

Study of Detailed Degradation Behavior of Solid Oxide Electrolyzer Cells (SOEC)

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Outline

- Introduction: Need for energy storage
Principle of solid oxide electrolysis
- Motivation and concept
- Cell manufacturing and characterization
- Degradation study and results from post-mortem analyses
- Conclusion



Storage of Electricity from Renewable Energy Sources

- Need for energy storage
 - Increasing fluctuating power generation
 - Mobile applications
- Electrical energy difficult to store
 - Conversion to chemical energy
- Water electrolysis: $\text{H}_2\text{O} + W_{\text{el}} \rightarrow \text{H}_2 + \frac{1}{2} \text{O}_2$
- Solid oxide electrolysis is one possible conversion technology



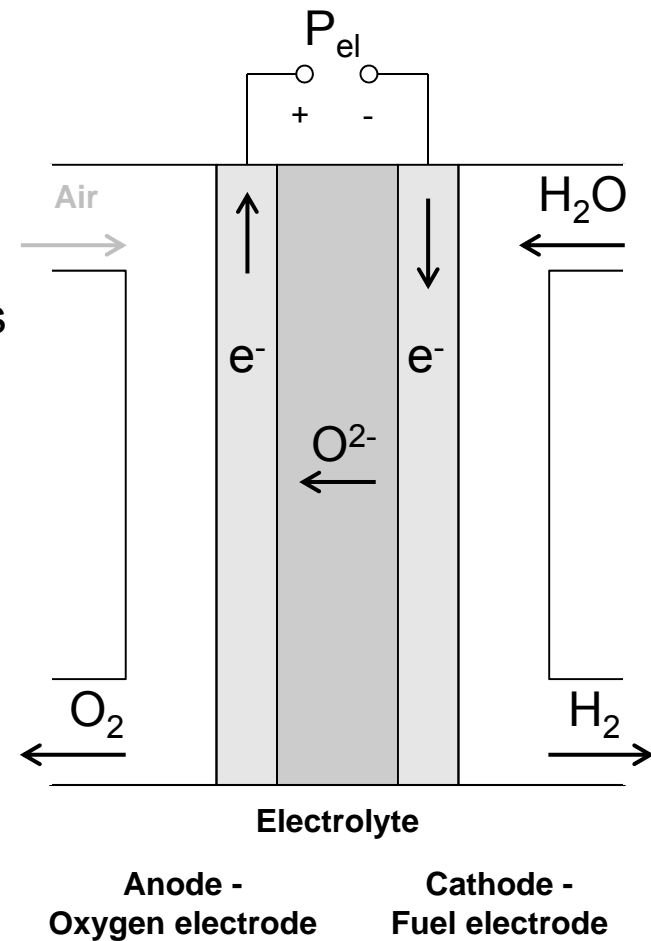
Principle of Solid Oxide Electrolysis

Advantages:

- High temperature (600 - 900° C)
 - Fast reaction kinetics
 - Low overvoltage
 - High efficiency & high current densities
- No noble metals as catalysts
- Fuel versatility: CO₂ electrolysis
 - Co-electrolysis of H₂O/CO₂ possible
 - Syn-gas production
 - External (or internal) hydrocarbon formation

Problem:

Low longevity - Degradation



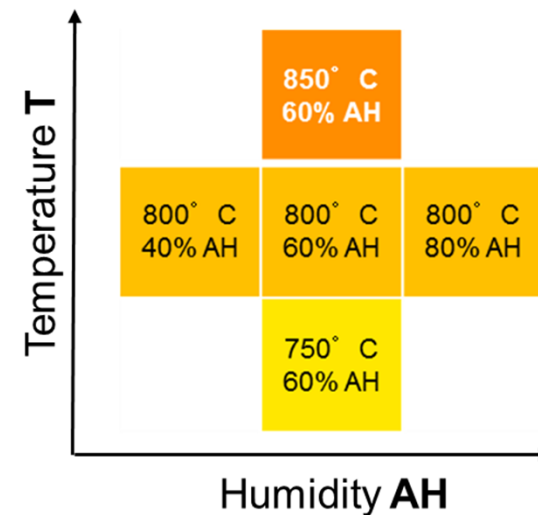
Present Work – Motivation and Concept

Systematic study: operating parameter → degradation

- Temperature (T)
- Fuel gas humidity (AH)
- Current density (i)

Experimental concept:

- Degradation experiments for 1000 h
- Test rig – quadruple cell measurement
 - Identical temperature, gas supply (and also incidents)
 - Four different current densities simultaneously
- Fuel electrode supported cells from FZ Jülich and CeramTec
 - Ni-8YSZ support | Ni-8YSZ | 8YSZ | CGO | LSCF

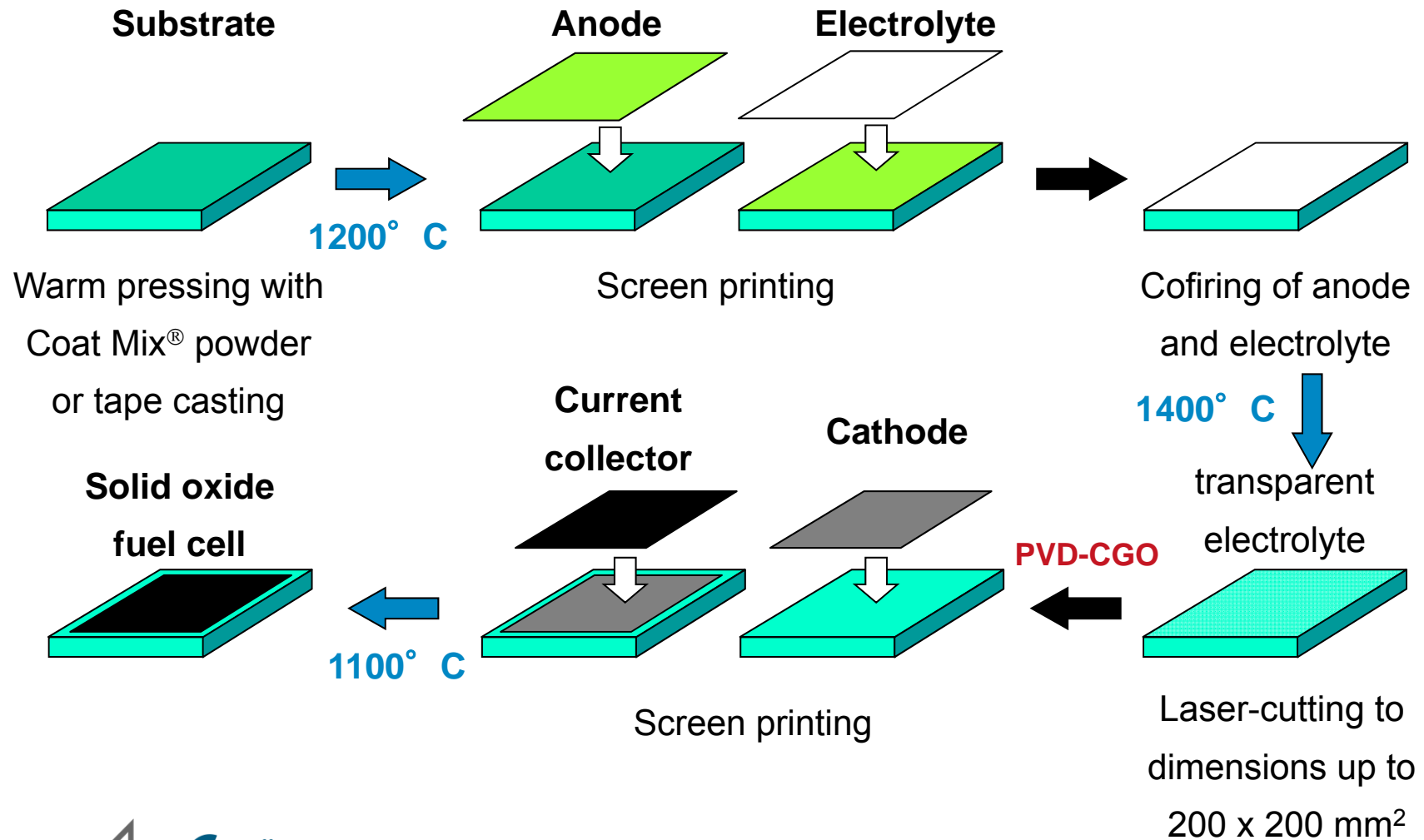


Objectives

- To gain fundamental understanding of degradation processes
 - Distinguish between degradation processes
 - Identify degradation mechanisms
 - Correlate them with operating parameters
- To optimize cells for electrolysis operation
- To adapt operating parameters for low degradation



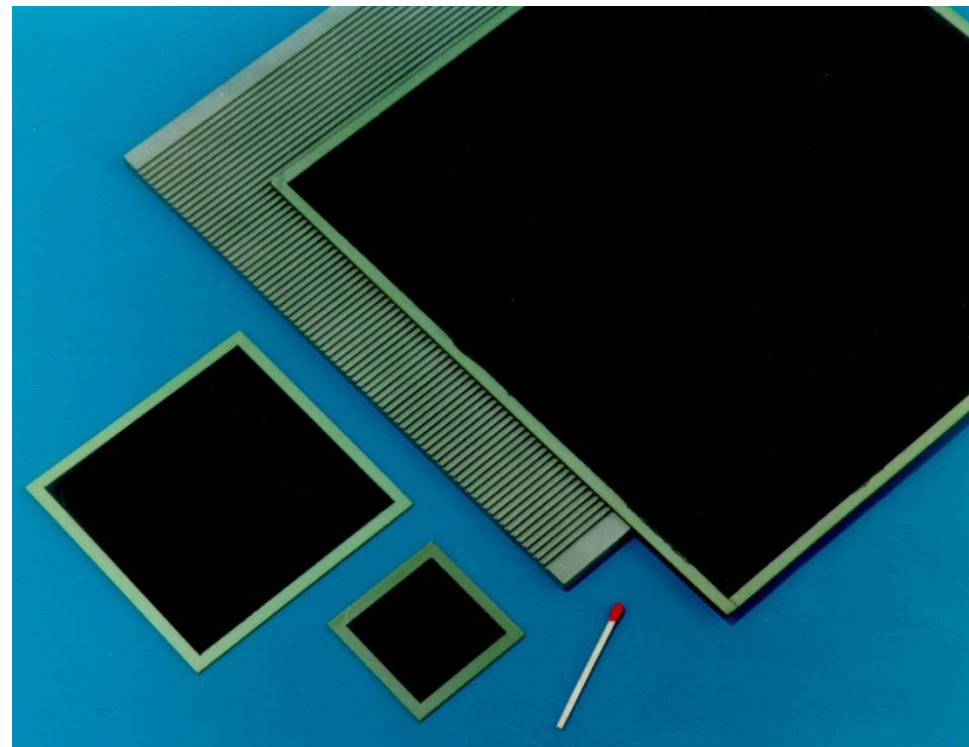
Manufacturing Steps of SOFC Anode-Supported Cells



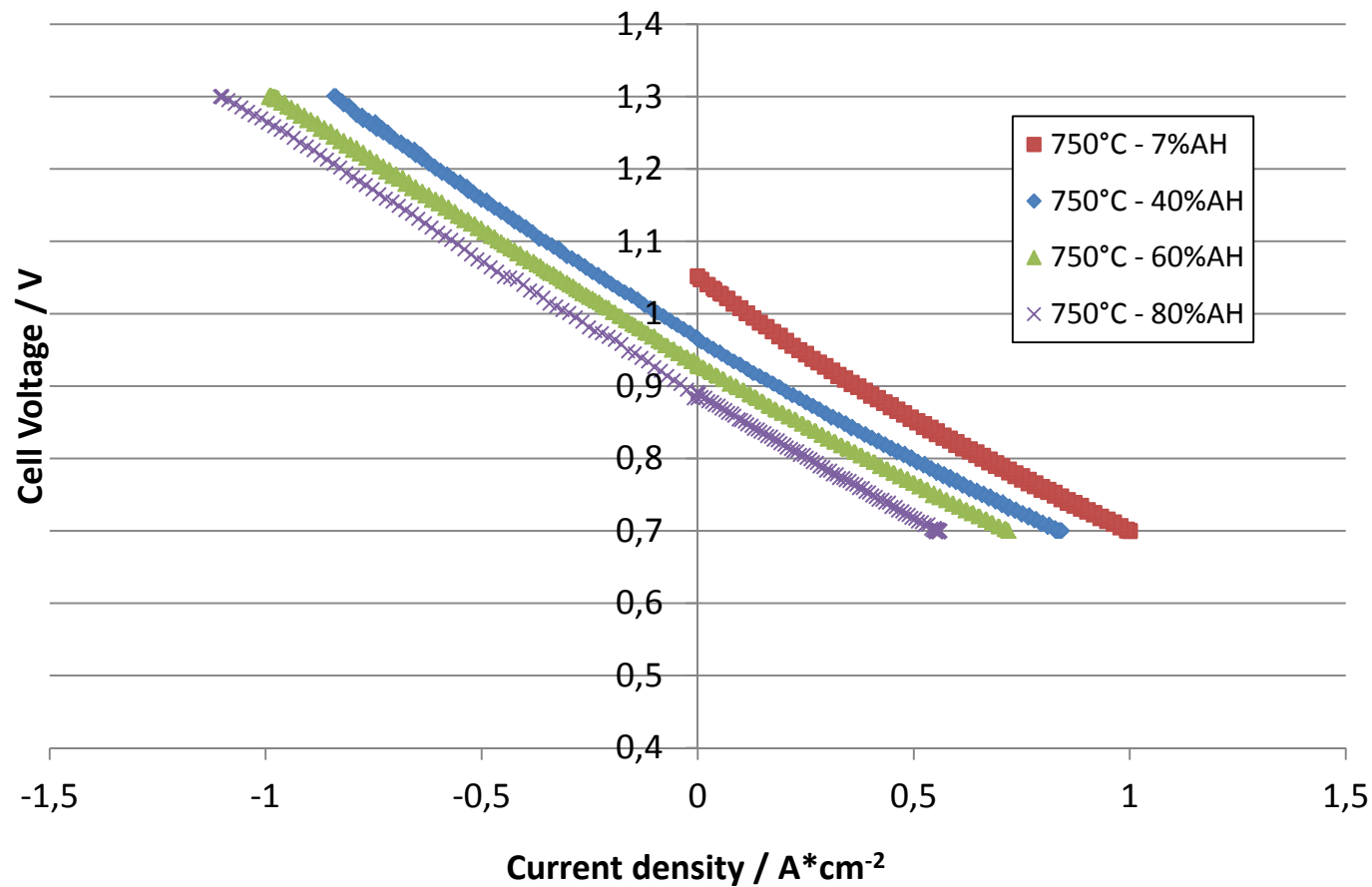
Solid Oxide Electrolyser Cells: Planar Design

Materials

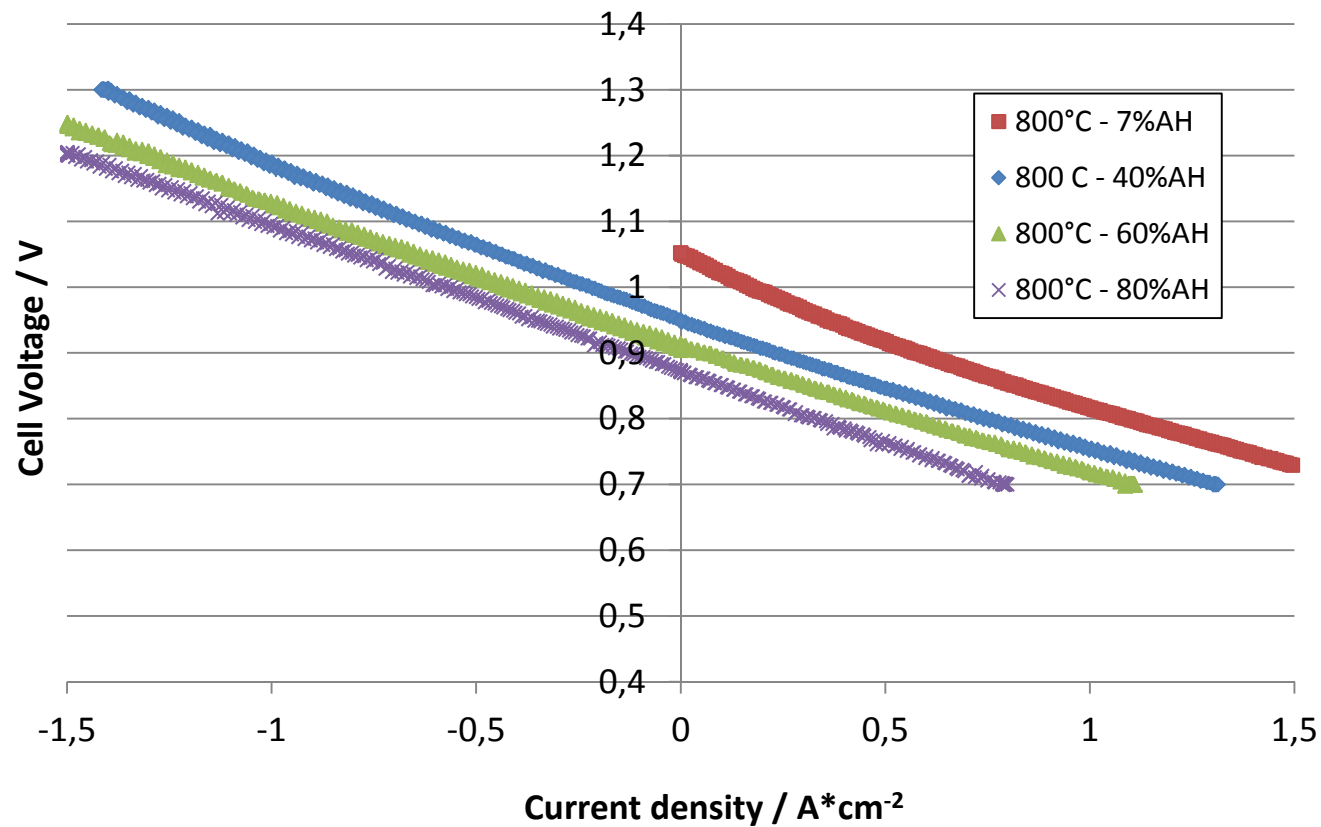
Anode:	$(\text{La,Sr})(\text{Fe,Co})\text{O}_3$
Diffusion barrier:	CGO – 1-5 μm
Electrolyte:	8YSZ – 5-10 μm
Cathode:	Ni/YSZ
Cathode Substrate:	Ni/YSZ



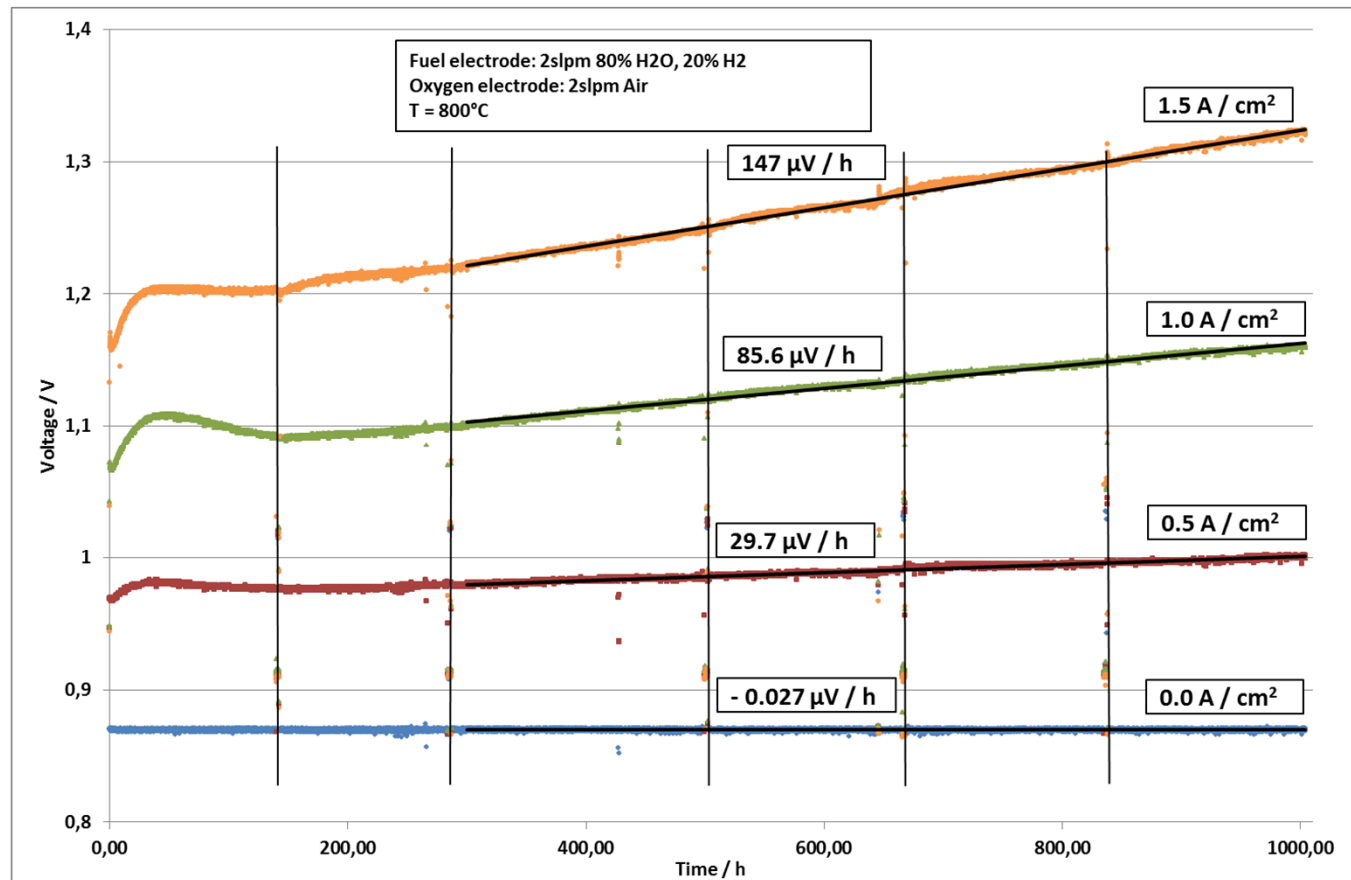
I-V Curves at 750 ° C as a Function of Steam Content (Flow rates: 2 l/min H₂/H₂O, 3 l/min air)



I-V Curves at 800 ° C as a Function of Steam Content (Flow rates: 2 l/min H₂/H₂O, 3 l/min air)



Degradation Experiment and Impedance Data Interpretation

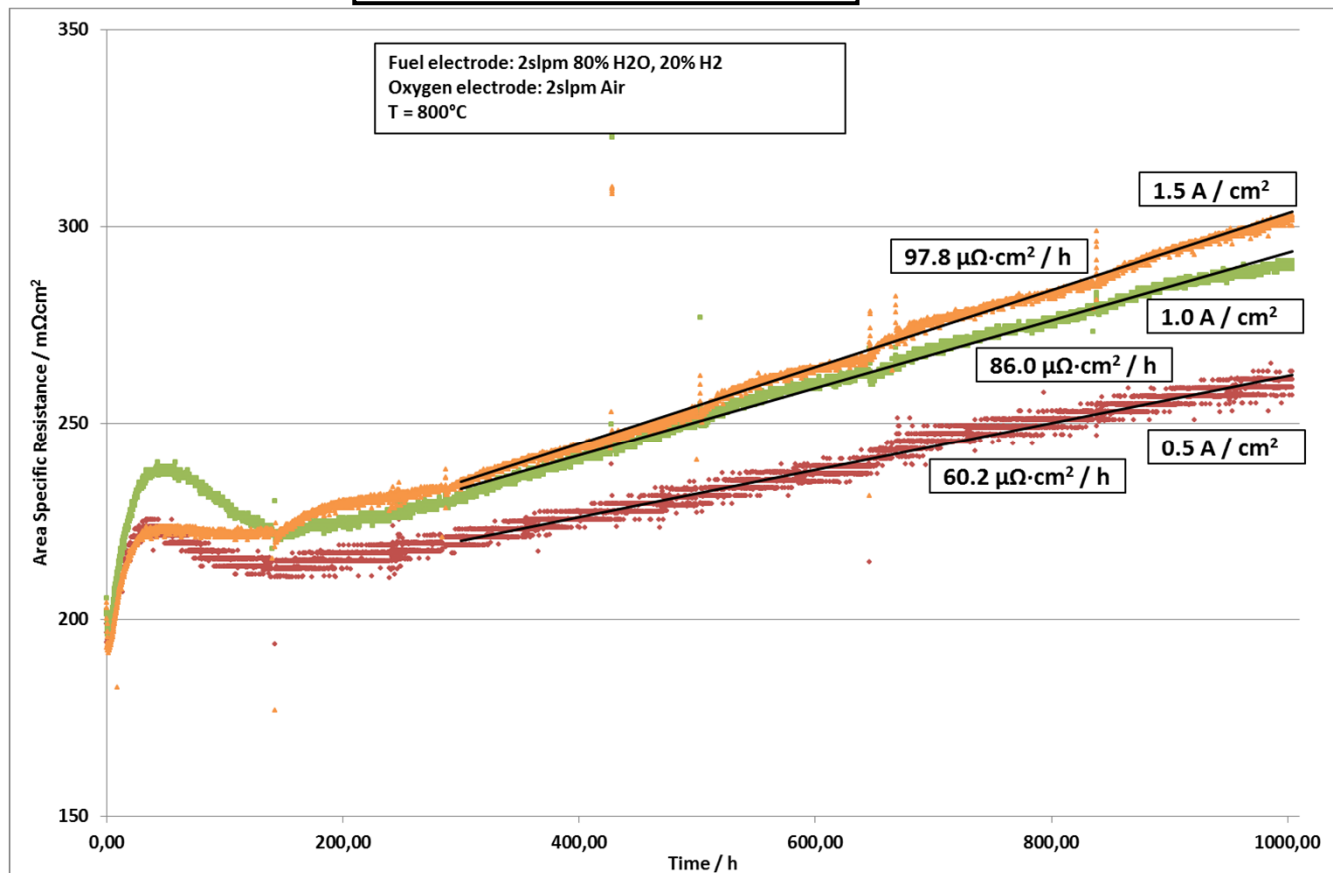


- 4 cells measured simultaneously at different current densities
- Linear degradation after initial phase
- Be careful with interpretation of voltage degradation rate



Degradation Experiment and Impedance Data Interpretation

$$ASR(t) = \frac{U(t) - OCV}{i(t)}$$



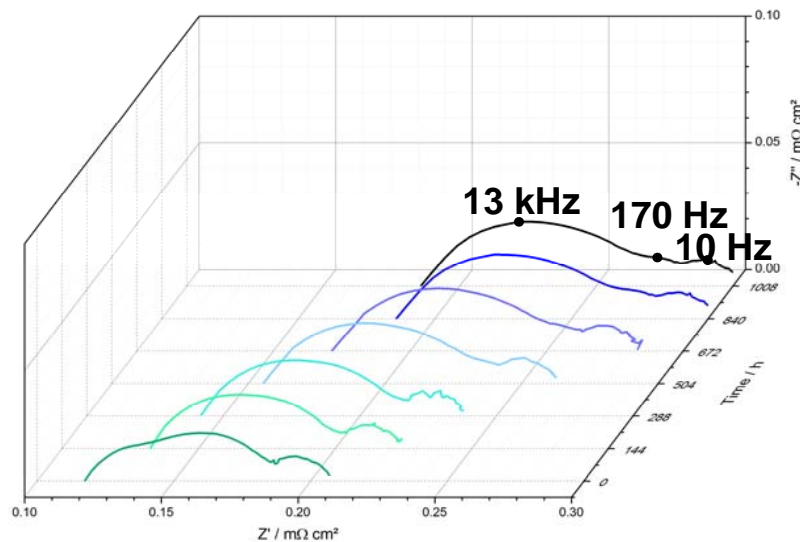
- Degradation rate at 1.5 A/cm² only 13 % higher than at 1.0 A/cm²
- Degradation rate at 0.5 A/cm² significantly lower
- ASR degradation rate about 30% compared to 3% voltage degradation (per 1000 h @ 0.5 A/cm²)



Degradation Experiment and Impedance Data Interpretation

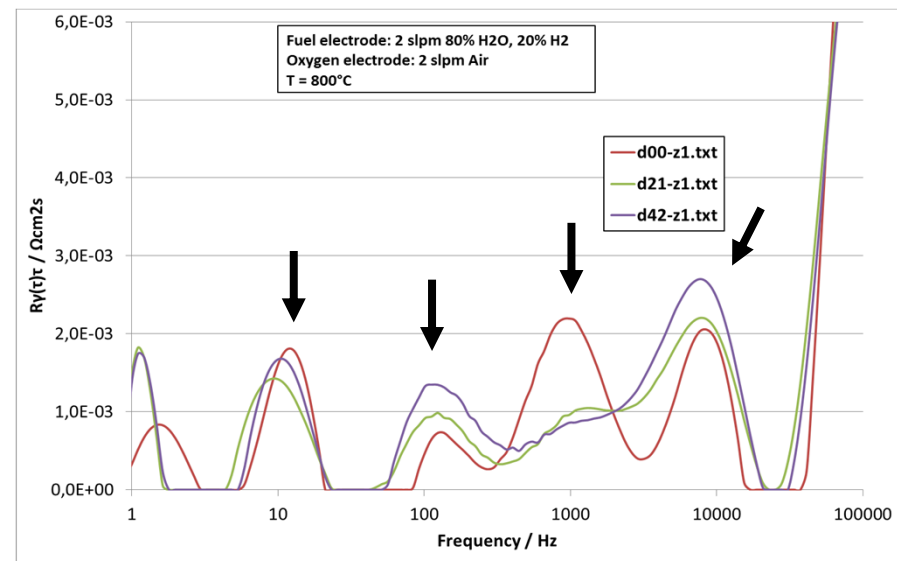
Method 1: DRT-Analysis with parameter variation

Impedance - Spectra



Levenberg-Marquardt
algorithm

DRT-Spectra



Information for improved CNLS fitting



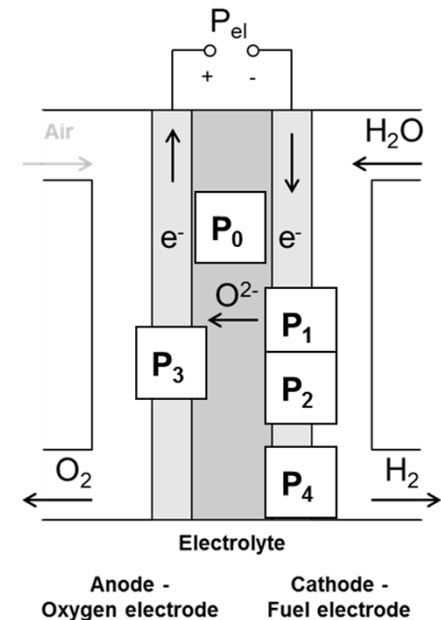
Degradation Experiment and Impedance Data Interpretation

Method 2: Physico-chemical modelling

5 rate limiting processes:

- Ohmic contributions
- First Fuel Electrode (FE) Process: $1\text{-}2\cdot 10^4$ Hz
Charge transfer reaction at TPB coupled with ionic transport in porous electrode geometry
- Second Fuel Electrode (FE) Process: approx. $1\cdot 10^3$ Hz
Charge transfer coupled at TPB
- Oxygen Electrode Process: $1\text{-}2\cdot 10^2$ Hz
- Mass transport limitation: $1\text{-}2\cdot 10^1$ Hz
Diffusion through FE-support along with gas conversion

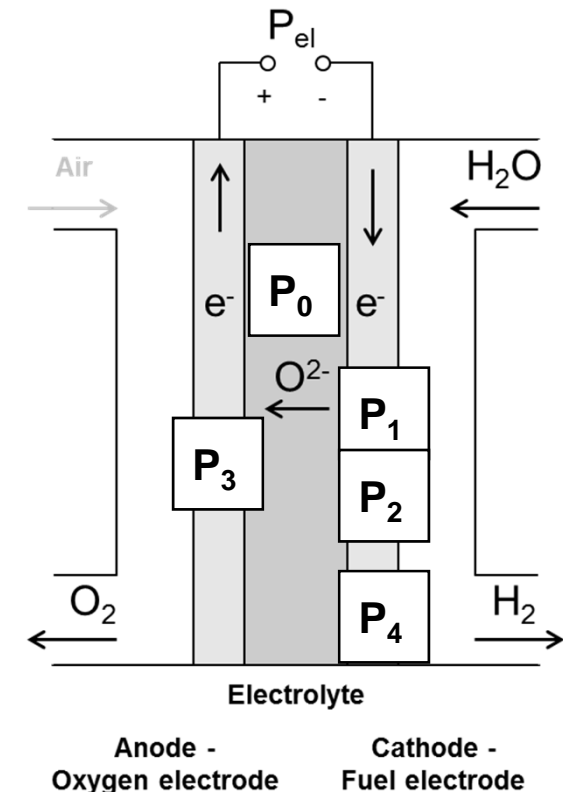
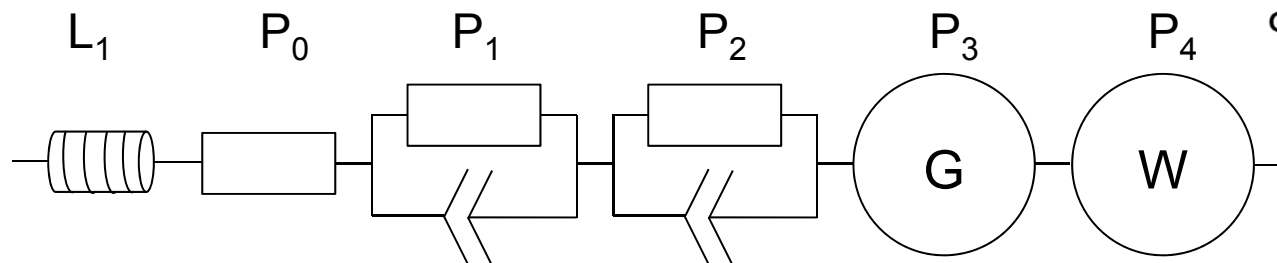
→ Both methods are in good agreement!



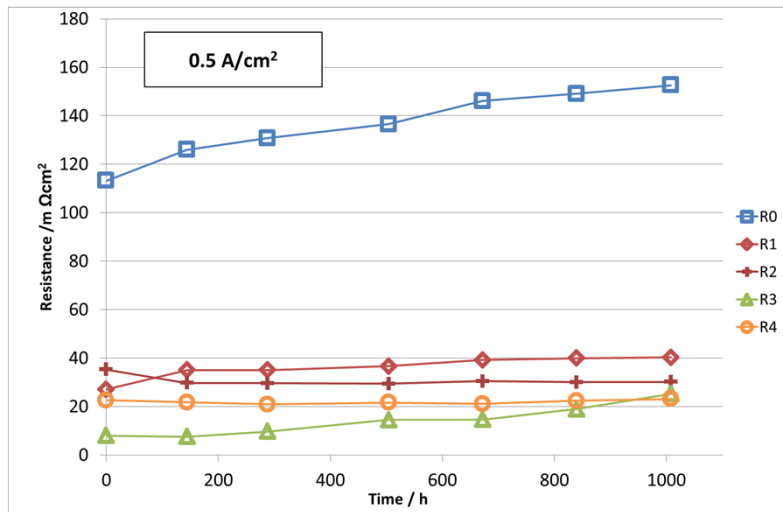
Degradation Experiment and In-situ Data Interpretation

Equivalent circuit model

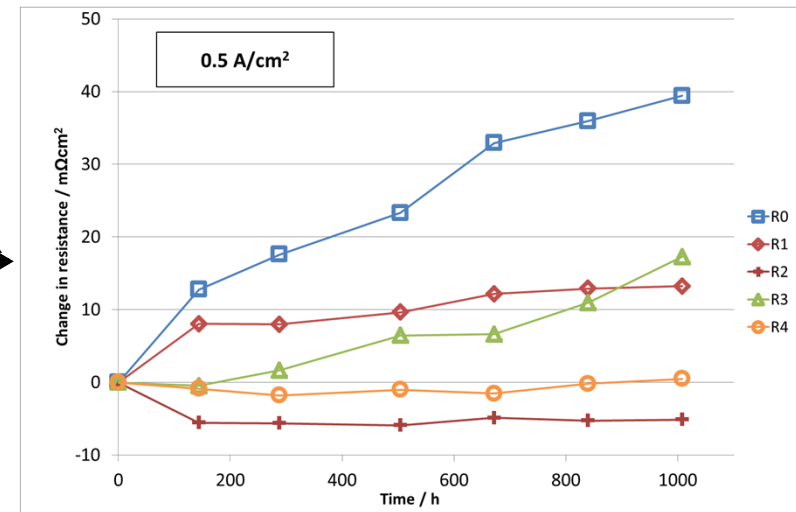
- L_1 : High frequency induction
- P_0 : Ohmic resistance ($> 10^5$ Hz)
- P_1 : Fuel electrode process A ($\sim 10^4$ Hz)
- P_2 : Fuel electrode process B ($\sim 10^3$ Hz)
- P_3 : Oxygen electrode process ($\sim 10^2$ Hz)
- P_4 : Fuel electrode mass transport ($\sim 10^1$ Hz)



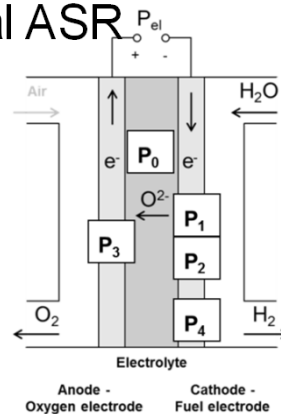
Influence of Current Density on Degradation



ΔR



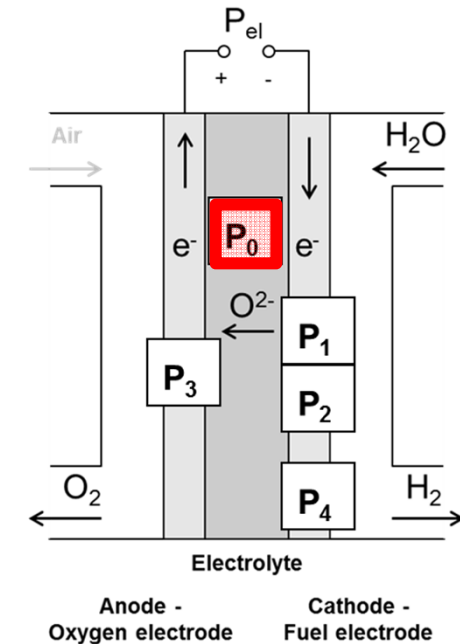
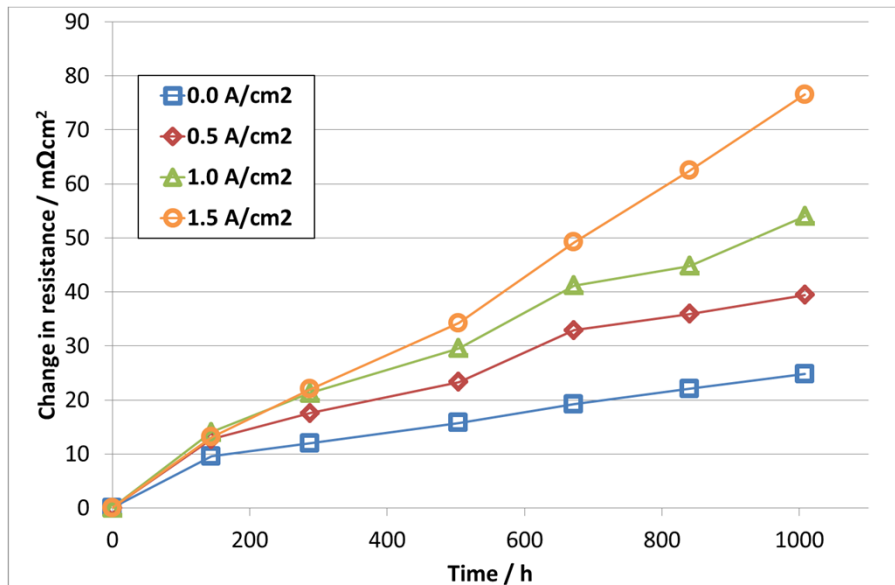
- Ohmic resistance contributes more than 50% of total ASR



- Degradation of ohmic resistance is most severe
- Oxygen electrode has small ASR but high contribution to degradation
- Fuel electrode process 1 degrades while process 2 improves performance



Influence of Current Density on Degradation

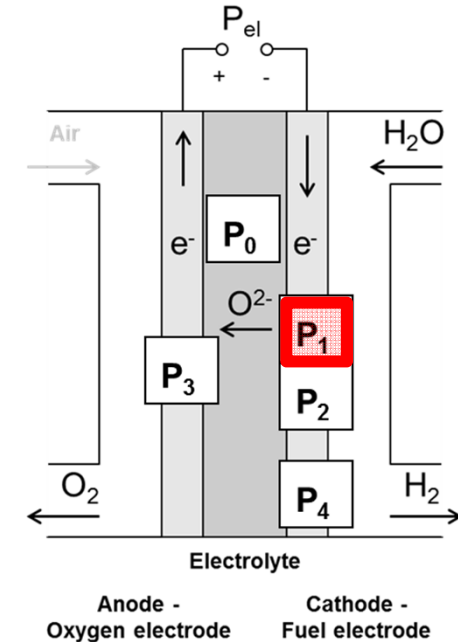
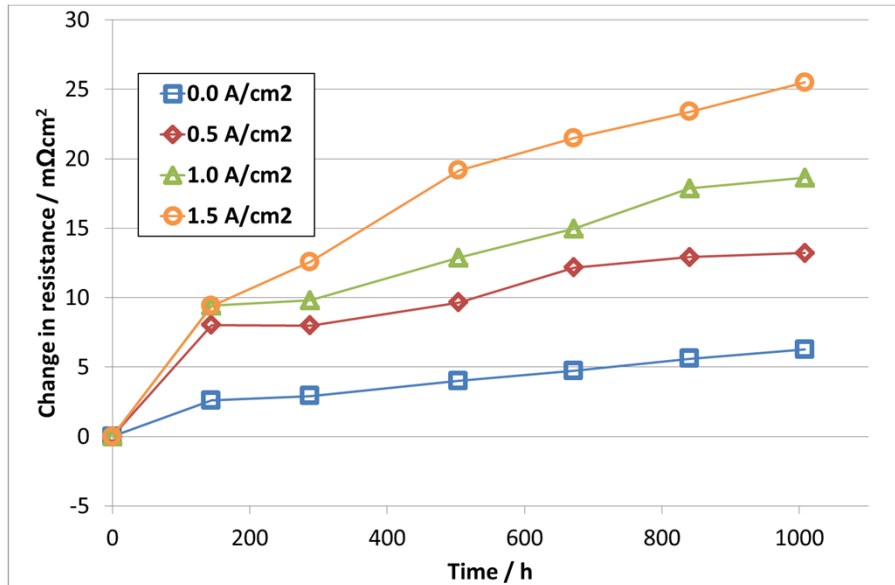


P_0 : Ohmic resistance

- Obvious correlation with current density
- Linear degradation with time



Influence of Current Density on Degradation

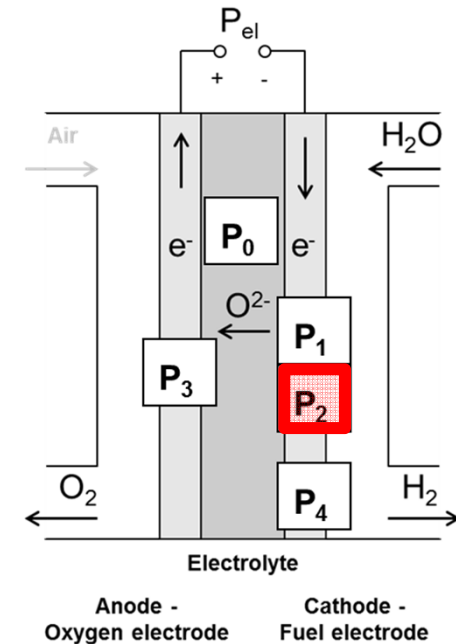
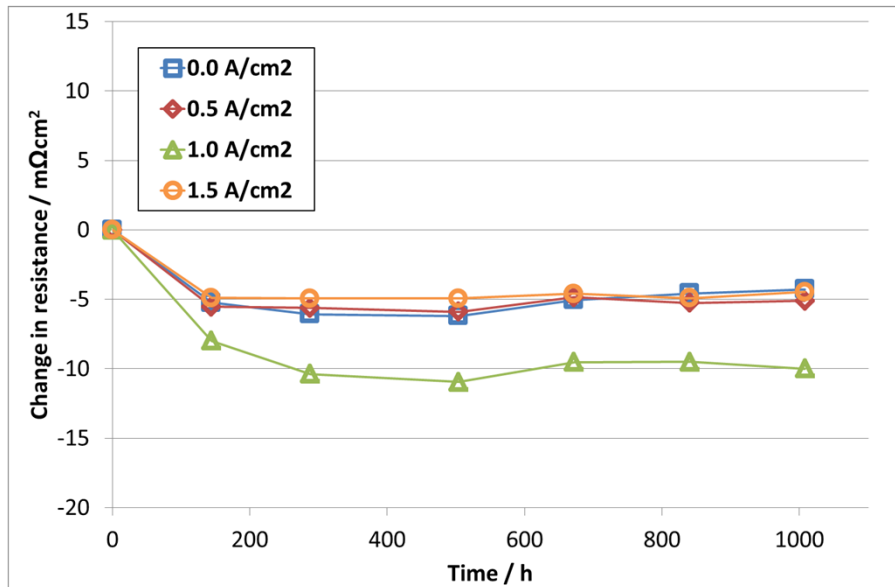


P₁: Fuel electrode process 1

- Also obvious correlation with current density
- Degradation initially fast but slowing down with time



Influence of Current Density on Degradation

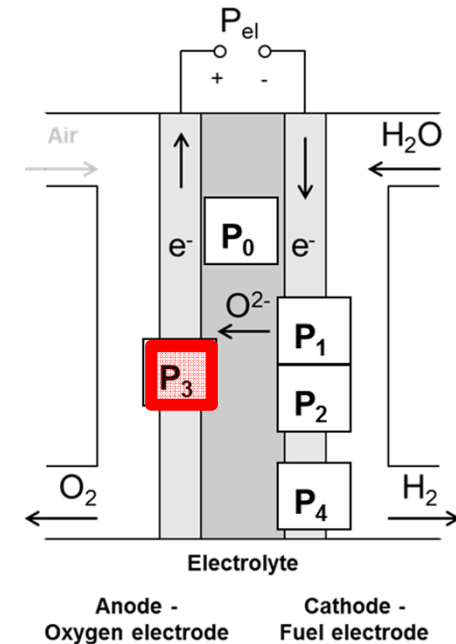
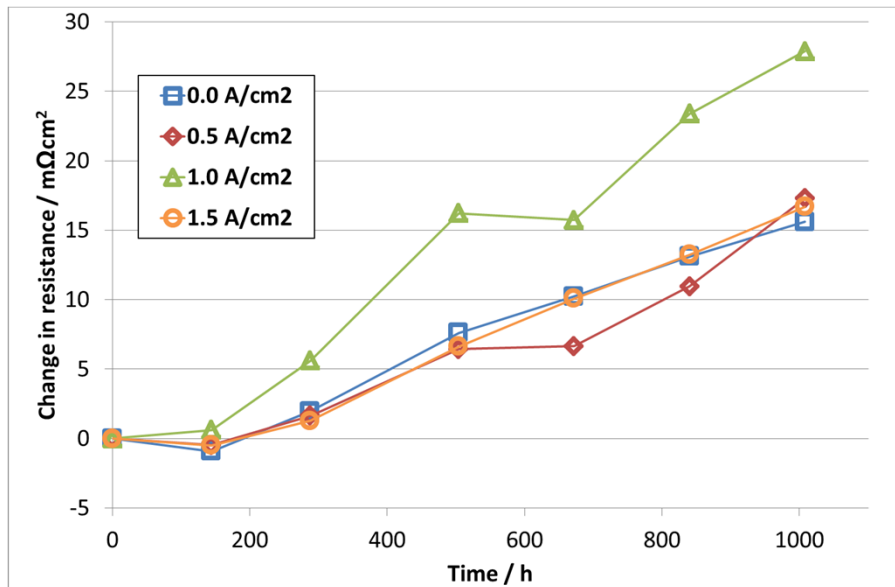


P_2: Fuel electrode process 2

- Offset of 1.0 A/cm² curve is likely artifact (compare process 3)
- Degradation independent of current density
- Initial improvement of performance
- Very stable after initial change



Influence of Current Density on Degradation

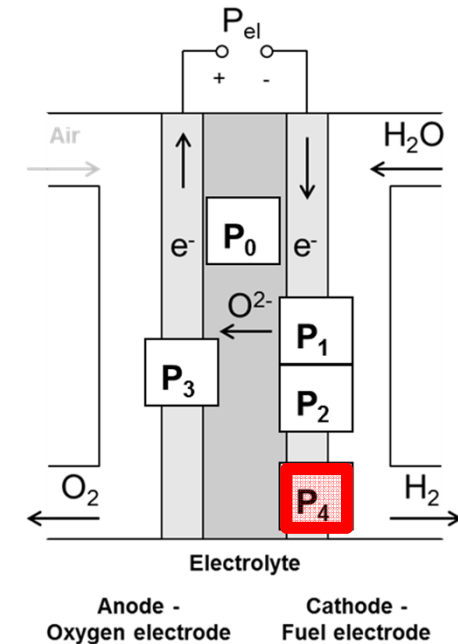
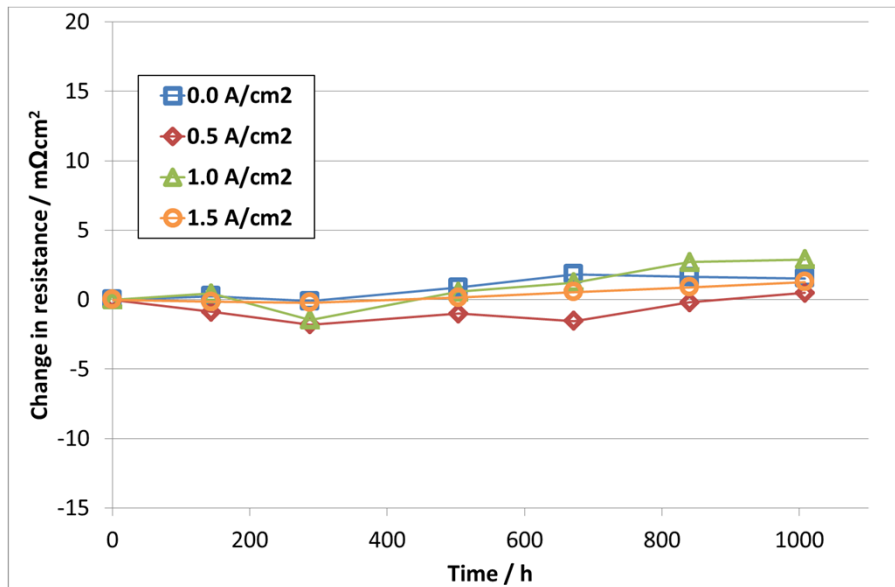


P_3: Oxygen electrode process

- Shift shown by 1.0 A/cm² curve is likely artifact (compare process 2)
- Initially stable → afterwards linear degradation
- Degradation independent of current density



Influence of Current Density on Degradation

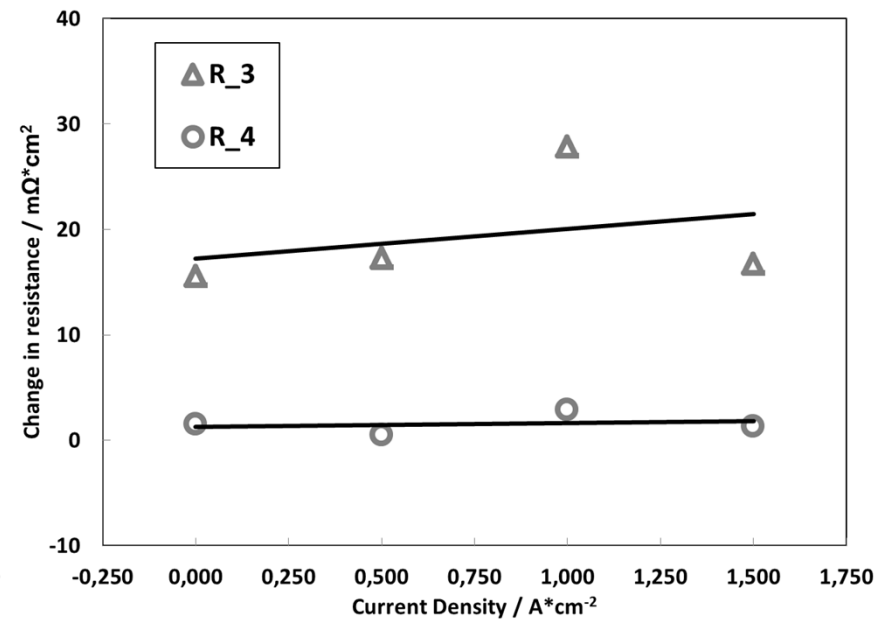
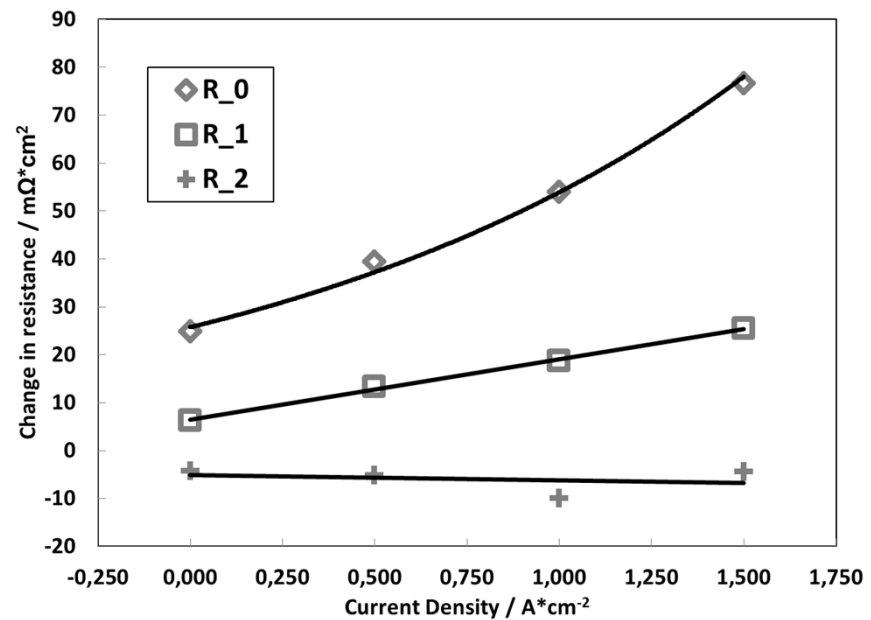


P₄: Fuel electrode mass transport

- Very little degradation
- Independent of current density



Influence of Current Density on Degradation

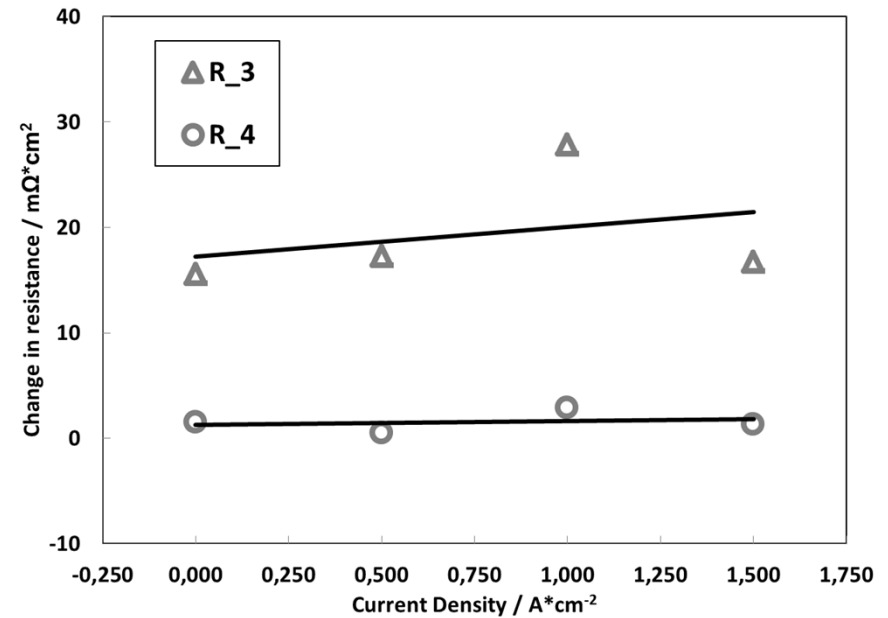
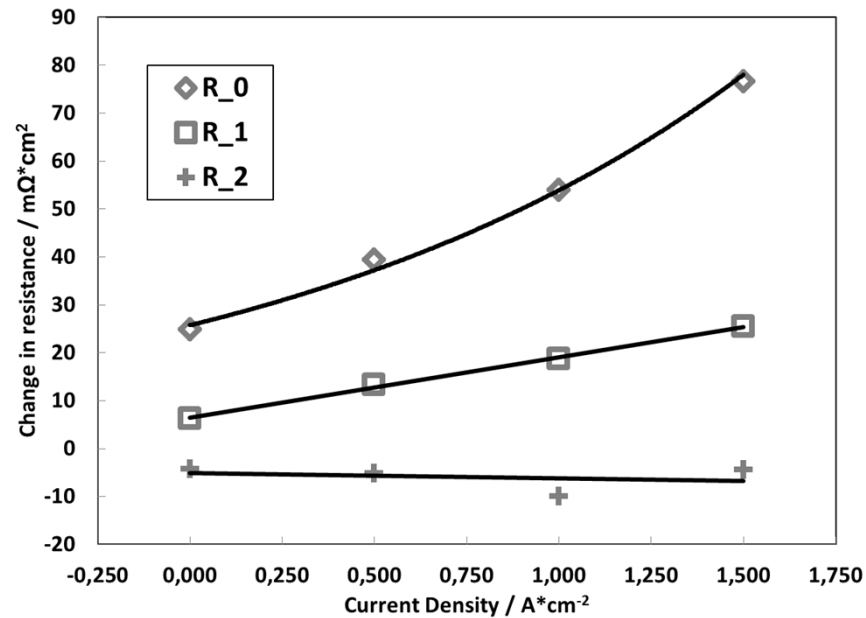


Degradation after 1000 h

- Ohmic resistance: strong dependence on current density
Dependence possibly exponential



Influence of Current Density on Degradation

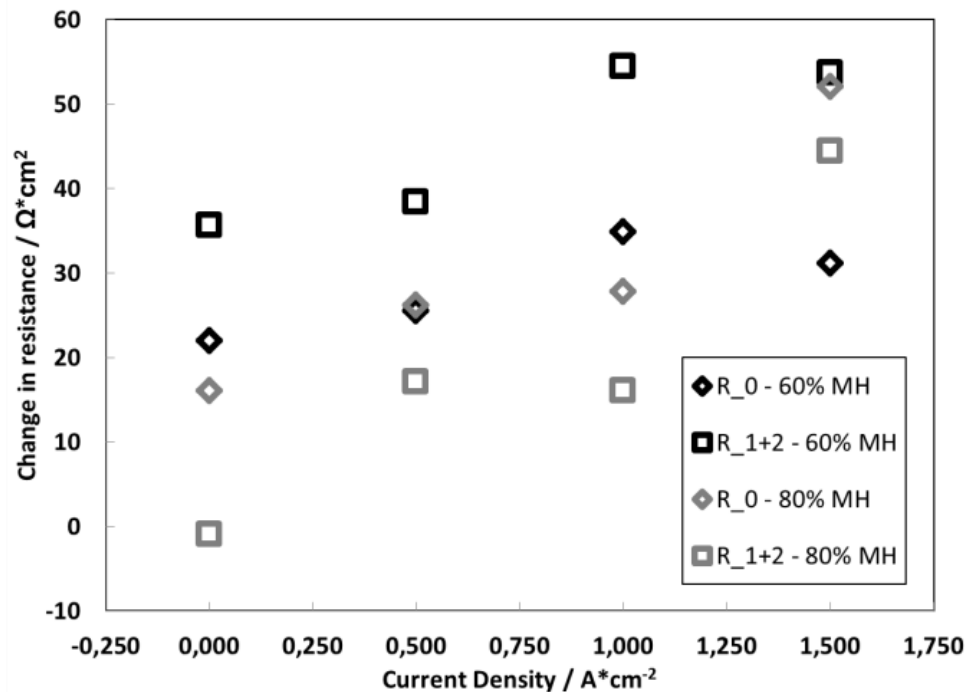


Degradation after 1000 h

- Fuel electrode process 1: clear linear dependence on current density
- Other three processes: no current dependency



Humidification



Ohmic resistance (R_0):

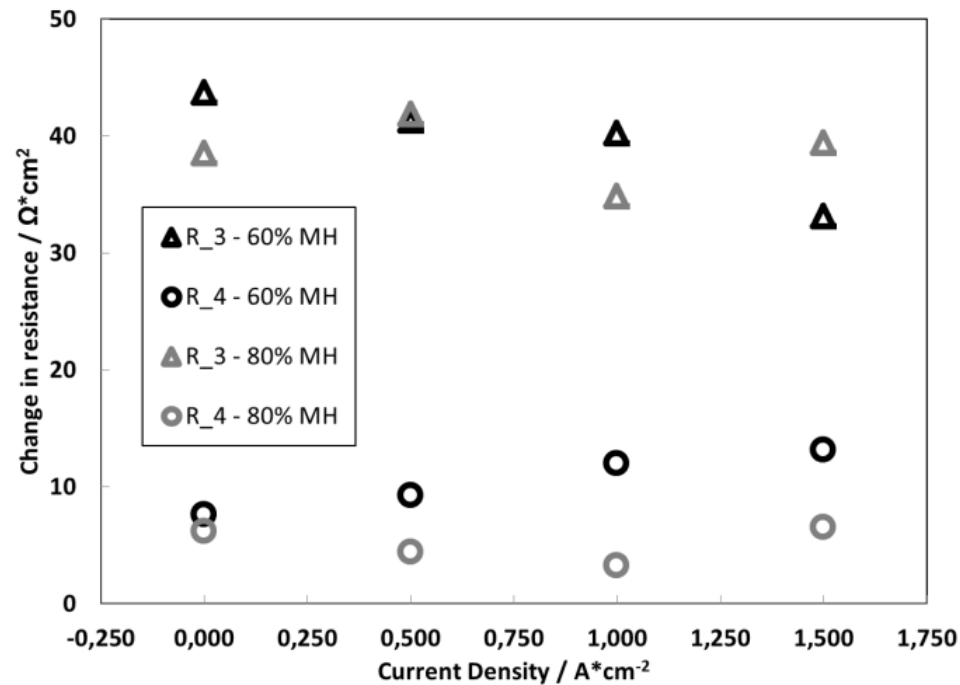
- Dependent on current density

Fuel electrode polarization (R_{1+2}):

- Lower degradation rate at higher humidities...
- ... but higher degradation dependence on current density



Humidification



Oxygen electrode polarization (R_3):

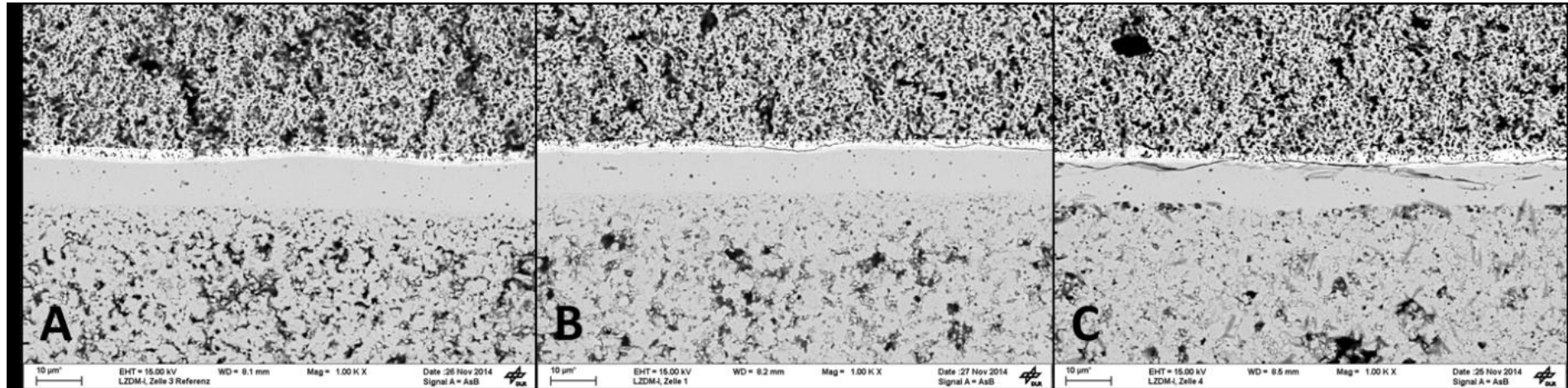
- Humidity has very little influence

Fuel electrode polarization (R_4):

- Generally small degradation
- Lower at higher humidity
- No obvious trend



Post-mortem Analysis – Electrolyte



Reference

1000 h @ OCV

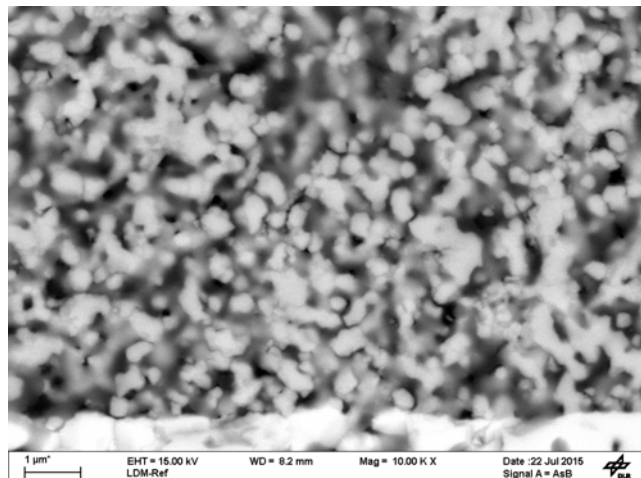
1000 h @ 1.5 A/cm²

Ohmic resistance:

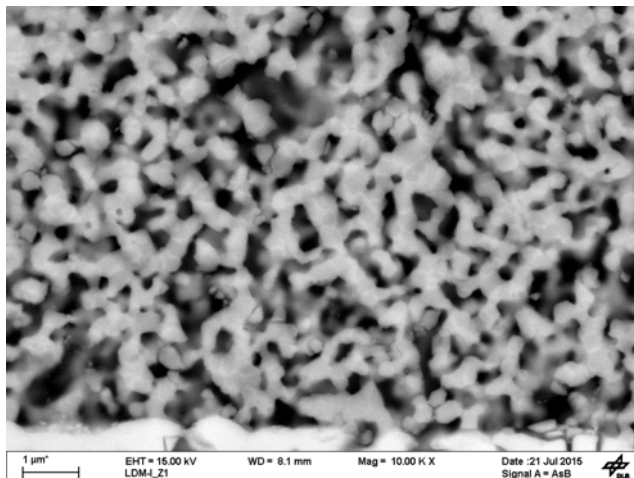
- Weakening of YSZ|CGO|LSCF interface → probably formation of cracks
- Visible cracks probably formed during sample preparation along weakened microstructure



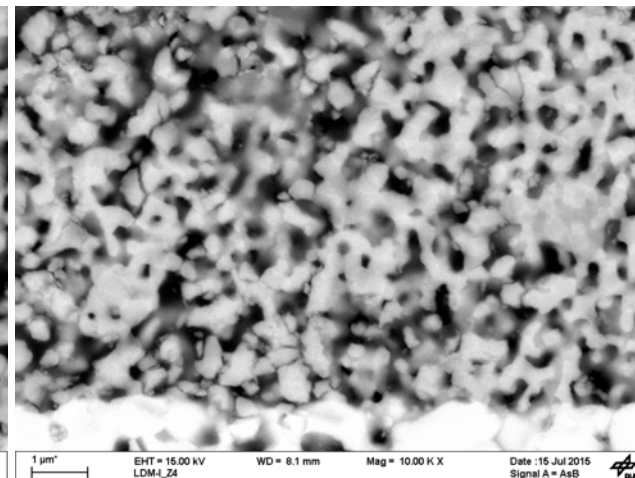
Post-mortem Analysis – Oxygen Electrode



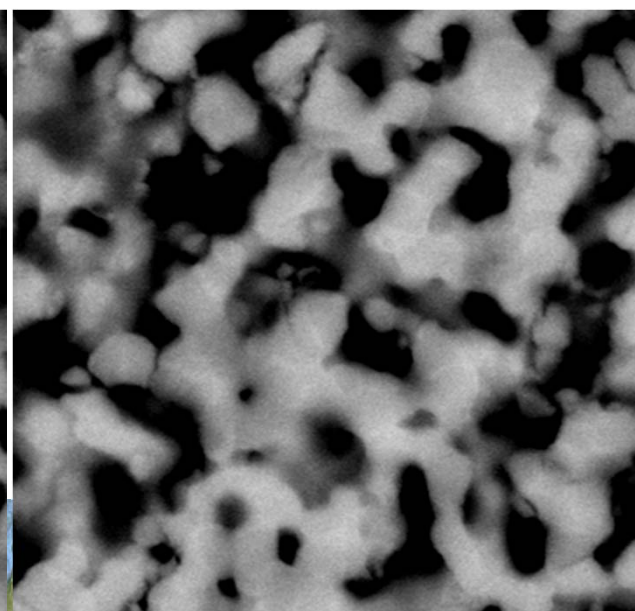
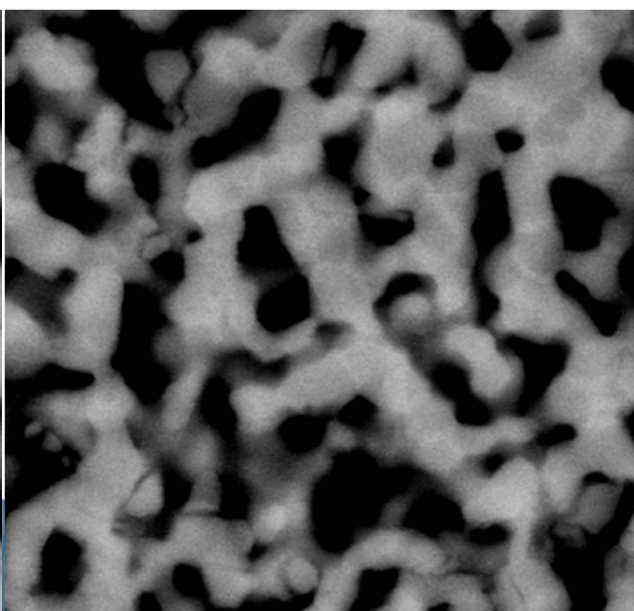
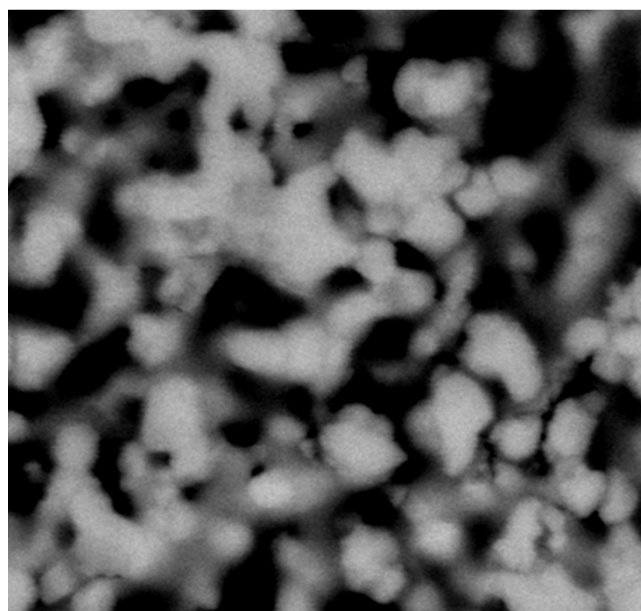
Reference



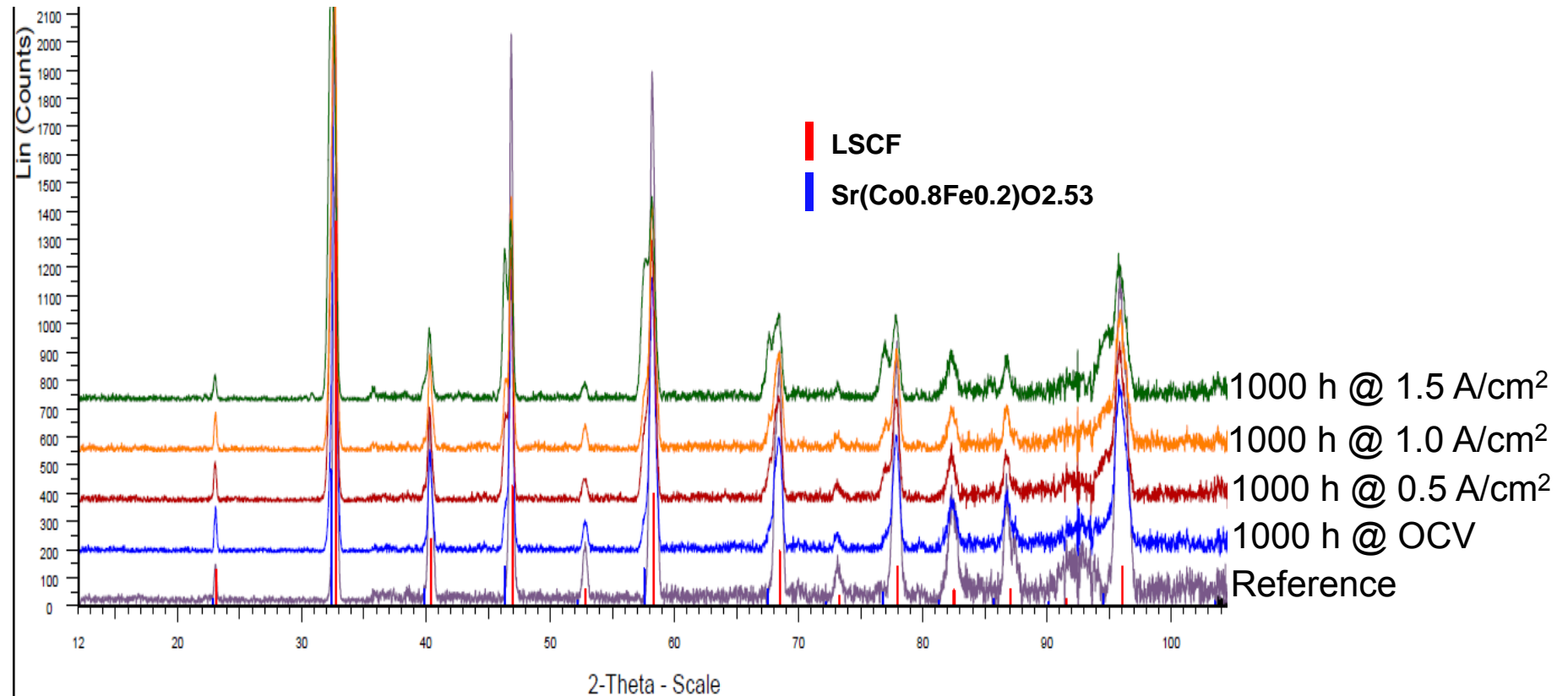
1000 h @ OCV



1000 h @ 1.5 A/cm²



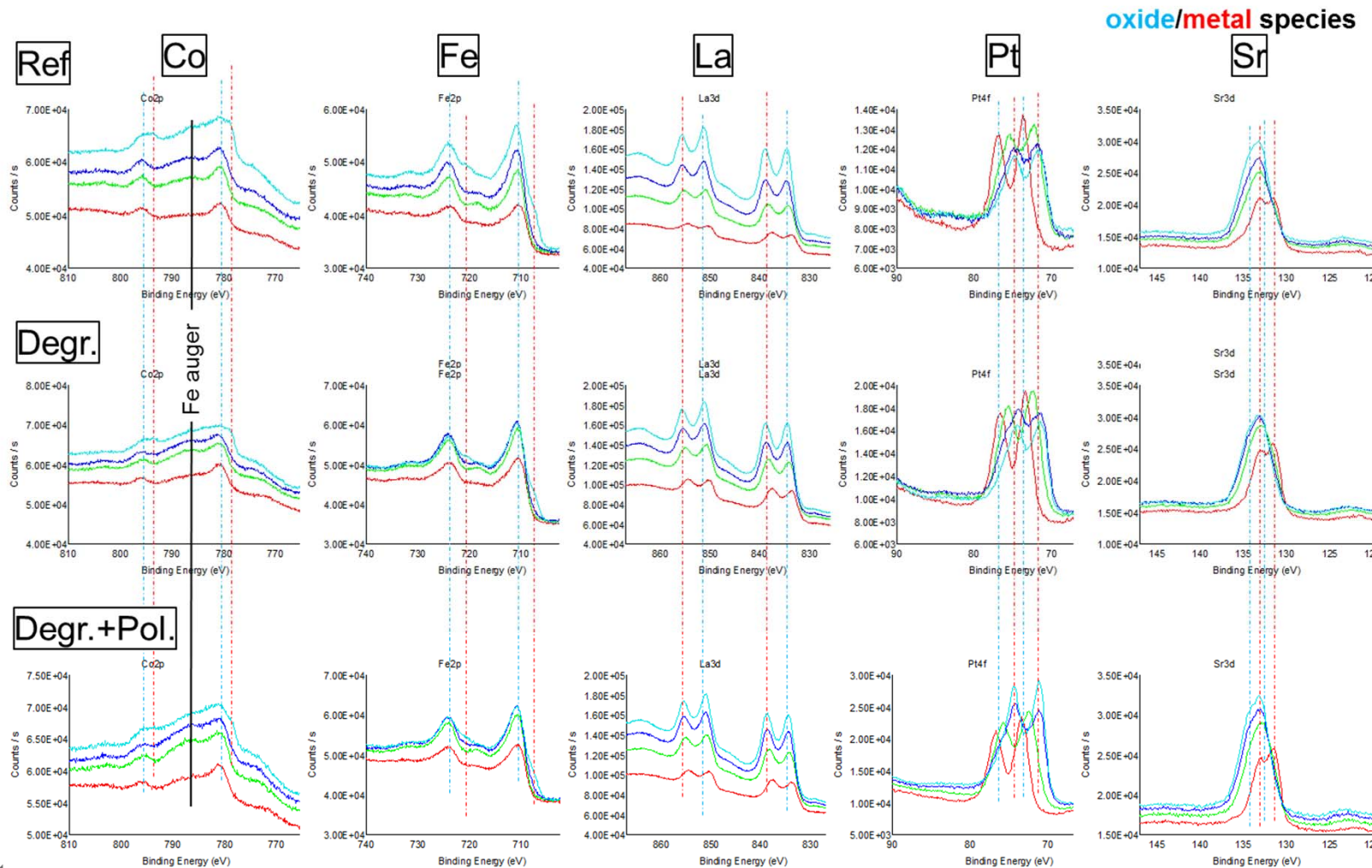
Post-mortem Analysis – Oxygen Electrode



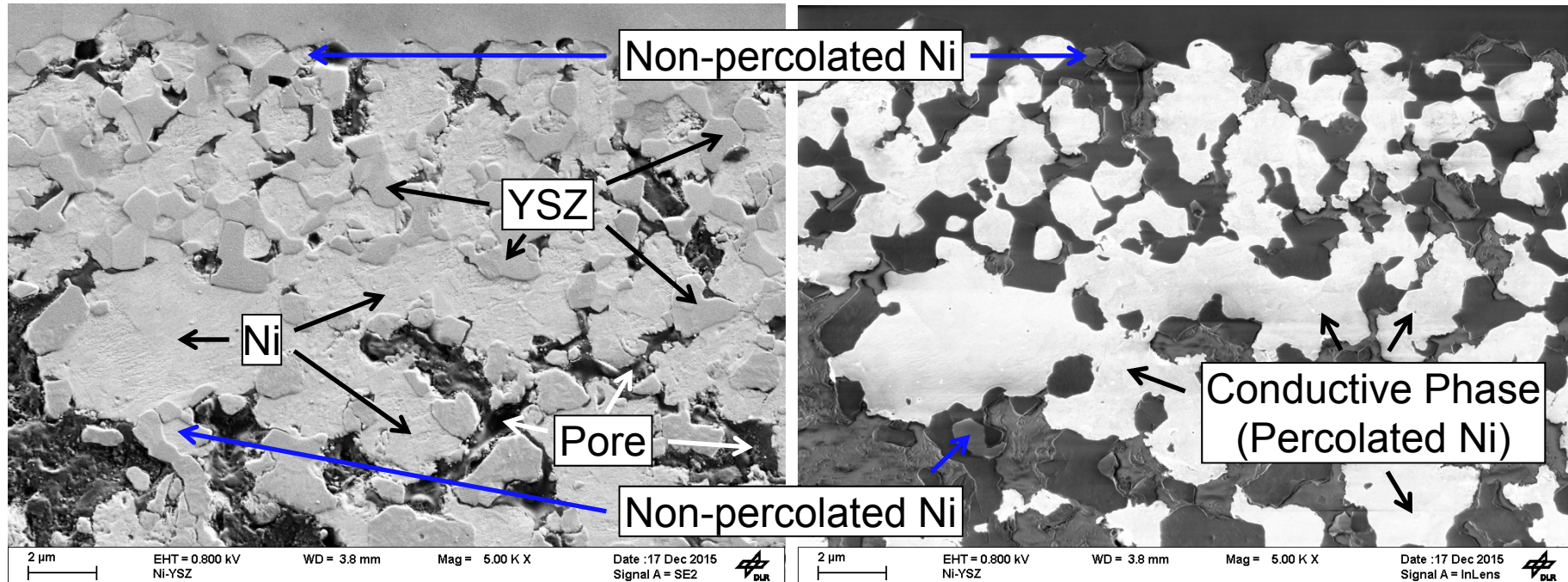
- Formation of a new crystalline compound
- Higher polarization → change more pronounced
- More detailed analyses necessary for reliable information on new phase



Post-mortem Analysis – Oxygen Electrode



Post-mortem Analysis – Fuel Electrode



Percolation

- Ni almost completely percolated
- Ni can be separated from percolation network in cross section

EDX measurement: no Ni depletion

1000 h @ 1.5 A/cm²,
850° C and 80% MH



Conclusion

- Correlation between degradation and current density has been investigated
- Ohmic resistance dominates degradation and increases with current density
- Oxygen electrode contributes significantly to degradation and is independent of current density
- Higher frequency fuel electrode process is significant for degradation and dependent of current density
- Lower frequency fuel electrode process is stable after initial activation and independent of current density
- No degradation in mass transport limitation
- Results of post-mortem analyses give further information and must be further evaluated



Acknowledgment

I'd like to thank my PhD student Michael Hörlein for his scientific work and strong effort and Frank Tietz and his co-workers from Forschungszentrum Jülich for manufacturing and providing cathode-supported cells for electrolysis operation.

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Thank you for your attention

