

1 The DLR SAR Calibration Center

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9

10 **Abstract**

11 A SAR sensor, like every other measurement device, has to be calibrated to perform
12 quantitative measurements. During this process all essential parameters of a SAR image are
13 linked to their geophysical quantities, like the pixel location, their complex-valued backscatter
14 and polarimetric information. The Germany Aerospace Center (DLR) has been a key player in
15 this field for more than 25 years and has concentrated its expertise and technology in
16 performing the calibration of spaceborne SAR sensors to the DLR SAR Calibration Center at
17 the Microwave and Radar Institute. During the last decades the DLR SAR Calibration Center
18 has developed plenty of novel techniques and dedicated reference targets for spaceborne SAR
19 system calibration. Some of these techniques which are also applied to current spaceborne
20 SAR missions like Sentinel-1, TerraSAR-X and TanDEM-X will be presented along with the
21 achievable performance.

22

23 **1 Introduction**

24 While the complexity of modern spaceborne SAR sensors increases, the calibration
25 requirements become more and more stringent. We have to deal with highly agile antennas
26 featuring a raising number of beams and sophisticated operation modes like TOPS (Terrain
27 Observation by Progressive Scans, [1]) or sliding spotlight. Current SAR systems are
28 operational sensors providing high quality products to scientific users and a growing
29 commercial market. For such missions it is important to reduce the in-orbit commissioning

1 phase to the bare minimum, which puts another tight constraint on the calibration activities.
2 These contracting demands require efficient calibration strategies individually adapted to the
3 specific needs of each SAR mission.

4 DLR's Microwaves and Radar Institute has gathered experience in the calibration of
5 spaceborne SAR sensors for many years: starting with ERS-1 (1991) and SIR-C/X-SAR
6 (1994), followed by SRTM (2000) as well as TerraSAR-X (2007), TanDEM-X (2010) and
7 Sentinel-1A (2014) to name the most important ones. The outstanding results with TerraSAR-
8 X & TanDEM-X and several requests by ESA and other international partners triggered the
9 initiative to establish the DLR SAR Calibration Center combining the expertise of an
10 experienced team with adequate facilities and analysis tools. The latest mission supported by
11 the SAR Calibration Center was Sentinel-1A for which in 2014 an independent
12 commissioning phase was performed.

13

14 **2 DLR SAR Calibration Center**

15 The DLR SAR Calibration Center is a well-equipped facility for the calibration of spaceborne
16 SAR systems. An important element of this facility is the infrastructure required to prepare
17 and execute large calibration campaigns. It owns a multitude of calibration targets for
18 different frequency bands and operates and maintains a large calibration field in Southern
19 Germany (Figure 1). This calibration field consists of more than 30 sites hosting 1.5 m and
20 3 m trihedral corner reflectors.

21 Six new calibration sites have been added to this calibration field in 2014 for ESA's
22 Sentinel-1 mission. Three of the sites have been equipped with remote-controlled trihedral
23 corner reflectors (Figure 2), the three other sites host in-house developed C-band transponders
24 (Figure 3) named 'Kalibri'.

25 Beside the transponder development team, the DLR SAR Calibration Center has experts for
26 every step required during calibration which guarantees constant development in the
27 appropriated fields of work. During the commissioning phase of a spaceborne SAR system all
28 members of the calibration team work in parallel on the mission to minimized calibration
29 time.

30

1 **3 Calibration Targets**

2 A radar transponder is an active device which receives an electromagnetic wave, optionally
3 modifies it (e.g. amplification or time delay), and finally retransmits it into space. For
4 calibration purposes transponders with high amplification gain are used to improve the signal-
5 to-background ratio (SBR) over passive targets. They can be also built more flexible i.e. to
6 produce different polarimetric signatures. Furthermore transponders can be extended to be
7 usable as ground receivers recording the signals transmitted by the SAR satellite. Amongst
8 others these data can further be used to retrieve the azimuth pattern of the SAR antenna or to
9 analyze individual radar pulses.

10 The in-house developed C-band transponders ‘Kalibri’ follow a two-antenna design which
11 enables small time delay between receive and transmit and large radar cross sections (RCS)
12 due to reduced back coupling, see Figure 4. All transponder electronics including the antennas
13 are place inside a water-proof housing. In combination with a precise temperature regulation
14 within the box this modern design allows a very stable operation (Table 1). The transponder
15 electronics is split into widely independent modules: the temperature controlling, digital data
16 handling and recording and radio frequency parts are working autonomously and can be
17 replaced individually. This does not only simplify maintenance, but also allows the adaption
18 to other frequency bands: an additional X-band version of the ‘Kalibri’ transponder is
19 likewise developed.

20 The absolute radiometric gain calibration of a target like a transponder is a critical task as it
21 defines the lower boundary for the overall radiometric accuracy of the whole SAR system.
22 The calibration for the ‘Kalibri’ transponders was performed using different measurement
23 setups [2] to provide additional confidence in the results of this extremely critical parameter:
24 Comparison measurements with precisely known trihedral corner reflectors and a circular
25 metal plate have been performed in the DLR’s own compact test range. Secondly, the
26 transponders were used as a radar, measuring trihedral corner reflectors in far field regime. In
27 a third setup, transponders and several corner reflectors were placed within one scene of the
28 Canadian C-band SAR satellite RADARSAT-2 to retrieve the RCS of the transponders
29 without relying on the original satellite calibration [3]. The detailed analysis of the whole
30 calibration campaign can be found in [4].

31 As part of the transponder calibration efforts a novel calibration technique was developed.
32 Extending the well-known ‘Three Antenna Method’ for the absolute gain determination of

1 antennas, the ‘Three Transponder Method’ was proposed [5]. This technique allows the
2 retrieval of the RCS of transponders without using a dedicated RCS reference. Instead
3 distance and frequency measurements are performed which can be conducted with high
4 precision. Due to the measured quantities, this technique allows an easy trace back of the RCS
5 measurement to the International System of Units with known uncertainty.

6 For calibration of ESA’s Sentinel-1 mission a second type of reference targets was also
7 employed: three novel 2.8 m trihedral corner reflectors were installed in DLR’s calibration
8 field. They are very precisely manufactured with a surface accuracy of better than 1 mm
9 which was verified on-site by dedicated measurements. This precision guarantees only small
10 deviation of the corner reflector’s RCS from its theoretical value (Table 2).

11 These new corner reflectors can be remotely controlled enabling unique features. The drives
12 of the corner reflector axes allow a very accurate alignment of better than 0.01 deg which
13 improves the overall accuracy and result in a constant phase center for a given alignment.
14 This is an important feature for radar interferometry. To protect the inner part from hazardous
15 weather conditions and dirt the corner reflectors are moved to a so called ‘parking position’
16 facing downwards when not used. Furthermore remote controlling of the corner reflectors
17 enables the DLR SAR Calibration Center to offer these targets to other agencies for
18 calibration.

19

20 **4 Calibration Procedures**

21 Every SAR mission requires an individual calibration strategy to be developed to satisfy its
22 system requirements and to release SAR products as soon as possible. One already proven
23 and established concept for calibration is based on an antenna model approach [6] to predict
24 the performance of the hundredths of beams of a modern active phased array antenna, which
25 is often employed. The calibration itself then consists of:

- 26 • Internal Calibration, for stable instrument performance over time.
- 27 • Geometric Calibration, to assign the SAR data to the geographic location on the
28 Earth’s surface.
- 29 • Antenna Pointing Determination, to precisely retrieve the beam direction of the
30 antenna.

- Antenna Model Verification, to verify the precision of the reference patterns generated by the model, including the gain offset between different beams.
- Polarimetric Calibration to align data between different polarimetric channels.
- Absolute Radiometric Calibration, for radiometric bias correction of SAR data products.

5 Calibration Techniques

Absolute radiometric calibration is one of the most critical tasks performed during commissioning phase of a SAR satellite. Several reference targets have to be used to achieve today's accuracy demands. The existing and well-equipped calibration field of the DLR SAR Calibration Center is a big advantage when performing this task.

The impulse response from each aligned reference target can be utilized to derive the calibration factor of the SAR instrument. An increasing number of targets or overpasses can be used to reduce the statistical uncertainty associated with every single measurement. For the retrieval the complex-valued image is interpolated in frequency domain, the total target power is accumulated and finally compensated for noise. This value will then be compared to the RCS of the target to derive the calibration factor. Linking all uncertainties, i.e. from the RCS measurement, the target's RCS knowledge and the propagation path a combined uncertainty for the measurement can be derived.

The most important point with respect to radiometric accuracy is the stability of a system like TerraSAR-X. Due to a re-calibration campaign two years after launch, extended by measuring several beams and a couple of reference targets, a precise evaluation of the stability with a high confidence level could be achieved. For this purpose, the absolute calibration factor averaged over all measurements performed in 2009, see Figure 5, has been compared to that derived from measurements performed during the commissioning phase in 2007. Consequently, an offset between both values is a measure for the stability. For a period of two years a radiometric stability of 0.15 dB could be proved for TerraSAR-X. This stability is more than one magnitude better than the requirement with 0.5 dB over six months.

For the TanDEM-X system an absolute radiometric accuracy of 0.14 dB was achieved for StripMap operation during the commissioning phase. Considering furthermore the same radiometric stability as the earlier launched TerraSAR-X satellite and propagation

1 uncertainties of 0.25 dB, an absolute radiometric accuracy of less than 0.5 dB could be
2 achieved for the mission time [6].

3 Linking a pixel position of the SAR image to a location on Earth is called *geometric*
4 *calibration*. Beside a precise knowledge of the target and the satellite location, the
5 propagation path has to be known. Especially, the delay, bending and dispersion of the
6 atmosphere, namely troposphere and ionosphere, have to be considered [7], [8].

7 The influence of the troposphere on the signal is frequency-independent and can be split into
8 a slowly varying hydrostatic (several meters in range) and a weather-dependent wet delay
9 (few centimeters offset). The ionosphere has a frequency dependency and is dispersive, which
10 mostly affects signals with frequencies below S-band. The range shift Δr can be quantified by
11 the total electron count (TEC) on the propagation path [9]:

$$12 \quad \Delta r \approx \frac{40.31 \frac{\text{m}^2}{\text{s}^2}}{f^2} \cdot \text{TEC} \quad (1)$$

13 where f is the frequency. This equation is also widely used by global navigation satellite
14 systems (GNSS) like GPS or Galileo.

15 Faraday rotation is a second effect caused by the ionosphere. It depends not only on TEC, but
16 also on the strength of the Earth's magnetic field along the propagation path:

$$17 \quad \psi = 2.610^{-13} \cdot \text{TEC} \cdot B \cdot \lambda^2 \cdot \cos(\theta) \quad (2)$$

18 with ψ in radian, TEC in electrons per m^2 , B the Earth's magnetic field, λ the wavelength and
19 θ the angle between the radar illumination and the magnetic field. The Faraday rotation angle
20 ψ is changing the orientation of linear polarized waves or expresses itself as an additional
21 phase offset for circular polarization.

22 The accurate mapping of a SAR image pixel to the Earth surface is finally performed by using
23 point targets like corner reflectors with known phase center as reference and accounting for
24 propagation effects. The results from the TerraSAR-X mission are shown in Figure 6. For
25 look angles up to about 40 deg, the slant range with a distance of about 600 km could be
26 derived down to an accuracy of 6 cm. At higher look angles, the variance of the residual error
27 increases as the propagation path through the atmosphere is longer. Nevertheless, considering
28 the complete range of look angles a pixel localization accuracy of 30 cm could be achieved
29 for TerraSAR-X.

1 To properly illuminate the scene and to correctly apply the antenna pattern correction during
2 SAR data processing the antenna pointing of a SAR instrument has to be known precisely.
3 The *antenna pointing calibration* estimates the difference between the real antenna pointing
4 and the desired one. This can be done by commanding regular beams or so called notch
5 beams on the phase array antenna either in elevation or in azimuth. Based on the gain drop of
6 notch beams, the boresight direction can accurately be recognized. For regular beams the
7 maximum power has to be determined.

8 Scenes over the Amazon rainforest which have a very homogeneous backscatter characteristic
9 can be used to derive the pointing in elevation. The azimuth or flight-direction pointing can be
10 found by analyzing ground receiver recordings. Ground receivers are used to store the power
11 received from the SAR instrument annotated with a precise time stamp. Knowing the satellite
12 and target position, the azimuth antenna pattern and consequently the real pointing in flight-
13 direction can be reconstructed from that data [15].

14 For TerraSAR-X and TanDEM-X the antenna pointing knowledge was proven to be better
15 than 0.002 deg in elevation, see Figure 7. By readjusting the attitude of the satellite, the
16 detected mispointing of the antenna beam can still be compensated.

17 Recordings from ground receivers can also be used to *verify the antenna model* of the SAR
18 instrument for different beams [13]. The modelled antenna pattern is compared to the
19 reconstructed data from ground measurements. Even for the complicated case of TOPS
20 (Terrain Observation with Progressive Scan) acquisition the DLR SAR Calibration Center
21 was able to successfully check the antenna model of Sentinel-1A see [10], [11], and Figure 8.
22 In TOPS operation hundredths of beams are commanded to steer the antenna main lobe from
23 sub-swath to sub-swath over an area of interest. This can be also seen in Figure 8 where several
24 main beams are visible (e.g. at about -0.2 s, 0.1 s or 0.3 s) together with the discontinuities in
25 between which occur when switching to another sub-swath (e.g. at about 0.2 deg in azimuth).

26 The DLR SAR Calibration Center is also permanently developing and improving its
27 calibration techniques. The pulse coded calibration (PCC) method [12] is one of them. It can
28 be applied to characterize the transmit-receive-modules (TRMs) of active phased array
29 antennas. As part of the *internal calibration* of a SAR instrument, several measurements are
30 performed on the phase array antenna where the phase shifters of the TRMs are varied
31 between 0 and 180 degree in a pseudo noise manner. From these measurements the deviation
32 of the TRMs from their nominal state can be retrieved while all modules are in full operation.

1 The accuracy of this technique was proven to be better than some hundredth of a dB in
2 amplitude and several tenth of a degree in phase [10].

3 Figure 9 shows the amplitude and phase drift of the Sentinel-1A instrument for a 25 minutes
4 Stripmap data take (DT), and the corresponding temperature variation in the front-end. The
5 instrument amplitude drift for such a long data take is less than 0.3 dB, while the phase drifts
6 about 12 deg. During this time, the front-end temperature increases by 16 °C. Theoretically,
7 this corresponds to an instrument drift of 0.012 dB and 0.007 deg per minute, which proves
8 the very high stability of the Sentinel-1A instrument and the accuracy of the PCC technique.
9 Furthermore, the measured instrument drift is compensated for at raw data level during SAR
10 data processing, so that the remaining instrument contribution to the SAR image is smaller
11 than 0.1 dB in amplitude and only a few degrees in phase.

12 A wide variety of analysis and calibration tools have also been developed by the Microwave
13 and Radar Institute during the last years. They support the calibration team in deriving the
14 various calibration parameters during the commissioning phase and in nominal operation of a
15 spaceborne SAR system. These tools are constantly enhanced and adapted to the individual
16 SAR missions to meet their specific requirements.

17 The tool CALIX is used to perform point and distributed target analysis. It reads focused SAR
18 data to extract image information like pixel location, resolution, side lobe level, background
19 noise and absolute target energy for single point targets. Also polarimetric information can be
20 extracted. The CALIX program can be used via a graphical user interface or by external
21 scripts for semi-automatic analysis. But also analysis tools for internal calibration and for
22 characterizing the antenna in-flight have been developed and are permanently improved and
23 adapted for the corresponding mission. Other tools are dedicated to calculate the alignment
24 angles for targets in the calibration field for a given satellite overpass or to design a
25 calibration field based on the orbit of a future SAR satellite.

26

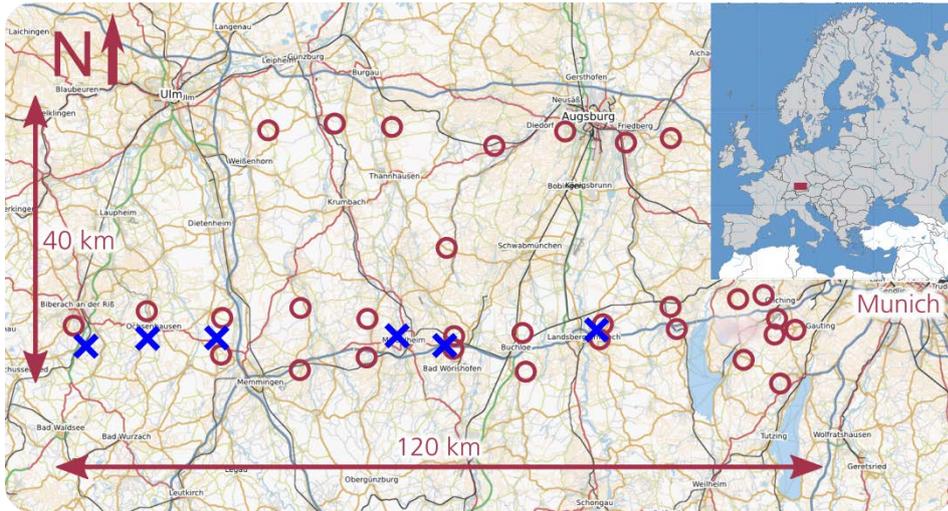
27 **6 Conclusion**

28 The complexity of SAR instruments and their calibration has increased during the last years
29 while the demand on highly accurate spaceborne SAR data products rose. To keep pace with
30 this development, the DLR SAR Calibration Center of the Microwave and Radar Institute has
31 built up, maintained and extended its calibration facilities. Efficient calibration concepts have

1 been developed based on innovative methods, like the antenna model approach or the PCC
2 technique. New innovative targets like remote-controlled trihedral corner reflectors or the
3 in-house developed C-band transponders ‘Kalibri’, as well as novel tools for product quality
4 control and performance analysis have been developed. An overview over the achievable
5 accuracies was given for the most relevant aspects of spaceborne SAR calibration
6 (summarized in Table 3).

7

1



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3 Figure 1 The DLR calibration field consists of 36 target positions with 20 corner reflectors
4 permanently installed. The newly installed six remote controlled targets are marked by blue
5 crosses. (Map: © OpenStreetMap contributors, Overview: David Liuzzo, CC-BY-SA-2.0-de)

6



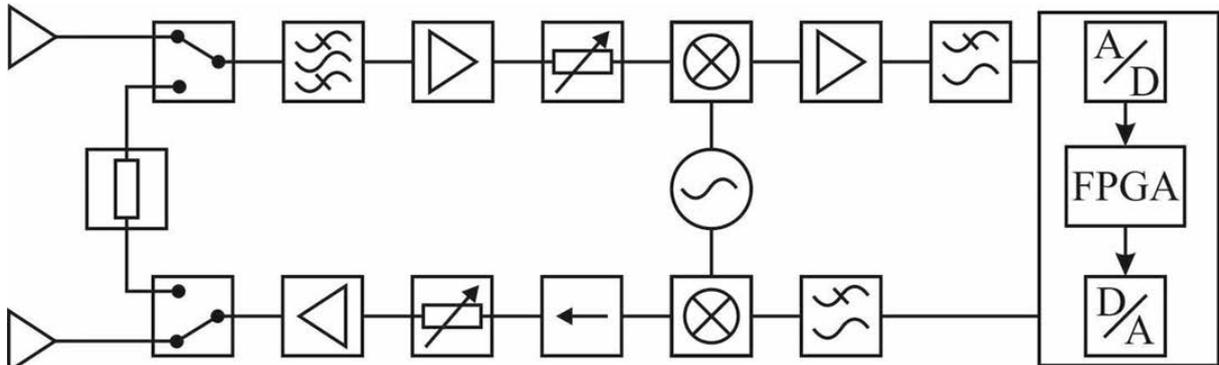
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8 Figure 2 New remote-controlled corner reflector with a leg length of 2.8 m.



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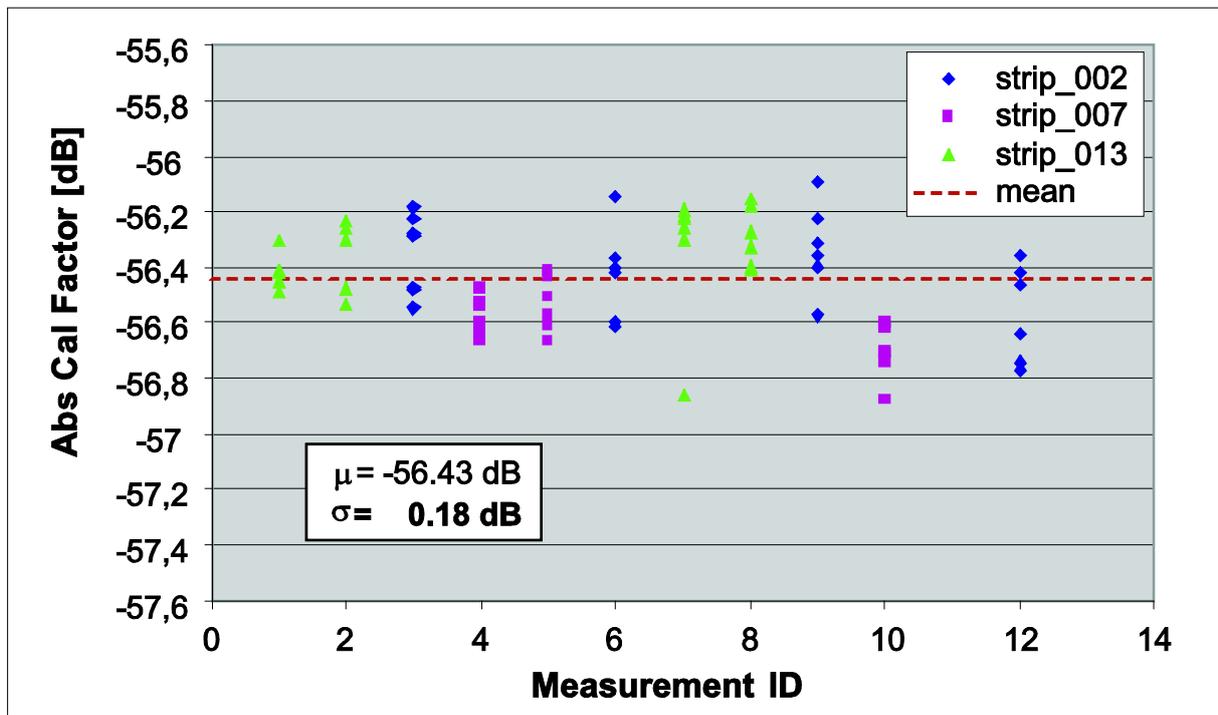
2 Figure 3 C-band remote-controlled 'Kalibri' transponder, housing of the positioner removed.



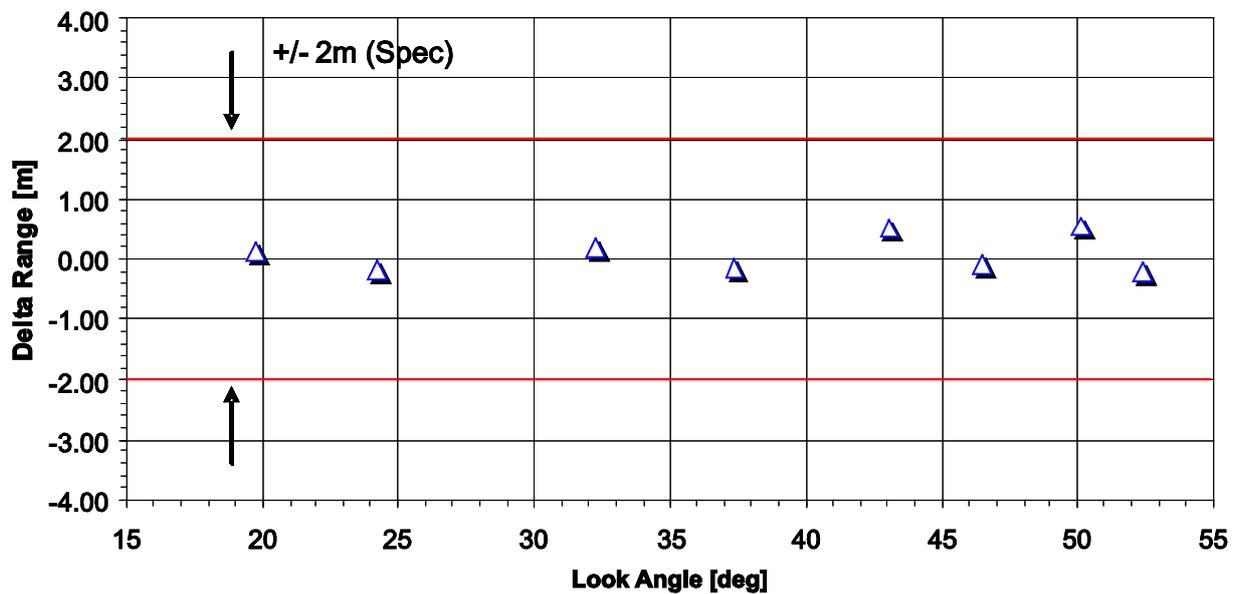
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4 Figure 4 Basic scheme of the 'Kalibri' transponder including up- and down-conversion

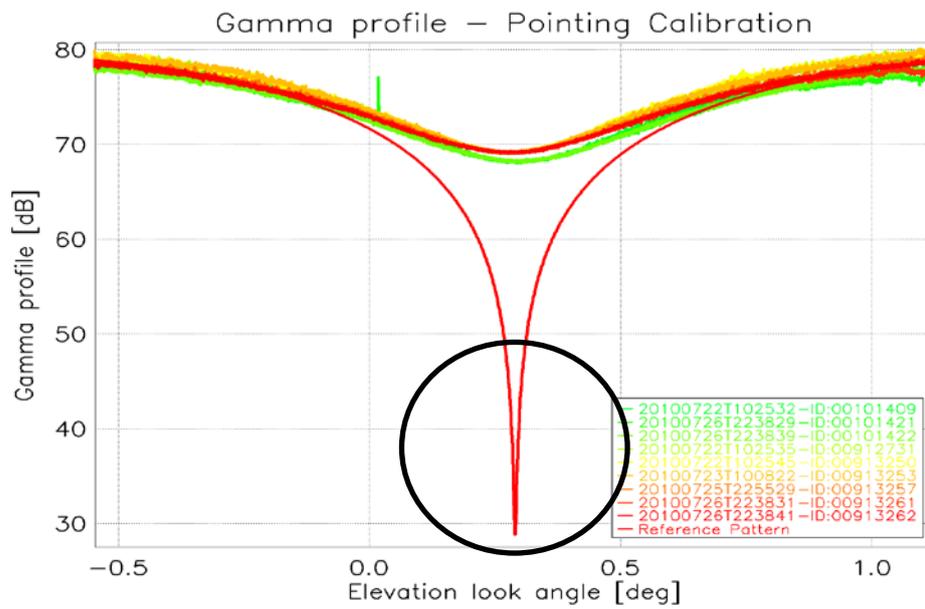
5 stages.



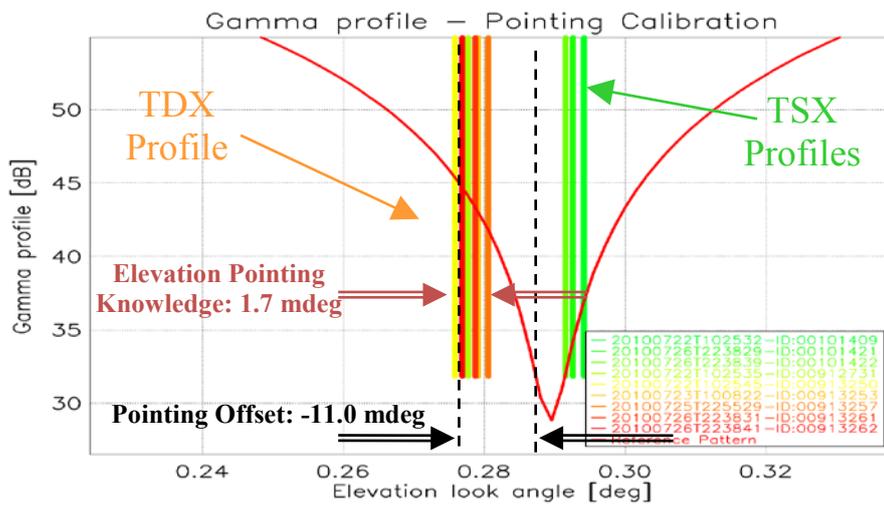
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 2 Figure 5 Absolute calibration factor versus measurement ID, derived from all reference
 3 targets deployed for re-calibrating TerraSAR-X in 2009. The instrument was operated in
 4 different StripMap beams [14].



5
 6 Figure 6 Residual slant range offset in dependence of the look angle after correcting for
 7 instrument delay and propagation effects [6].

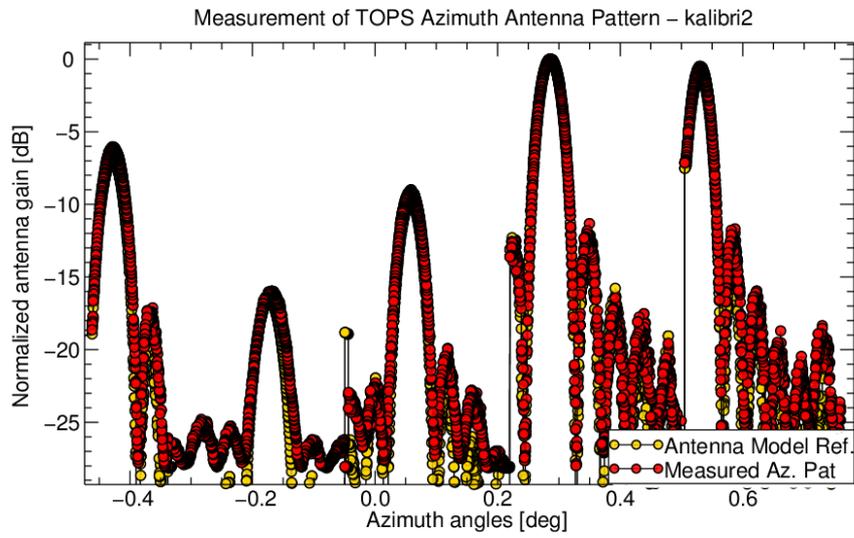


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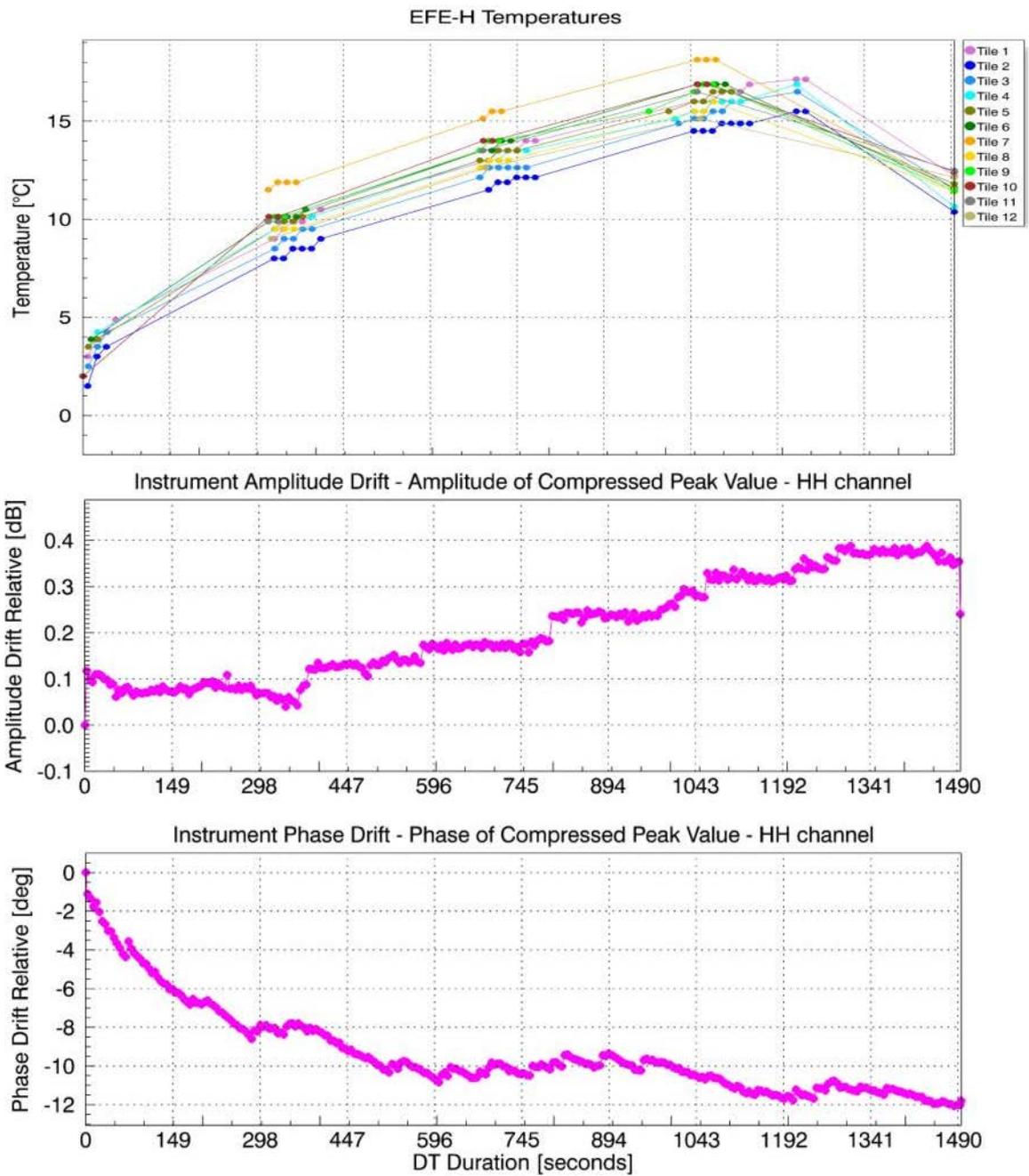
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3 Figure 7 Beam pointing in elevation of TerraSAR-X determined by notch patterns measured
 4 across the rainforest (gamma profile). The measurements depicted were performed at different
 5 days.



1

2 Figure 8 Comparison between antenna model and transponder measurements of an azimuth
 3 pattern of the extrawide swath mode realized by TOPS operation of Sentinel-1A [11].



1

2 Figure 9 Front-end temperature drift (upper plot), instrument drift in amplitude (middle plot)
 3 and instrument drift in phase (lower plot) of the co-polar channel (HH) for a 25 minutes long
 4 Stripmap data take of Sentinel-1A acquired on the 06.08.2014 [10].

5

1 Table 1 Specification of the ‘Kalibri’ transponders in C-band

Center Frequency	5.405 GHz
Bandwidth	100 MHz
RCS	60 dBm ²
Radiometric Stability	≤ 0.1 dB (1σ)
Abs. Radiometric Accuracy	0.2 dB (1σ)
Polarization	Adjustable backscatter matrix

2

3 Table 2 Specification of the remote-controlled corner reflectors

Leg Length	2.8 m
RCS (X-,C-,L-Band)	54.3, 49.2, 36.6 dBm ²
Mechanical Tolerance	≤ 1.0 mm
Abs. Radiometric Accuracy	0.2 dB (1σ)
Pointing Accuracy	< 0.1 deg

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5

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2 Table 3 Accuracy of the DLR SAR Calibration Techniques

TRM Characterization

Amplitude / Phase < 0.2 dB / < 2 deg

Geometric Calibration

Azimuth / Range ~10 cm / ~10 cm

Pointing Determination

Azimuth / Elevation < 2 mdeg / < 2 mdeg

Antenna Model Verification

Gain < ± 0.2 dB

Radiometric Calibration

Accuracy < 0.3 dB

Stability < 0.2 dB

3

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