  $\text{TiO}_2@\text{NiO}$  and  $\text{TiO}_2@\text{AgO}$  disappear nearly completely. This matches perfectly with SEM morphology where for  $\text{TiO}_2@\text{AgO}$  some rods of submicron dimension appeared on the surface (Fig. 3c). However, by measuring the d-values from SAED patterns, the rutile crystals indexed from the above XRD analysis were confirmed.

### 3.3 Electrical measurements and gas sensor tests

Based on surface adsorption, charge transfer and subsequent desorption of gas species, the sensing mechanism of  $\text{TiO}_2$ -based gas sensors as well as other MOX, such as  $\text{SnO}_2$ ,  $\text{ZnO}$ , and  $\text{In}_2\text{O}_3$  and so on is well established. Sensing at nano-scale is still challenging, since the control of critical defects play a great role. Moreover, the factors related to measurement conditions, such as operating temperature, applied voltage and specific gas concentration range, to conduct gas sensor tests can definitely affect the performance of the final device in real life applications. Most of the scientific papers, now-a-days, focus only on the laboratory based performance of these gas sensors. The factors that may lead to the false readings of the gas sensors are seldom reported. Towards this end, the authors found that the significant role of these factors is not only influence the final performance of a gas sensor, but also the inversion of the conductivity (n/p) type.

**Sensor performance:** After mounting the samples and prior to exploring the gas sensing characteristics, we kept the measuring chamber heated at particular operating temperature (200 – 400  $^\circ\text{C}$ ) for at least 1 hour to achieve the chemical equilibrium on the sensor surface. Depending on the operating temperature, during this essential warm-up period the oxygen species ( $\text{O}_2^-$ ,  $\text{O}^-$ , and  $\text{O}^{2-}$ ) from air may be adsorbed on the sensor surface and subsequently diffused at the grain boundaries. To begin with, we firstly consider the performance of our sensor. We performed the gas sensor tests in operating temperature range of 200–400  $^\circ\text{C}$  with variable applied voltage range of 0.05–5 V for various reducing ( $\text{H}_2$ ,  $\text{CO}$ ,  $\text{NH}_3$ , and  $\text{CH}_4$ ) and

oxidizing ( $\text{NO}_2$ ) gases of 0.1 vol. % diluted in air. The sensors demonstrate high selectivity to  $\text{H}_2$  gas in the presence of all these gases at all applied voltages under the same given experimental conditions and gas concentrations (Fig 5a). The value of selectivity factor ( $S_F$ ), estimated as the response ratio of  $\text{H}_2$  against other gases (1000 ppm), is circa constant  $S_F \sim 24$  ( $S_F = S_{R,\text{H}_2}$ ) at 0.1 V against all gases except for CO where  $S_F$  drops to  $\sim 8$ . Meanwhile, the values of  $S_F$  drops significantly with increasing applied voltage (for instant at 1, 2 and 3 V the respective values of  $S_F$  are  $\sim 7$ , 4 and 6) having the same ratio  $S_F = S_{R,\text{H}_2}$ . The dynamic response of the sensors to above mentioned gases are shown in supplementary data (Fig. S3 in ESI). Despite our sensors show reproducible responses at all above mentioned parameters, it is found that the best operating temperature and applied voltage are 300 °C and 0.1 volt respectively. In combination with thermal activation energy, the influence of operating temperature and applied voltage will be discussed later in this section.

The typical sequential dynamic responses of Ti-Ti sensors measured at 300 °C with 0.1 V for the  $\text{H}_2$  gas concentrations ranging from 40 to 100 ppm are shown in Fig. 5b. While the responses at 200 and 300 °C with 2 V are shown in Fig. S4 of ESI. As noticeable, at 0.1 V the Ti-Ti sensors show n-type semiconducting behaviour (i.e. decrease of resistance with reducing  $\text{H}_2$  gas) with stable baseline resistance and fully reversible responses (e.g.,  $S_R \sim 1.5$ ) for each concentration (e.g., 40 ppm). In comparison to Ti-Ti samples, the responses of Ti-Ag and Ti-Ni samples for high  $\text{H}_2$  concentrations reduced, however; for low concentrations (e.g., 40 ppm) the responses improved (e.g.,  $S_R \sim 1.9$  and  $S_R \sim 4.8$  for Ti-Ag and Ti-Ni respectively) with 0.1 V (see Fig. S5 in ESI). For further evaluation we plotted the sensor responses ( $R_0/R_g$ ) against each corresponding  $\text{H}_2$  concentrations in the inset of Fig. 5b. For low concentrations (below 100 ppm) the sensor response increases almost linearly with the  $\text{H}_2$  concentration instead of following the power law dependency: that is  $R_0/R_g \sim K_{\text{H}_2} C_{\text{H}_2}^m$ , where “ $K_{\text{H}_2}$ ” is a response constant to  $\text{H}_2$  and “ $m$ ” is a coefficient of power law [35]. At other temperatures (200 °C and/or 400 °C) the sensor response is rather low, so it tends to saturate at certain increasing  $\text{H}_2$  concentrations (e.g., 300 ppm), see Fig. S6 of ESI. And the comparison of the current work with previous works was shown in Table 1.

The short-term (i.e. repeatability) and long-term (i.e. reproducibility) stability of the sensors were checked to determine the surface poisoning effect that may lead to drift in the sensor signal and false measurements. The sensors suffering from surface poisoning need frequent calibration and are highly unsuitable for practical application. The short-term stability was confirmed by recording the repeating gas sensing measurements for a specific gas at least three times under the same experimental conditions (Fig. 5c). On the other hand, the long term stability was confirmed by the sensor tests performed with the specific time interval during which the sensors were kept in open air environment. The long-term stability tests are shown in Fig. 5d. The time interval between successive measurements in the figure is 1, 2, 14 and 120 day(s) respectively. As depicted in Fig. 5c, the sensor response after several months maintained the same reading level to all respective gas concentrations. For the application point of view, the performance of such sensor is extremely suitable where the sensor device can be placed near the muffler of the exhaust engine to monitor the hydrogen leakage.

In addition, it is highly important to estimate the response ( $\tau_{Res}$ ) and recovery ( $\tau_{Rec}$ ) times of a specific gas sensor. Here, the values of  $\tau_{Res}$  and  $\tau_{Rec}$  are specified as the necessary time to reach 90% of the saturated resistance value in the gas and 90% of the recovery to the initial baseline resistance value, respectively. The estimated values of  $\tau_{Res}$  and  $\tau_{Rec}$  as a function of

hydrogen concentration  $C_{H_2}$  (ppm) in Fig. 5d indicate asymmetrical behaviour. This means, the values of  $\tau_{Res}$  becomes shorter as  $H_2$  concentration,  $C_{H_2}$  increases, in turn, the values of  $\tau_{Rec}$  becomes longer. For instance, for Ti-Ti sample at 200 °C under 2 V biasing, the values of  $\tau_{Res}$  ( $\tau_{Rec}$ ) decrease (increase) from 2.2 to 0.7 (0.8 to 3.4) towards respective increasing hydrogen gas concentrations  $C_{H_2} \sim 40 - 1000$  ppm, respectively. Here relatively high estimated values of  $\tau_{Res}$  and  $\tau_{Rec}$  are found than those mentioned in some previous reports [36]. The longer reaction times in our experiments can be explained on the basis of delay caused by gas evolution in gas mixing chamber and its further transportation through  $\sim 3$  m long piping with an inner diameter of  $\varnothing \sim 6$  mm before it reaches to sensor surface. If an ideal gas mixing process is considered where  $C(t)$  represents the dynamic time dependent gas concentration,  $C_{mix}$  as the gas mixture concentration flowing towards the chamber and  $\tau_{mix}$  ( $\sim 0.87$  min) as the time constant given by ratio of the test chamber volume ( $\sim 350$  cm<sup>3</sup>) to the flow rate (400 sccm), then the gas evolution in the measurement chamber can be defined by the following differential equation:

$$\frac{dC(t)}{dt} = -\frac{C(t)-C_{mix}}{\tau_{mix}} \quad 1$$

By applying the above mentioned parameters to the equation 1, the solution is given by the equation below:

$$C(t) = C_{mix} - C_{mix} e^{-t/\tau_{mix}} \quad 2$$

Equation 2 gives the time-evolution of the actual concentration in the chamber after the ON/OFF cycle of the gas, e.g., for 1000 ppm  $H_2$  the gas evolution is  $\sim 1000 - 1000 \times e^{-0.015}$ . To further elaborate the response vs. recovery time asymmetry, we simulated the typical gas evolution process by using equation 2 for long period (30 minutes) and short period (10 minutes) as shown with our measurements in Fig. 5e. As can be seen that the gas evolution process takes several minutes before reaching the sensor surface, hence yielding relatively long reaction times as explained in previous reports elsewhere [37]. However, to achieve short reaction times the volume of the gas mixing cylinder and piping system should be as small as possible. Hence, in our case, it is reasonable to infer that the shortest possible reaction time constants we are able to obtain are thus limited by the gas mixing process and the real reaction times may be shorter.

In this work the most interesting results were the strong dependence of conductivity inversion (n/p) behaviour on the measurement conditions, such as the gas concentration, operating temperature and applied voltage (Fig. S7, 8 in ESI). The gas concentration-dependent and (operating) temperature-dependent conductivity inversion are reported previously for intrinsic [38], doped semiconductor [39] and mixed oxide composite films [40]. However, according to author's best knowledge, the voltage-dependent conductivity transition has not been studied previously. Strikingly, for each sample and each measurement condition, there exists a critical point at which the conductivity inverses. This is something which is intriguing to tailoring the selectivity of the sensors yielding novel sensing characteristics phenomena to be exploited. For further analysis and discussion, it is essential to define this critical point as threshold-concentration ( $C_{th}$ ), critical-temperature ( $T_{th}$ ) and critical-voltage ( $V_c$ ).

Under ordinary circumstances,  $TiO_2$  shows n-type response to reducing gases [19, 20] and

oxidizing gases [21]. Irrespective to the operating temperature, all sensors showed as expected n-type response to overall range of  $H_2$  concentrations (40–100 ppm) at the lowest applied voltage 0.1 V. An inversion of conductivity from n- to p-type was observed for temperature below 300 °C at higher  $H_2$  concentrations (e.g.  $C_{th}$  [ppm]  $\sim$  750 and 825 at 200 and 250 °C). The values of  $C_{th}$  further decreases for the samples of Ti-Ag<sub>2</sub>O ( $C_{th}$  [ppm]  $\sim$  625 at 200 °C) and Ti-NiO ( $C_{th}$  [ppm]  $\sim$  250 at 200 °C) at these temperatures. Whereas, for applied voltage 1 V and above the conductivity inverts to p-type at lower  $H_2$  concentrations (Fig. 6a-c). At low operating temperatures the sensors show p-type behaviour for relatively low concentrations (e.g., 50 ppm or below) that inverts (p- to n-type) at higher  $H_2$  concentrations, e.g.,  $C_{th}$  [ppm]  $\sim$  50, 74, 125, and 500 at  $T_w$  [°C] = 200, 250, 300, 350 and 400 °C. At higher applied voltages, the values of  $C_{th}$  increase for Ti-Ag<sub>2</sub>O and Ti-NiO samples with increasing temperatures. It is also found that an inversion in conductivity occurs for high temperatures, which is time-dependent (Fig. 6d-f). For instance, the resistance of TiO<sub>2</sub> having p-type conductivity initially increases sharply above baseline stable resistance with  $H_2$  concentration, then consequently overshoots above the saturated resistance in gas. For a fixed concentration, in this case, the first step is p-type response transient which reverses to n-type with jagged saturate resistance in  $H_2$  gas. When the  $H_2$  gas is turned OFF, the resistance again initially overshoots (instead of resistance decrease), and finally recovers to baseline resistance. This time-dependent phenomenon is observed for high  $H_2$  concentrations, at high voltages and temperatures above 350 °C. The time-dependent conductivity inversion depends heavily on surface charge carriers and becomes dominant with Ag<sub>2</sub>O and NiO modifications (Fig. 3).

In fact the aforementioned critical points are all linked together as depicted in Fig. 7a-d. Irrespective to the electrical conductivity inversion, n- to p-type (red open circles) or p- to n-type (green open up-triangles),  $C_{th}$  in Fig. 7a,c increases proportionally with working temperature. In contrast a decrease in  $C_{th}$  against increasing voltage is observed. On the other hand, both critical voltage and critical temperature decreases linearly against each other Fig. 7b,c. Meanwhile the surface modification of TiO<sub>2</sub> with Ag<sub>2</sub>O and NiO brings further steep increase of the  $C_{th}$  against working temperature, see Fig. 7d.

#### 4. Discussion of sensing mechanism

Above presented data enable us to infer that a polycrystalline TiO<sub>2</sub> must inevitably inhere twofold electrical conductivity and its inversion is universal phenomenon related to the intrinsic nature of sensing layer surface at which a specific gas analyte can significantly switch the concentration of charge carriers. The statement must be true as our TiO<sub>2</sub> contains large crystallites, with diameter (50–70 nm as estimated via XRD analysis) considerably surpasses the Debye-length, where the bulk may still shows n-type conductivity, and contrary, due to the pre-adsorbed oxygen present on the surface exhibits p-type conductivity. Various reports to account for such phenomenon have been published [41]. Nevertheless, the conductivity inversion contains decisively confutable arguments and remains, to date, still debatable. Following, we propose and discuss the hydrogen sensing mechanism together with selectivity and electrical conductivity inversion on the basis electrode-sensing layer interface, grain boundary charge transport via finite barriers connected in series and the inversion layer emanating due to acceptor levels creation just above the valence band.

To begin with, and as stamped by our conductivity inversion specifically with Ag<sub>2</sub>O and NiO surface sensitization, we proceed with the fact that the sensor response is solely the surface reaction phenomena rather than the bulk (of Ti-discs) which contribute to the electrical conductivity only. This scenario for high voltage seems to be most likely improbable. In addition, it is also observed that Ag<sub>2</sub>O and NiO migrate several nm deep into TiO<sub>2</sub> oxidized layer. Another fact that must be considered beforehand is the polycrystalline nature of our samples giving rise to the origin of grain boundaries. In our model which is sketched in Fig. 8a, for simplicity, we assume that the Pt-TiO<sub>2</sub> plays only a negligible role for low applied voltages. In this case, the sensor response can be attributed mainly to the change in intergranular surface potential  $eV_s$  in the vicinity between successive grains.

During oxidation process at higher-temperatures, oxygen from the surrounding static-air enters into metallic Ti-discs yielding rutile TiO<sub>2</sub> as a consequence of several reactions and formation of donor-type doubly ionized oxygen vacancies ( $V_O^{\bullet\bullet}$ ) and titanium ( $V_{Ti}^{\bullet\bullet\bullet\bullet}$ ) vacancies, and acceptor-type titanium interstitials ( $Ti_i$ ). Later, under critical warm-up heating conditions in the presence of surrounding air and at temperature above 200 °C, firstly the sensor surface adsorbs ionic oxygen ( $O^-$  and/or  $O^{2-}$ ) which trap surface charge carriers (mostly surface conduction electrons). According to J. Nowotny et al. [10], both these situations are extremely critical because pre-adsorbed oxygen results in a variation (being most likely reduction) of electrons ( $e'$ ) or holes ( $h^\bullet$ ) concentration depending on whether it reacts with vacancies like oxygen ( $O_O \rightleftharpoons V_O^{\bullet\bullet} + 2e' + 1/2 O_2 + 2h^\bullet$ ) and titanium ( $O_2 \rightleftharpoons VTi^{\bullet\bullet\bullet\bullet} + 2OO + 4h^\bullet$ ) or in rare cases with surface Ti ( $2O_2 + 3e' + O_2 + 4h^\bullet$ ). Under these circumstances, an insulating space charge region (so-called depletion layer) at the grain surface is formed where donors are initially immobile. Now consider the experimental conditions below critical point in an air flow, when electric field is applied (in our case the field generated by applied voltage below 1 V), initially all donors in this region become ionized and their concentration outnumbers their counterparts. The charge carrier density at this stage is still small, but gives rise to the inceptive n-type electron conductivity (usually very low for high band-gap TiO<sub>2</sub>) and its transport is impeded by Pt-TiO<sub>2</sub> interface and thermally activated intergranular barriers ( $eV_s$ ) connected in series.

The experimental data presented in Fig. 9 explicitly validate above mentioned assumptions. The characteristics of the I-V curves are found to be strongly dependent on  $C_{th}$  and  $T_{th}$  and account for the sensing mechanism basis. As expected, the symmetrical nonlinear I-V characteristics are obtained in air environment that correspond to the rectifying behaviour at both Pt/TiO<sub>2</sub> interfaces (Fig. 9a). To ensure better qualitative analysis the scan rate is fixed very low for accurate I-V measurements, the typical I-V curves containing the reverse biased conditions (negative applied voltage) are shown in Fig. S9 of ESI. A variation in I-V curves can be seen, although not significant as the qualitative rectification feature is maintained. This difference portends the variation in pre-adsorbed oxygen on the surface these samples. The thermionic field emission conduction mechanism and diffusion theory is valid here as our polycrystalline TiO<sub>2</sub> contains low carrier density. For this case, the Schottky barrier

( $\phi_{SB}$ ) heights for each sample can be estimated by  $\phi_{SB} = k_B T \ln \left( \frac{I_s}{AA^* T^2} \right)$ , here  $k_B$  is

Boltzmann constant, T is temperature, A is the effective electrode area,  $A^*$  is the Richard's constant, and  $I_s$  is saturation current which can be obtained by extrapolating the exponential increase of the current to zero applied voltage [42]. The calculated values of  $\phi_{SB}$  for the TiO<sub>2</sub>-TiO<sub>2</sub>, TiO<sub>2</sub>-Ag<sub>2</sub>O and NiO samples are ~0.38, 0.34 and 0.33 eV respectively. The

values are quite distinct from the theoretically estimated value. For a comparative Pt/TiO<sub>2</sub> system, the difference of Pt work function ( $\Phi_{Pt} \sim 5.65$  eV) and TiO<sub>2</sub> electron affinity of ( $\chi_{TiO_2} \sim 4.16$ ) should result in a Schottky barrier height of 1.44 eV. The lower  $\phi_{SB}$  values in our case are understandable as during contact formation between Pt-electrodes and Pt-wires the silver paste is used as bond and further annealed at 550 °C to make it dry. This temperature is enough to diffuse Pt into TiO<sub>2</sub> several nm thickness [19, 43]. Fig. 9b confirms the second assumption, the electrical conductivity of our samples show strong dependent to the temperature. From Arrhenius curves, plotted with R-T data, the values of extracted thermal activation energies (which we denote as effective barrier height between the grains) are  $eV_s$  [eV]  $\sim 1.28$ , 1.32 and 1.73 for the TiO<sub>2</sub>-TiO<sub>2</sub>, TiO<sub>2</sub>-Ag<sub>2</sub>O and NiO samples respectively. For the fair comparison, we used the high temperature slope of Arrhenius plot for TiO<sub>2</sub>-NiO sample, as it indicates two distinct  $eV_s$  values (0.89 eV and 1.73 eV). Theoretically, on the basis of Pt electrode spacing (10  $\mu$ m) and grain size which is estimated as an average of all rutile crystallites size, obtained from XRD analysis for TiO<sub>2</sub>-TiO<sub>2</sub> ( $D_g \sim 65$  nm), TiO<sub>2</sub>-Ag<sub>2</sub>O ( $D_g \sim 50$  nm), and TiO<sub>2</sub>-NiO ( $D_g \sim 55$  nm), the values of  $eV_s$  for TiO<sub>2</sub>-TiO<sub>2</sub> should be smaller followed by TiO<sub>2</sub>-NiO and TiO<sub>2</sub>-Ag<sub>2</sub>O, as number of grains ( $N_g$ ) between the electrodes should follow the following sequence: TiO<sub>2</sub>-TiO<sub>2</sub> ( $N_g \sim 145$ ), TiO<sub>2</sub>-NiO ( $N_g \sim 180$ ) and TiO<sub>2</sub>-Ag<sub>2</sub>O ( $N_g \sim 200$ ). Hence, it can be inferred that for the large grains the effective  $eV_s$  values estimated by Arrhenius plots does not explicitly represent the average barrier heights of the depleted grains connected in series. Thus, the hypothesis – small grains lead to large  $eV_s$  values – is no longer valid. Apparently, in controlled dry air flow, the samples exhibit the conventional low charge concentration-based intrinsic characteristics.

Upon exposure, H<sub>2</sub> gas diffuse onto respective rutile TiO<sub>2</sub> surface and subsequently reacts with the pre-adsorbed oxygen to release captured immobile charge carriers that eventually reduce Pt-TiO<sub>2</sub> interface as well as the width of depletion region and intergranular barriers. To some extent this is true for unmodified TiO<sub>2</sub> under operating conditions below critical point. On the other hand, the origin of innate p-type TiO<sub>2</sub> sensor response to H<sub>2</sub> above the  $C_{th}$  and  $T_{th}$  can be understood on the basis of electronic band gap theory. As sketched in Fig. 8, the presence of surface defects give birth to intrinsic and extrinsic surface states that introduce energy levels with the forbidden energy gap of TiO<sub>2</sub>. At this stage if acceptor concentration surpasses donors the depletion region spontaneously splits up in two distinct regions of  $e^-$  (above Fermi level) and  $h^+$  (below Fermi level) majority carriers as sketched in Fig. 8b. The latter strongly gives rise to p-type conductivity and, thus, is known as inversion layer. Following the increase of H<sub>2</sub> concentration and operating temperature above their respective threshold value, the H<sub>2</sub>-TiO<sub>2</sub> surface reaction leads in excess of localized acceptor levels [10] to fully demolish the depletion layer where inversion layer overtakes the sensing mechanism and its thickness consequently extends to increase the resistance. The selectivity towards H<sub>2</sub> can be accomplished by the fact that molecules of the other reducing gases (CO, CH<sub>4</sub> and NH<sub>3</sub>) are too large and thus cannot diffuse through the surface to the bulk. The authors, however, believe that the selectivity of these sensors can be efficiently tuned by proper adjustment of the measurement conditions, specifically operating temperature and applied voltage.

Under H<sub>2</sub> exposure with low concentrations the sensor did not show rectifying behavior as shown in Fig. 9c. The electronic current first increases for low voltages and then decreases followed by another increase for further high applied voltages. This behavior is strongly related to conductivity inversion with threshold limit of the concentration. On the other hand, for high H<sub>2</sub> concentration, the current increases linearly and then saturates after 4 V. There is

an obvious decrease ( $\sim 0.05\text{--}0.2$  eV) in the Schottky barrier height for higher concentration, however, this is small as compared with high intergranular barrier height ( $\sim 0.5\text{--}0.9$  eV) for 200 ppm  $\text{H}_2$  as shown in Fig. 9d. This observation again confirms our above mentioned assumption. With regard to the role of  $\text{TiO}_2$  surface modification with  $\text{Ag}_2\text{O}$  and  $\text{NiO}$  towards low  $\text{H}_2$  concentrations, the high sensor response can be attributed to the formation of n-p heterojunction at the sensors surface. The statement seems to be true only for low voltages. Conversely, p-p heterojunction is expected for high applied voltages ( $\sim 2$  V). As mentioned in the section 3.2 above, due to large difference in the effective ionic radius of  $\text{Ag}^+$  and  $\text{Ti}^{4+}$ , so the substitution of  $\text{Ti}^{4+}$  by  $\text{Ag}^+$  is improbable. While  $\text{Ni}^{2+}$  incorporation into  $\text{TiO}_2$  lattice is highly possible ionic radii of  $\text{Ni}^{2+}$ . Both Ag and Ni begin to oxidize on the surface by taking electrons and their interface regions is the most favorable to provide  $e^-/h^+$  recombination as it contains high defects concentration related to  $e^-$  traps or donors [45]. The electrons must transfer from  $\text{TiO}_2$  to the  $\text{Ag}_2\text{O}$  and  $\text{NiO}$ , as  $\text{TiO}_2$  has higher electronic fermi level. Thus additional depletion zone originates at the heterojunction to hinder the charge carrier transport and, consequently, under  $\text{H}_2$  exposure the  $h^+$  charges become dominant to give p-type conductivity.

The conventional models, however, fail to explain anomalous n/p conductivity inversion against applied field. The reason for this is obvious. Because the electrical resistance must decrease for typical n-type  $\text{TiO}_2$  even in air flow environment with the rise of applied voltage as the electronic current flows through the bulk of the oxidized Ti-disc where the concentration of free conduction electrons ( $n_{cb}$ ) increases directly with generated electric field. Mathematically, as reported in [46], for inter-digitated electrodes with known separation distance ( $s$ ), electrode width ( $w$ ), and applied voltage  $V_0$ , the electric field density  $E(x,y)$  and surface charge distribution  $\sigma(x)$  can be estimated by using following equations:

$$E(x, y) = -\nabla V(x, y)$$

$$\sigma(x) = -2\varepsilon \left( \frac{2V_0}{\pi} \right) \left( \frac{1}{\sqrt{(2x/s)^2 - 1}} \right) (2/s)$$

Where

$$V = \frac{4V_0}{\pi} \sum_{n=1}^{\infty} \frac{1}{2n-1} J_0 \left( \frac{(2n-1)\pi s}{2(s+w)} \right) \sin \left( \frac{(2n-1)\pi x}{2(s+w)} \right) \left( -\frac{(2n-1)\pi |y|}{2(s+w)} \right)$$

For low applied voltages (below 1 V) on the same film, more than 90% of the electric current flows at the heavily packed with the pre-adsorbed oxygen near surface. Thus, the conductivity as well as the sensing mechanism is predominantly governed by intergranular active thermal barriers. On the other hand, for high voltage, the calculations with the known parameters ( $V_0 = 2$  V,  $s=w=10$   $\mu\text{m}$ ,  $y=0$ ) would give high accumulated potential ( $\sim 1.2$  V) at the edges of the electrodes and an excess potential drop. This is a situation that cannot be applied in our case because of the fact that the electrodes along its sides have uniform dimensions. Now, as confirmed by SEM cross-section (not shown), if we consider 100 micron thick  $\text{TiO}_2$  film and for 2 V applied voltage, about 85% of the current might flow deep 25  $\mu\text{m}$  through the bulk of  $\text{TiO}_2$  loaded with free conduction electrons ( $n_{cb}$ ).

In agreement with the mentioned arguments  $R_{air}$  decreased from 650  $\text{M}\Omega$  to 8  $\text{M}\Omega$  with

voltage from 0.1 to 1 V. On the contrary,  $R_{air}$  value is increased from 200 M $\Omega$  to 500 M $\Omega$  when the voltage is further increased from 1 to 2 V. This is something contradicting the theory. This anomalous behavior can partially be validated in terms of electric potential fluctuation model and electron trapping-releasing process. As argued by Konenkamp et al. [47], the existence of potential gradient must occur in comparative systems due to the presence of localized charges resulted by various defects. Under the high injection potential and ideal electron behavior, the electrons move away from the electric field and diffuse linearly to the electrode stripe where the pre-adsorbed oxygen on electrode edges account for the electron trap resulting in charge accumulation [46]. The result is high potential and electric distribution at the electrode stripe edges. At the same time, bulk oxygen vacancies become positively charged ionic center and act as another electron trap at higher voltage. The simultaneous trapping/releasing of the electron might happen within a fraction of second, and thus, compensating influence is exerted. For such case, the potential fluctuations are highly probable leading to invalidity of local charge neutrality condition. As both the amplitude and screening length of potential fluctuations are strongly dependent on  $n_{cb}$ , due to which the height of the Pt/TiO<sub>2</sub> Schottky interface would rather increase. This situation is in agreement of our I-V data where an unforeseen increase of Schottky barrier height is observed (Fig. 8d). Such high Schottky barrier height reduces the sensor response significantly as observed in our high voltage response and is consistent with previous reports [20]. This is an appealing and important feature of current study that offers relationship between sensor characteristics and measurement conditions. The study would notably help for the careful fabrication of future smart sensors for remote gas monitoring with controlled critical voltage, threshold temperature and gas concentration.

While the electric potential fluctuations and electron trapping/releasing mechanism enable us to clarify some of the conflicts in previous studies and describe the applied voltage effect on n- to p-type conductivity inversion, based on some assumptions, yet it does not account for some of the above properties in details. The method seems to be justified as long as the grain size is sufficiently large but becomes complicated with for small grains and films with low thickness. For this case, a better understanding of these mechanisms with the help of dc Hall measurements may therefore be necessary, which will allow explanation of the nature of dominant charge carriers. Our current setup does not allow us to perform such measurements. In-situ XPS analysis may be worthy to determine the formation of various other titanium oxide phases (such as Ti<sub>n</sub>O<sub>2n-1</sub> Magneli phases) with gas exposure under high applied voltage. In addition, due to the involvement of photoresist, developer and etchants in the electrode fabrication process on the sensor surface, one may expect surface contamination and extra surface defects. The role of active top Pt-electrode cannot be overruled, as Pt acts as a catalyst, something to be taken care in the future. These analyses, despite answering several questions, however, would extend out of the scope of this paper. Nevertheless, additional related work for better understanding of such complexities is planned as future collaboration among the authors.

## 5. Conclusion

A simple gas sensor configuration was designed for the detection of hydrogen at intermediate temperatures 200-400 °C. Intensive XRD studies show no significant changes in structure, meanwhile, morphological and surface chemistry states of TiO<sub>2</sub> were strongly altered by Ag<sub>2</sub>O and NiO surface modification as attested by SEM and TEM analysis. The

sensors performance is excellent as it shows significant response (1.5) to low ppm H<sub>2</sub> (40 ppm) at given operating temperature (300° C) even with low applied voltage (0.1 V). The breakthrough data was obtained which shows strong correlation of sensor response with gas concentration ( $C_{Th}$ ), operating temperature ( $T_{Th}$ ) and applied biased voltage ( $V_C$ ). This suggests that co-existence of both n- and p-type conductivity and its inversion, at threshold gas concentration ( $C_{Th}$ ), operating temperature ( $T_{Th}$ ) and applied voltage ( $V_C$ ), is universal phenomenon found in polycrystalline TiO<sub>2</sub> that must be extended to other semiconducting metal oxides such as SnO<sub>2</sub>, ZnO and etc. Further the detailed study of sensing mechanism and conductivity inversion enable the novel physical-chemical model which shows that dominant part of sensing mechanism is related to the variations in inversion layer and intergranular surface potential. We believe that these results and analyses provide significant conceptual as well as technological advance to open novel means in gas sensor technology to trigger enhance and selective monitoring of specific gas analyte.

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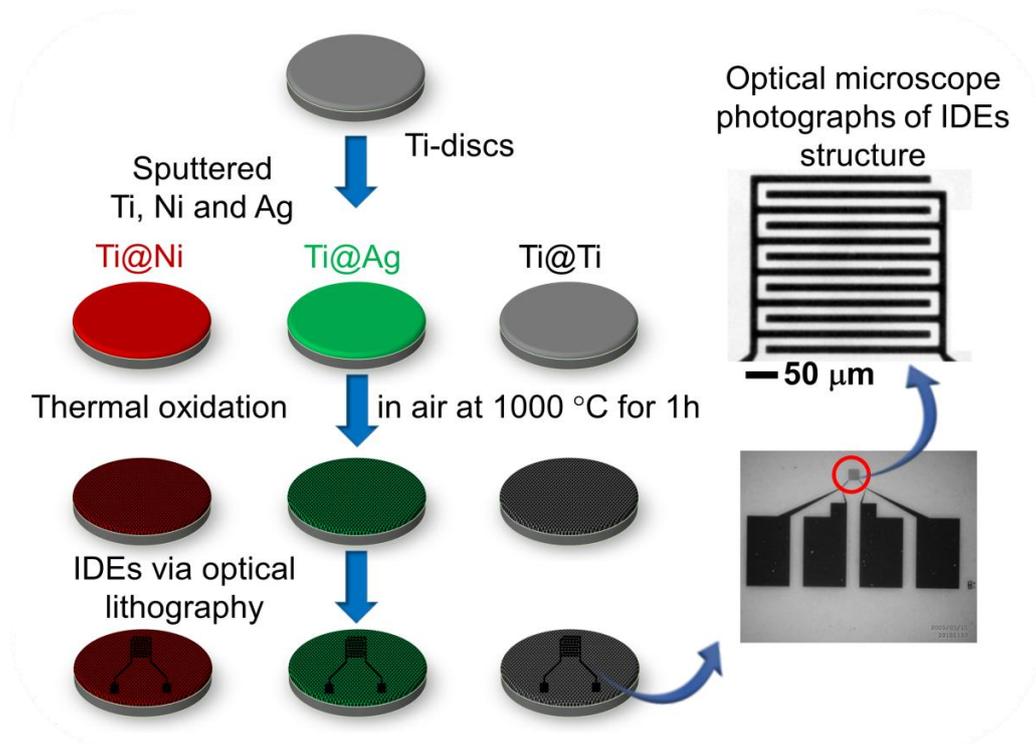
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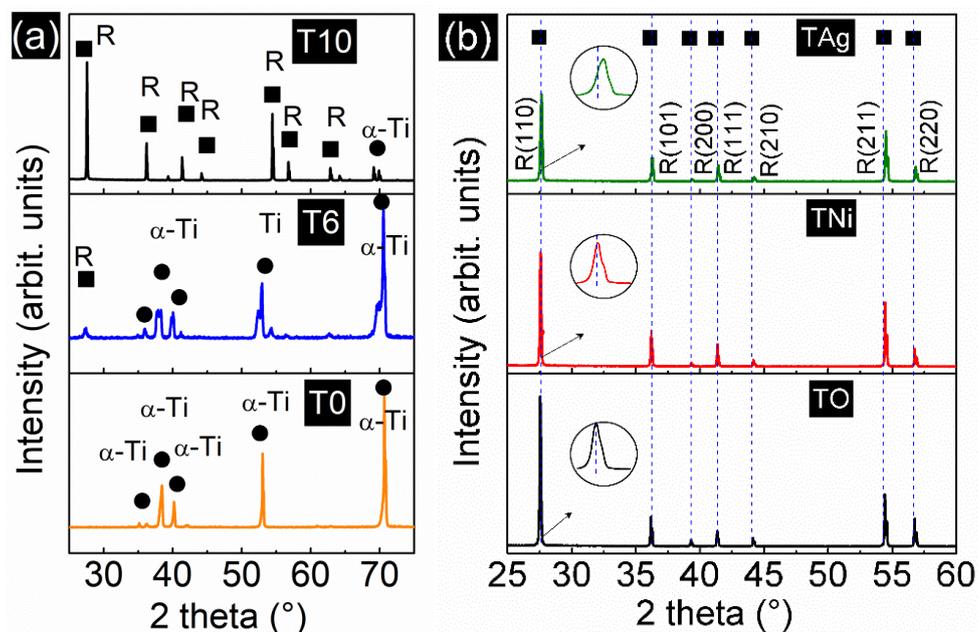
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Table 1: Comparison of the current work highlights with previous works.

Sensor system	Background condition	C <sub>H2</sub> (ppm)	T (°C)	Sensor Response	Voltage(V)	Remarks
Nanoporous TiO <sub>2</sub>	Dry air	1250	225	1.13	-	Nanoporous TiO <sub>2</sub> was prepared by anodization [29].
	Humid air	Not Reported (NR)				
TiO <sub>2</sub>	Dry air	150	300-400	-	-	Flame-spray-made unloaded TiO <sub>2</sub> ; selectivity was not reported [30].
	Humid air	Not Reported (NR)				
Pt-TiO <sub>2</sub>	Dry air	40	300-400	1.1	-	Flame-spray-made Pt-loaded TiO <sub>2</sub> nanopowders [30].
	Humid air	Not Reported (NR)				
Pd-TiO <sub>2</sub>	Dry air	10	180	1.25	5V	Anodization of Ti film obtained Pd-decorated TiO <sub>2</sub> tubular structures, which showed good selectivity to CO, CO <sub>2</sub> , ethanol and acetone [31].
	Humid air	1-50	140-180	-		
	N <sub>2</sub>	10	180	25		
Al-TiO <sub>2</sub>	Dry air	500	200-400	1.3	-	Aluminium doped porous titania (TiO <sub>2</sub> ) thin films were grown by thermal oxidation. [32]
	Humid air	Not Reported (NR)				
NiO-TiO <sub>2</sub>	Dry air	300	200	1.47	-	P-type to n-type transition was mentioned [9].
	Humid air	Not Reported (NR)				
SnO <sub>2</sub> -TiO <sub>2</sub>	Dry air	50	300	0.9	-	S=(R <sub>0</sub> -R)/R <sub>0</sub> [33]
	Humid air	Not Reported (NR)				
CdO-TiO <sub>2</sub>	Dry air	500	275	0.3-3.06%	0.25V	%S = (R <sub>0</sub> -R)/R <sub>0</sub> × 100 [34]
	Humid air	Not Reported (NR)				

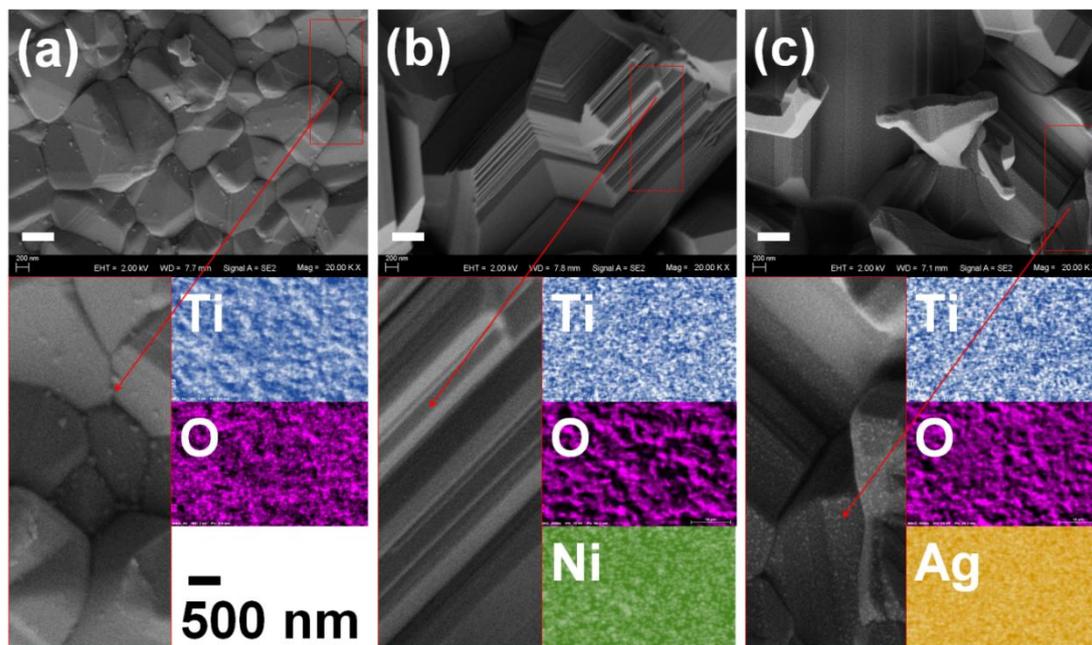


**Fig. 1** (color online) The schematic diagram showing the fabrication process of gas sensors based on  $\text{TiO}_2$  films with  $\text{TiO}_2$ ,  $\text{NiO}$  and  $\text{Ag}_2\text{O}$  modification, the figure also includes the optical microscope photographs of interdigitated electrodes (IDEs) structure, the scale bar on the most top right optical microscope photograph of the comb-like Pt electrodes with 10  $\mu\text{m}$  spacing indicates the scale of 50  $\mu\text{m}$ .

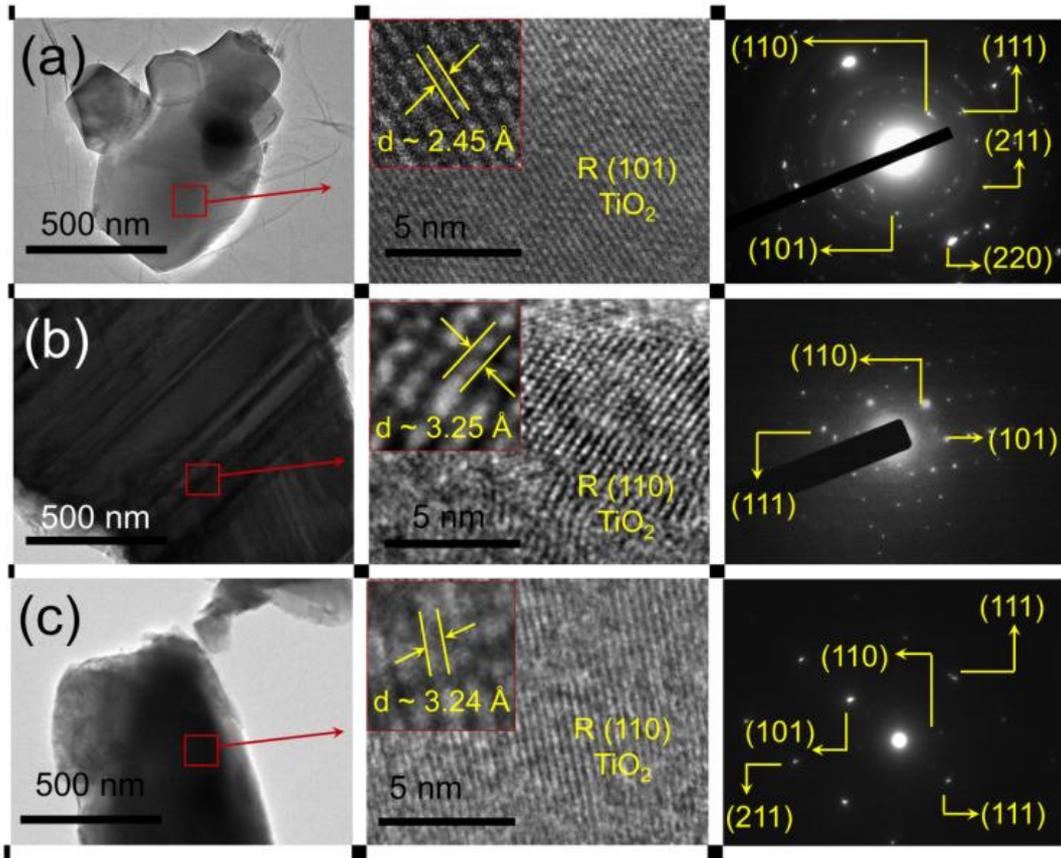


**Fig. 2** (color online) The XRD diffractograms of as-received Ti-discs (T0) and oxidized Ti-discs at 600 °C (T6) and 1000 °C (T10) are shown in (a). The comparative diffractograms of Ti-discs modified with Ti (TO), Ni (TNi), and Ag (TAg), the inset of each curve shows variation in peak intensity and right shift of the zoomed R (110) crystal in (b). The XRD diffractograms were

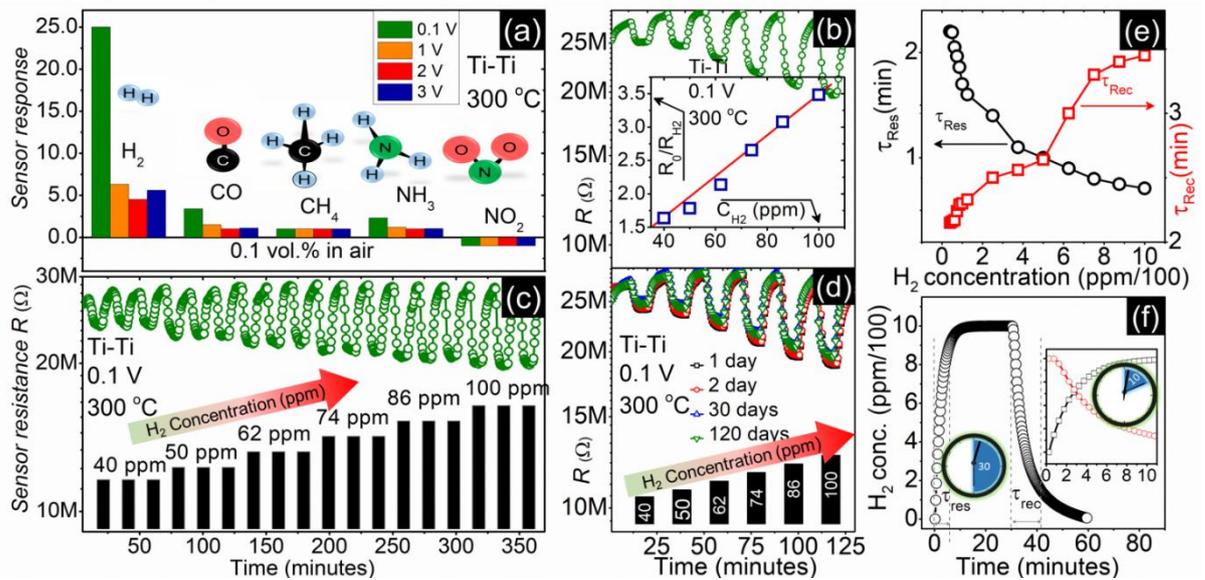
compared with standard powder diffraction card JCPD-44-1294 ( $\alpha$ -Ti with hexagonal closed packed,  $a = 2.9504 \text{ \AA}$ ,  $c = 4.6833 \text{ \AA}$  and  $c/a$  ratio of  $\sim 1.587$ ) and JCPDS-21-1276 (rutile with tetragonal symmetry of space group  $P4_2/mnm$  with  $a = b = 4.5933 \text{ \AA}$ ,  $c = 2.9592 \text{ \AA}$  and  $c/a$  ratio of  $\sim 0.644$ ).



**Fig. 3** (color online) The SEM and EDS analysis of  $\text{TiO}_2@ \text{TiO}_2$  (a),  $\text{TiO}_2@ \text{NiO}$  (b), and  $\text{TiO}_2@ \text{AgO}$  (c) oxidized discs. The enlarged SEM micrographs and EDX elemental mapping of these samples are shown on bottom figure. Solid white lines in a-c indicate the 500 nm scale bar in SEM micrographs. The EDX analysis of  $\text{TiO}_2@ \text{NiO}$  (b) and  $\text{TiO}_2@ \text{AgO}$  (c) confirms the presence of NiO and AgO due to thermal oxidation process.

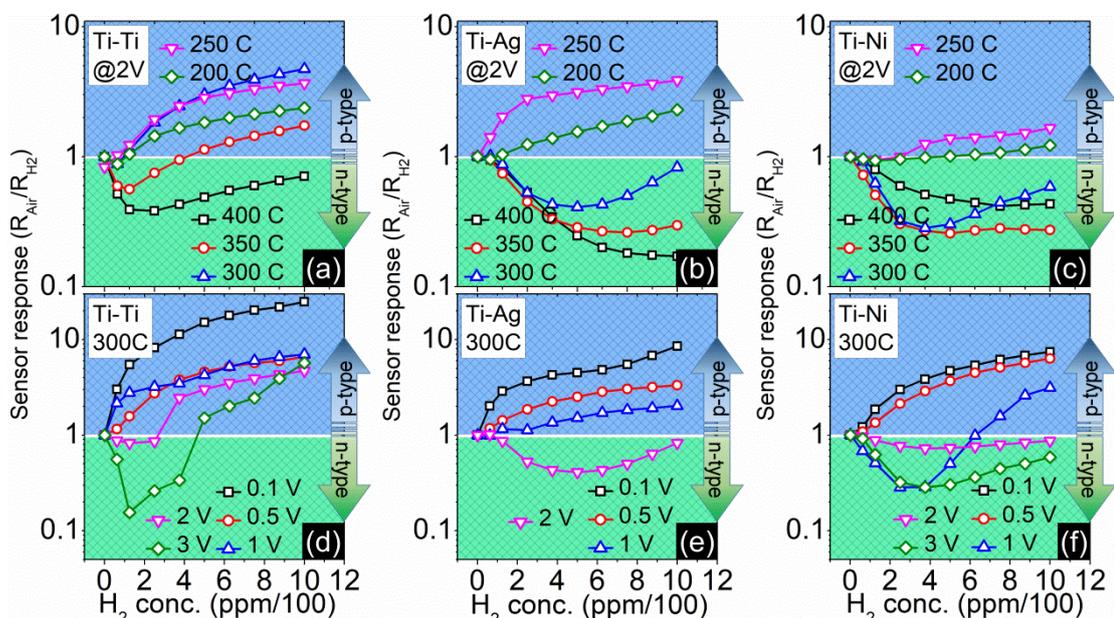


**Fig. 4** (color online) The TEM micrographs of  $\text{TiO}_2@\text{TiO}_2$  (a),  $\text{TiO}_2@\text{NiO}$  (b), and  $\text{TiO}_2@\text{AgO}$  (c) oxidized discs are shown on left figures. The middle figures show corresponding HRTEM images with the inset shows magnified HR image and estimated d-spacing values for each samples. The figures on the right show respective selected area diffraction (SAED) pattern.

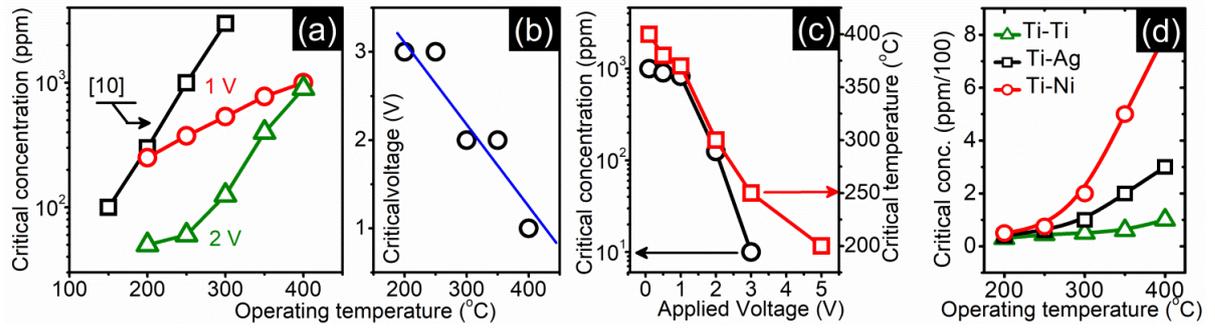


**Fig. 5** (Color online) Selectivity of the sensors to hydrogen against other gases such as CO, CH<sub>4</sub>, NH<sub>3</sub>, and NO<sub>2</sub> is shown in (a). Hydrogen gas sensing characteristics of  $\text{TiO}_2@\text{TiO}_2$  sensors, the typical real time changes in the electrical resistance upon the gas in/out cycles, id est

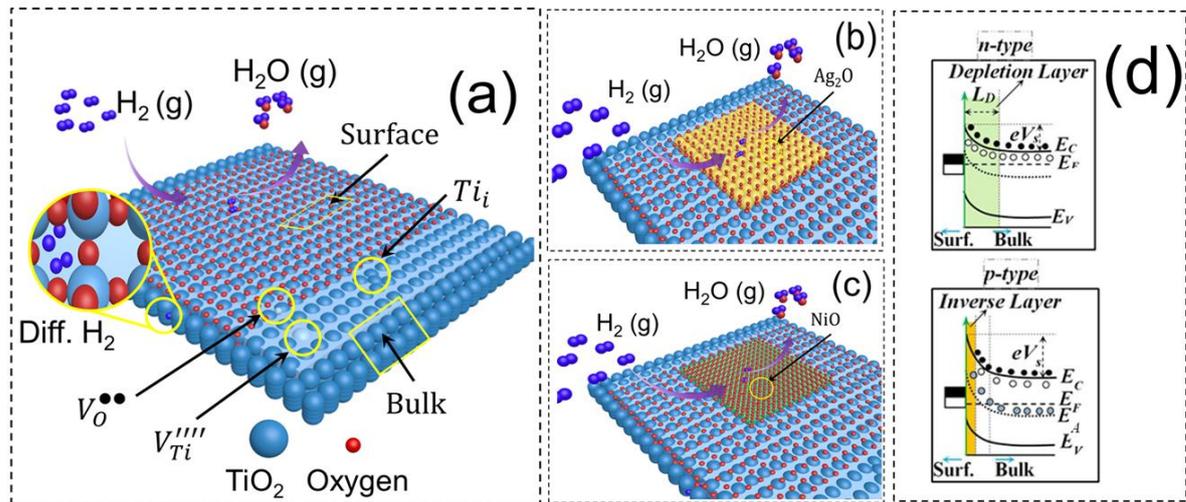
dynamic-responses, to sequential cycles of 40, 50, 62, 74, 86 and 100 ppm hydrogen gas balanced in technical air (a). The dynamic responses were recorded by using in-house made software in LabVIEW with a fixed time (10 minutes) for each sequential cycle at operating at 300 °C with 0.1V biasing. Inset: The plots of sensor response ( $S = R_0 / R_g$ ) versus increasing hydrogen gas concentrations for the TiO<sub>2</sub>@TiO<sub>2</sub> sensors evaluated from the dynamic responses of the sensors presented in (b). The sensor responses were calculated from the ratio of stable base resistance in air ( $R_0$ ) to saturated resistance value ( $R_g$ ) in specific hydrogen concentration (62 – 1000 ppm). The long term and short term stability of the sensors is demonstrated in (c) and (d) respectively. The x-axis scales on (b) and (d) are same. The estimated response ( $\tau_{Res}$ ) and recovery ( $\tau_{Rec}$ ) times plotted against hydrogen concentration (62 – 1000 ppm) are shown in (e). The simulated plot of typical H<sub>2</sub> 1000 ppm concentration evolution of 30 minutes cycle inside the chamber is shown in (f). Inset: The zoom-in (enlarge) view of the simulated plot of 1000 ppm H<sub>2</sub> evolution inside the chamber for initial 10 minutes, the y-axis scale is equal to the scale of main plot.



**Fig. 6** (color online) The plots of sensor response ( $S_R = R_0 / R_g$ ) as a function of hydrogen gas concentrations ( $C_{H_2}$ ) at various working temperatures 200 °C (green open diamond  $\diamond$ ), 250 °C (magenta open down-triangle  $\nabla$ ), 300 °C (blue open up-triangle  $\triangle$ ), 350 °C (red open circle  $\circ$ ) and 400 °C (black open squares  $\square$ ) for the sensors based on Ti-Ti (a), Ti-Ag (b) and Ti-Ni (c), the  $S_R$  values were evaluated from step-like transient responses recorded at 2 V. The plots of sensor response  $S_R$  as a function of hydrogen gas concentrations ( $C_{H_2}$ ) at various working temperature 300 °C for the sensors based on Ti-Ti (a), Ti-Ag (b) and Ti-Ni (c), the  $S_R$  values were evaluated from step-like transient responses recorded at various voltages 0.1 V (black open squares  $\square$ ), 0.5 V (red open circle  $\circ$ ), 1 V (blue open up-triangle  $\triangle$ ), 2 V C (magenta open down-triangle  $\nabla$ ) and 3 V (green open diamond  $\diamond$ ).

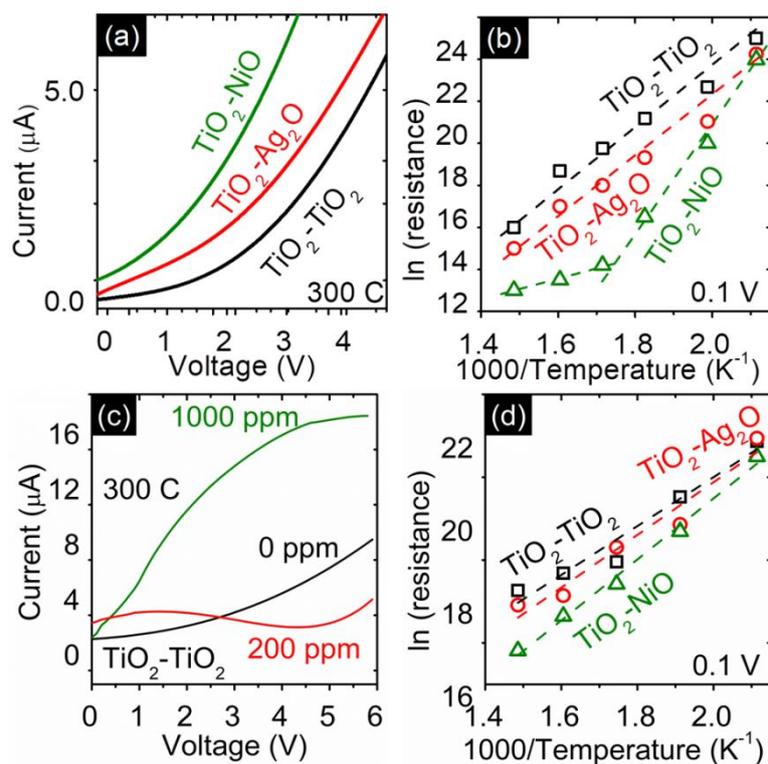


**Fig. 7** (color online) The interdependence of critical concentration, critical temperature and critical voltage. The plot of critical concentration and critical applied voltage against working temperature is shown in (a) and (b). The values of critical concentration and applied voltage are taken from step-like measurements of TiO<sub>2</sub>-TiO<sub>2</sub> samples measured at 1 V (red open circle ○) and 2 V (green open up-triangle △), the data plotted as black open box □ were measured at 1 V by I. Kostic et al. [10].



**Fig. 8** (color online) The illustration of sensing mechanism with physical-chemical method, H<sub>2</sub> surface reaction, H<sub>2</sub> diffusion through the surface, various kinds of defects related to O, Ti vacancies, Ti interstitials and the representation of bulk TiO<sub>2</sub> and oxygen rich surface (a). The reaction of H<sub>2</sub> gas with Ag<sub>2</sub>O (b) and NiO (c) modified TiO<sub>2</sub>-surface. The band bending schematic representation of n- and p-type TiO<sub>2</sub> responses is shown in (d). For n-type the conductivity is dominated by the depletion layer where the Fermi level lies near the conduction level and the majority carriers are electrons (on left). On the other hand, for p-type surface the inverse layer is formed where the Fermi level is situated near the donor energy level and the majority carriers are holes (on right). Here electrons, oxygen vacancies and holes are represented by filled black circles ●, open circles ○, and striped circles ⊕, respectively. The energy bands E<sub>C</sub>, E<sub>F</sub>, E<sub>D</sub> and E<sub>V</sub> represent conduction, Fermi, donor and valence energy level respectively, L<sub>D</sub> is the Debye length of the depletion layer and qV<sub>s</sub> is the height of surface potential barrier. The figure also depicts the mechanism behind conductivity inversion with threshold concentration (C<sub>Th</sub>), threshold temperature (T<sub>Th</sub>) and critical applied voltage along with TiO<sub>2</sub> surface modification with Ag<sub>2</sub>O or

NiO forming a heterojunction.



**Fig. 9** (color online) The current-voltage (I-V) characteristics performed in dry air flow at 300° C (a). The extracted Arrhenius plots for TiO<sub>2</sub>-TiO<sub>2</sub>, TiO<sub>2</sub>-Ag<sub>2</sub>O and NiO samples from operating temperature (200 – 400 °C) dependent resistance measurement in dry air flow (b). Here, the symbols indicate the original data points and dashed-lines indicate the linear fit. The current-voltage (I-V) characteristics performed for TiO<sub>2</sub>-TiO<sub>2</sub> sample in 0, 200 and 1000 ppm H<sub>2</sub> flow at 300° C (c). The extracted Arrhenius plots for TiO<sub>2</sub>-TiO<sub>2</sub>, TiO<sub>2</sub>-Ag<sub>2</sub>O and NiO samples from operating temperature (200 – 400 °C) dependent resistance measurement 200 H<sub>2</sub> flow (d).

**Supplementary Material**

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