

CMC Rocket Thrust Chamber Technology Status and Perspectives

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Technologies for Future Liquid Propulsion



Outline

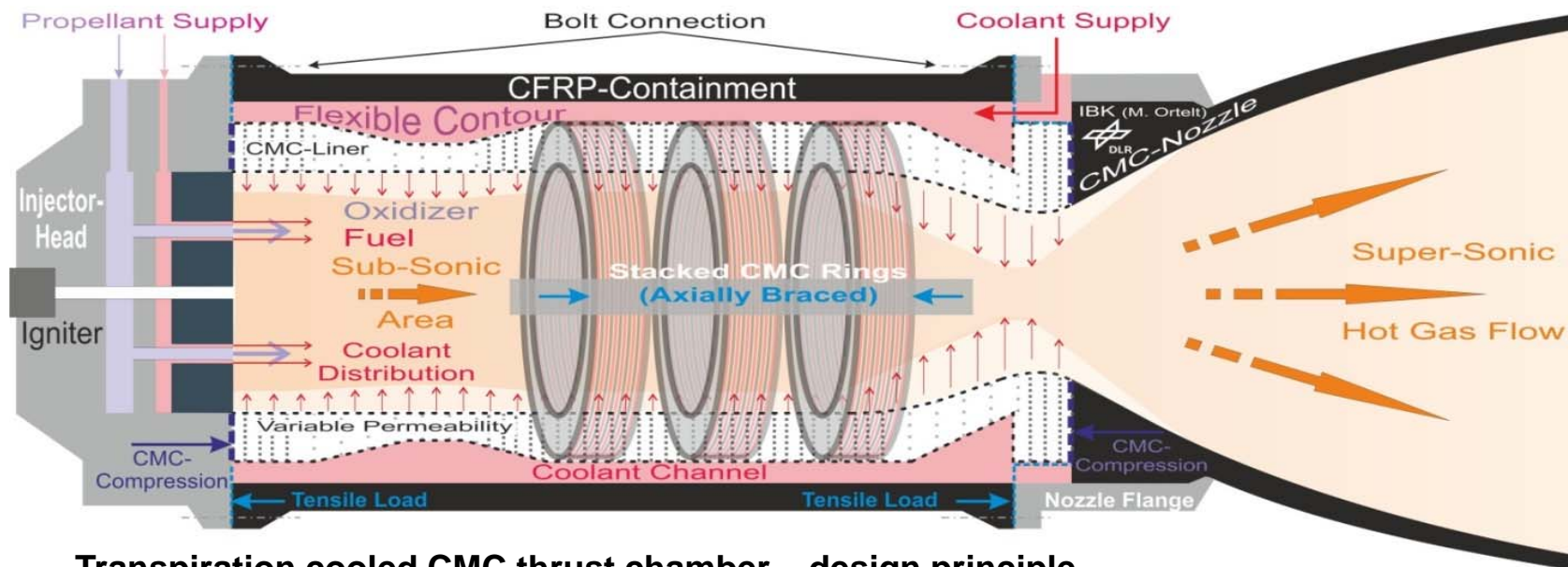
- Conceptual aspects of the transpiration cooled CMC TCA
- Development status
 - Structural components
 - Materials
 - Test data
- Some future perspectives for CMC in space propulsion components
- Summary & outlook



CMC thrust chamber – Design concept

Features

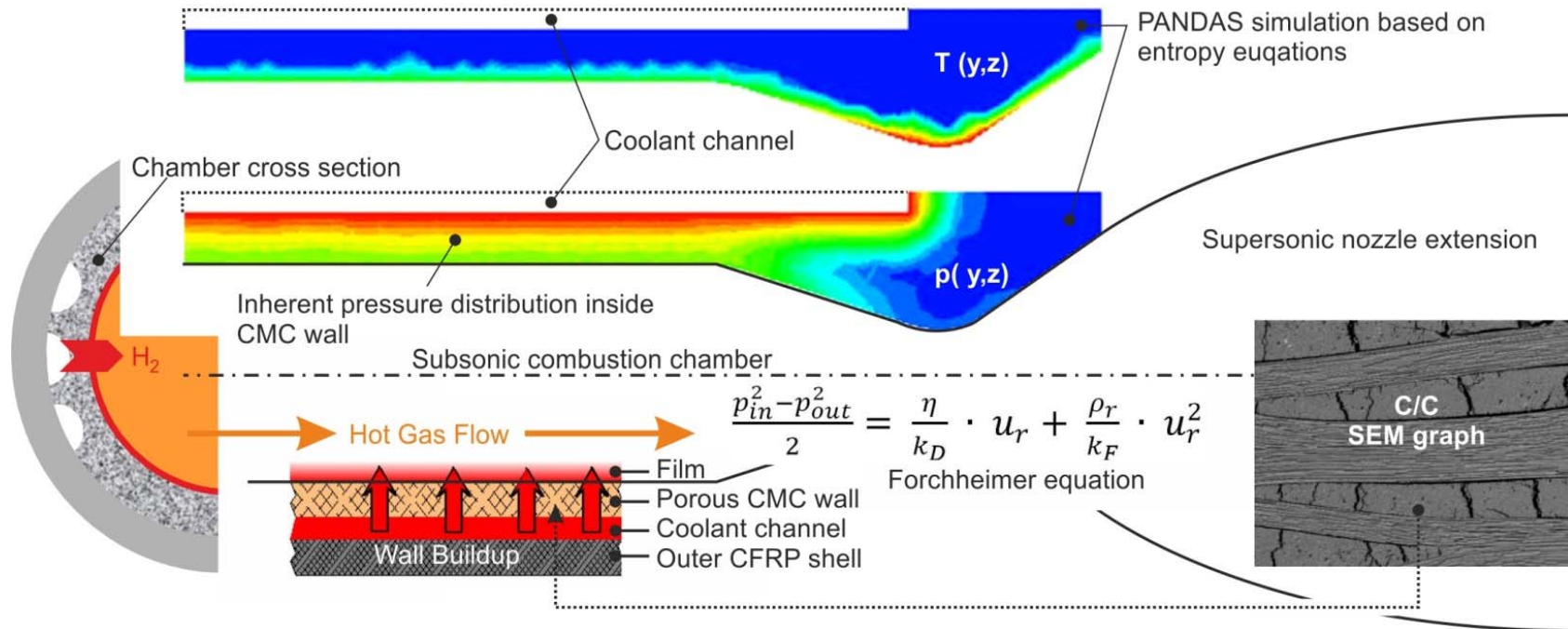
- Decoupling of single components – no bonding
- Decoupling of mechanical and thermal loads
- Specific hybrid interface technologies
- Selective inner liner design



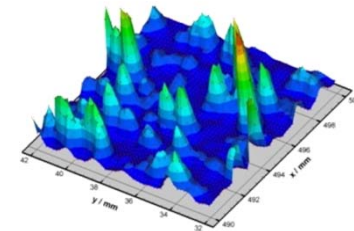
Transpiration cooled CMC thrust chamber – design principle



Functional aspects



- Standard CFD systems (FLUENT, CFX, ...) are constructive (pure flow coupling)
- Ongoing tool-development for 'structure-flow-coupling' (TAU)
- Investigations on materials out-flow homogeneity →

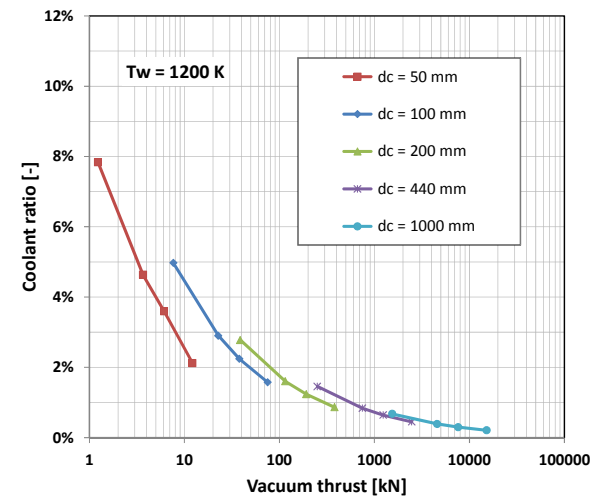
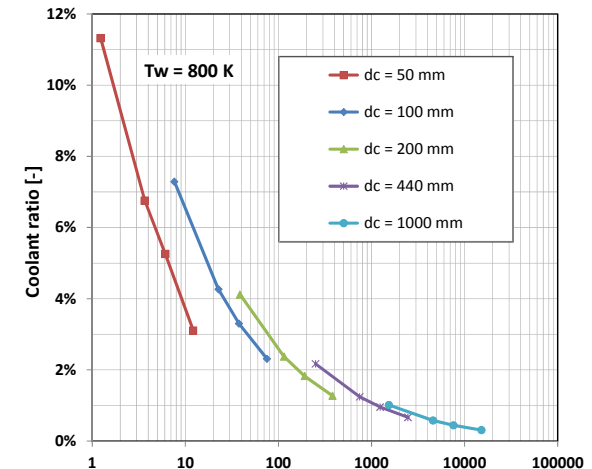


System analysis of transpiration cooling

- Comparison of chamber size (scaling)
- 50 mm chamber demonstration

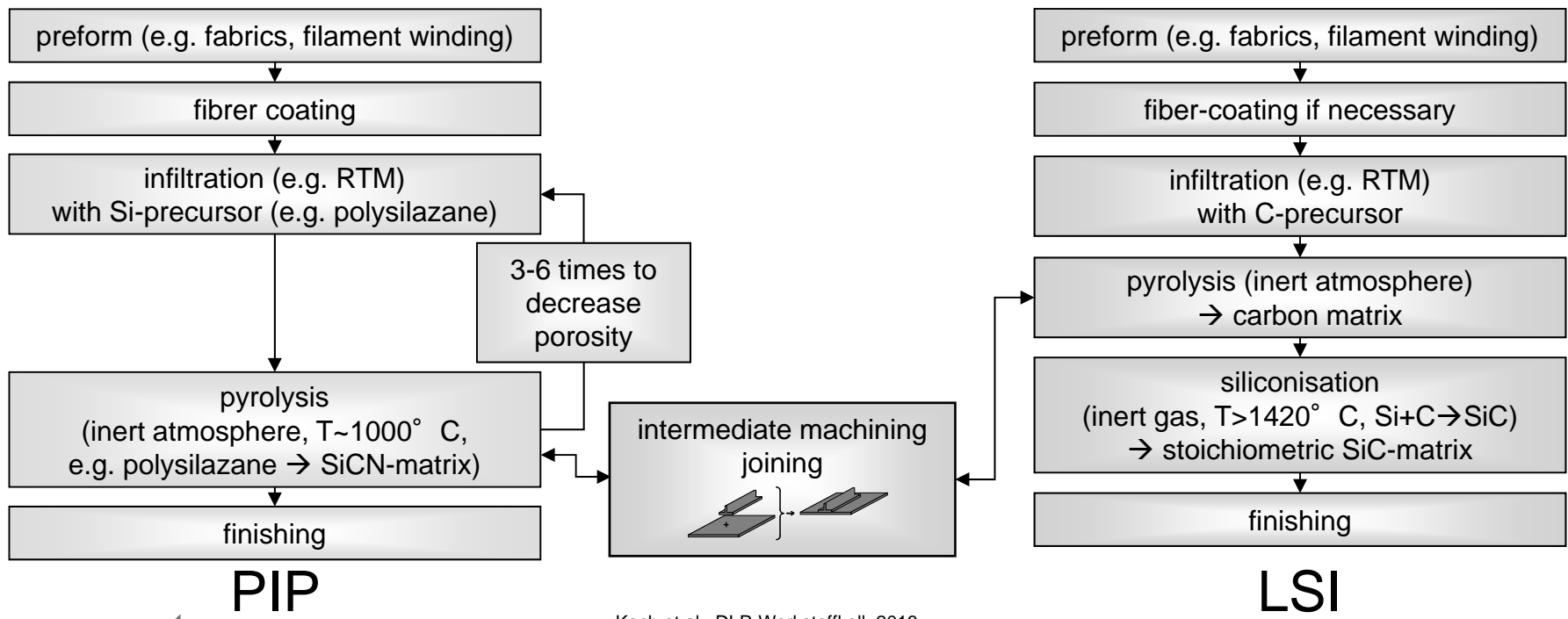
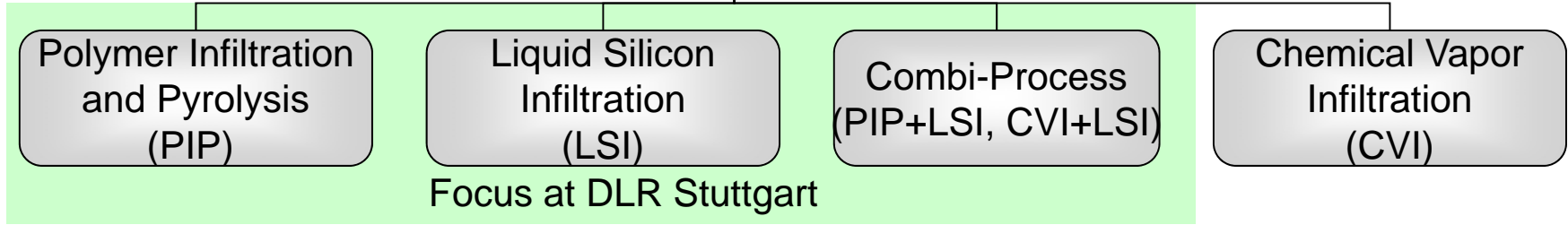
- O/F = 5.5 (injector)
- Contraction ratio 6.25
- Characteristic chamber length $l^*=1.84$ m
- 7 % coolant ratio
- Damage free operation
- Amount of coolant depends on
 - Hotgas conditions, A_s , T
 - $D \nearrow + p \nearrow \rightarrow$ required coolant ratio \searrow
- Further coolant ratio reduction potential
- Chamber length can be shortened

→ High operational efficiency predicted



Processes for Manufacturing of Nonoxide CMC

C, SiC fibers in C, SiC, SiC(N) matrix



Processing of Ceramic Matrix Composites (DLR-ST, BT)



- Autoclave
30 bar, 350° C
- Warm Press 350° C
- RTM 300° C
- Pyrolysis, LSI, 2000° C
- Machining Center



Thrust chamber – potential CMC derivatives

Initial C/C model material LOX-sensitive!

Other derivatives damage free after efficiently cooled and non-cooled operation:



Oxipol

AvA-Z-ISC

C/SiCN

C/C (CVI)

Open porosity ε [%] (porosity + permeability k_d / k_f adaptable by manufacturing process)

10

35

18

7

Density kg/cm³

2.3

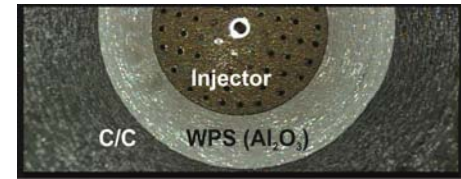
2.6

1.6

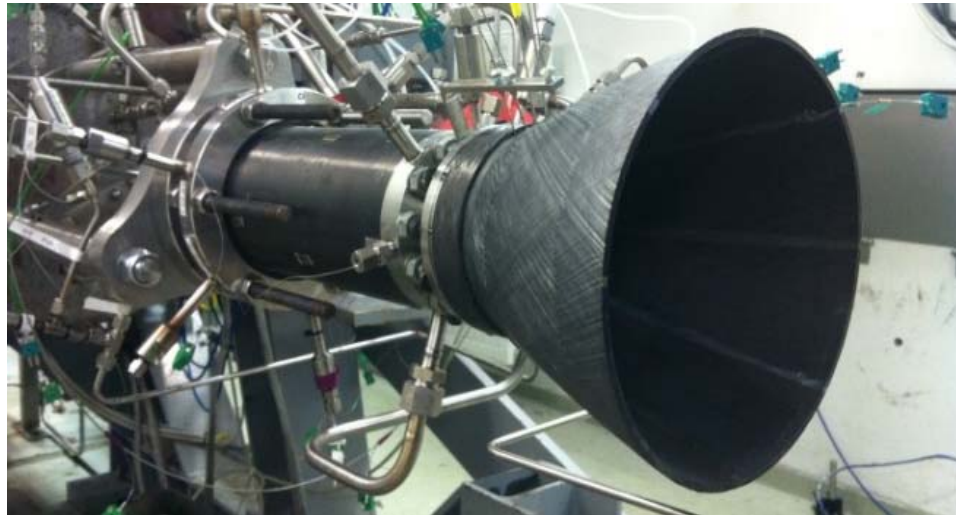
1.6



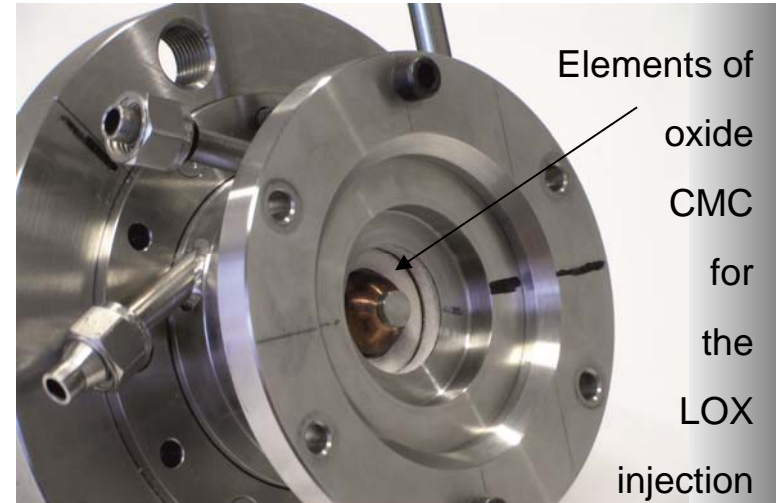
CMC thrust chamber – Components



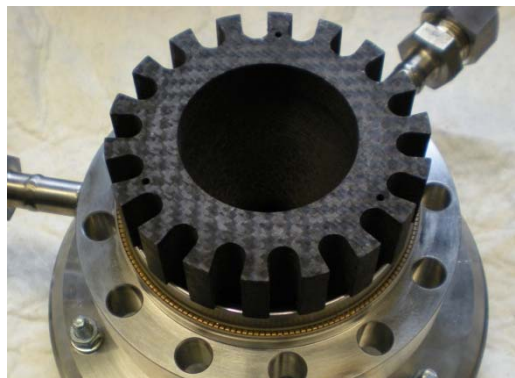
Porous metal injector



Integrated 'BlackEngine' demonstrator, $\varnothing_{\text{cyl.}}$ 50 mm

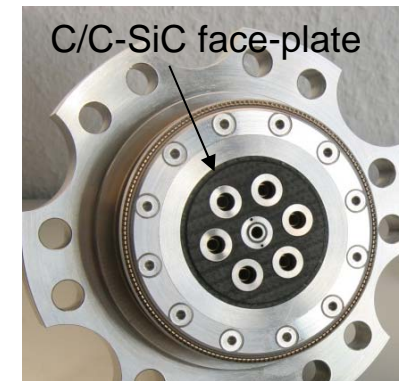


Porous CMC injector



Inner liner segment

Applied injector systems for $\varnothing_{\text{cyl.}}$ 50 mm

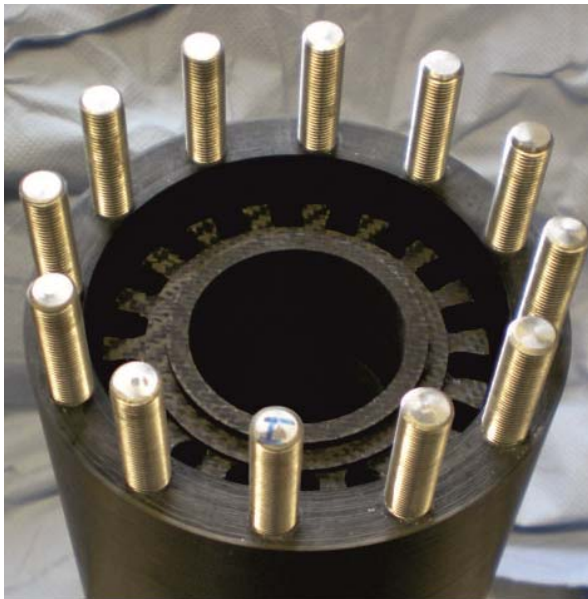


Co-axial injector



CMC thrust chamber – mechanical interfaces

Characteristic hybrid interface types



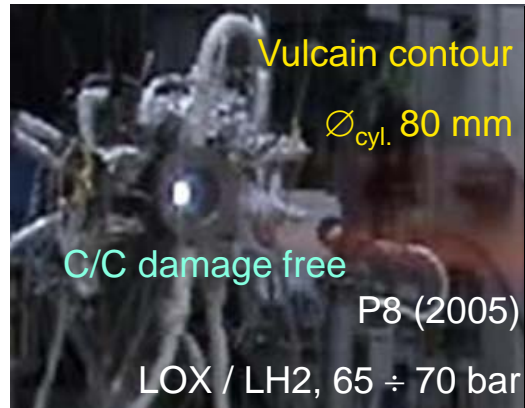
Bolt interface for CFRP-metal joining



Load-de-coupling double-shell nozzle extension with keyed joint elements for CMC-metal joining



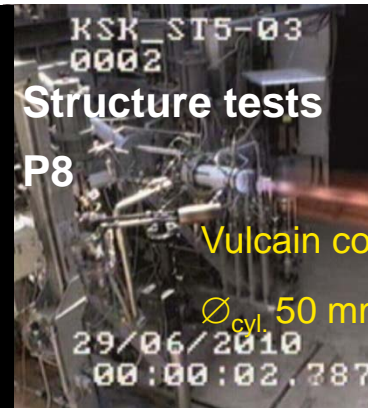
Thrust chamber - hot gas verification (LOX/LH2; LOX/GH2)



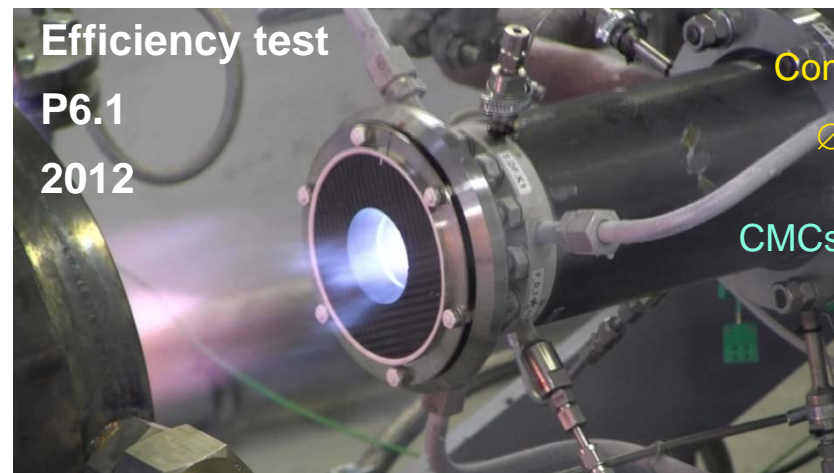
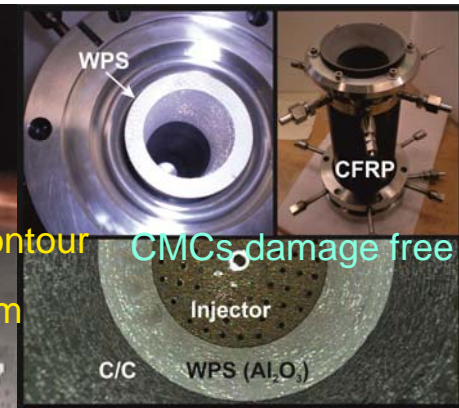
52 s, 5 ÷ 6 kg/s, $\tau = 4.2 \%$



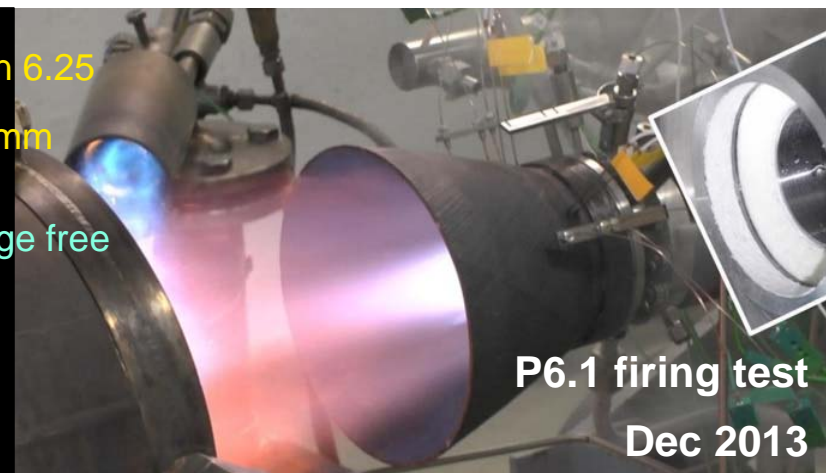
90 bar tests



120 s, $p_c = 55$ bar, LOX / LH2 operation, $\tau = 15 \%$



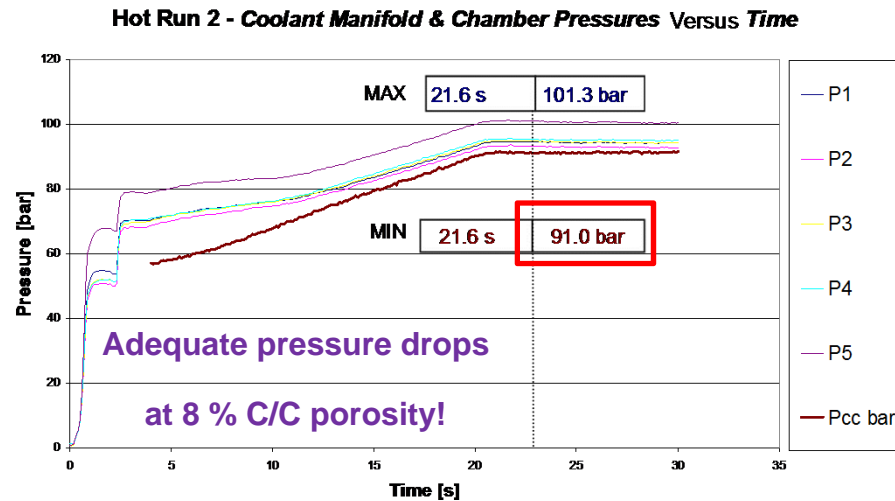
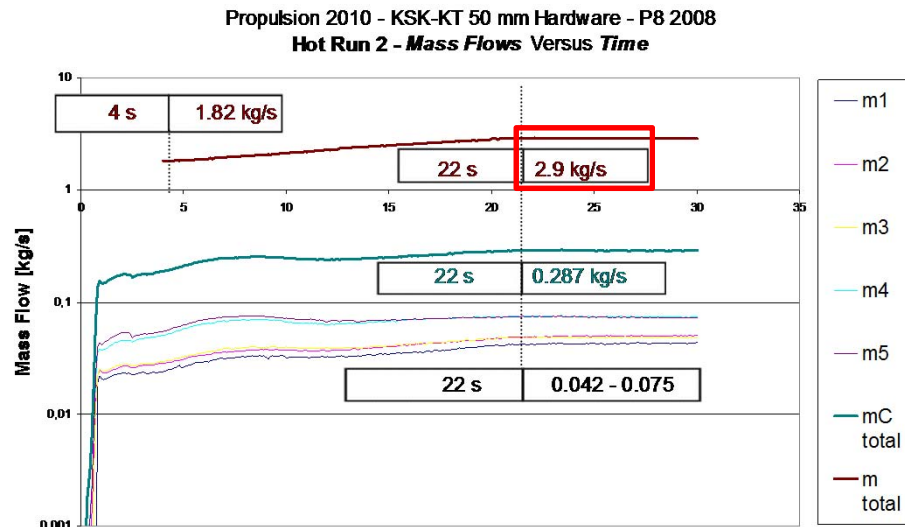
20 s, $p_c = 55$ bar, LOX / GH2 (120 K), $\tau = 9 \%$



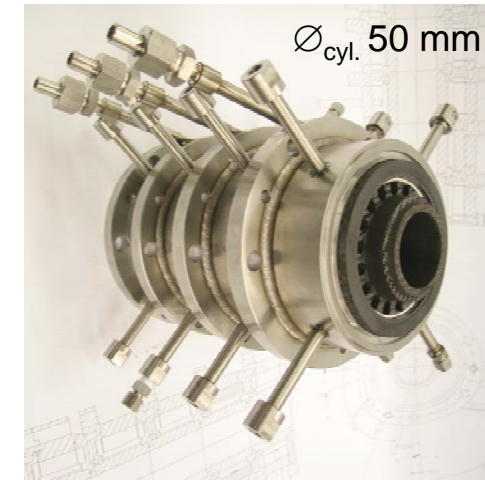
Demonstration of the integrated CMC TCA



Thrust chamber – pressure loads during hot-run

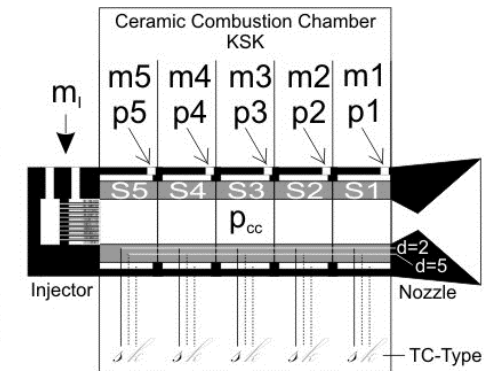
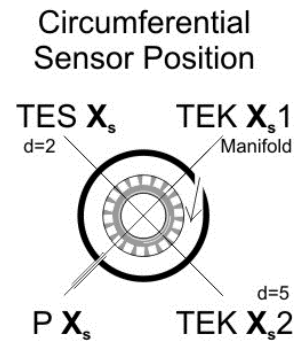


Segmented chamber module



Inner liner:
Initial model
material
C/C

O/F = 5.5

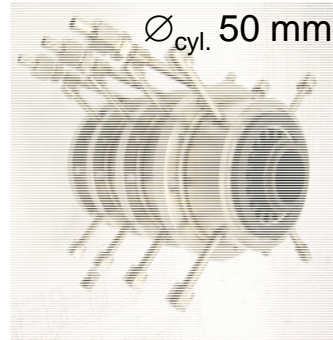


Thrust chamber – thermal loads during hot-run

P6.1, 2012

Nominal hotrun-sequence

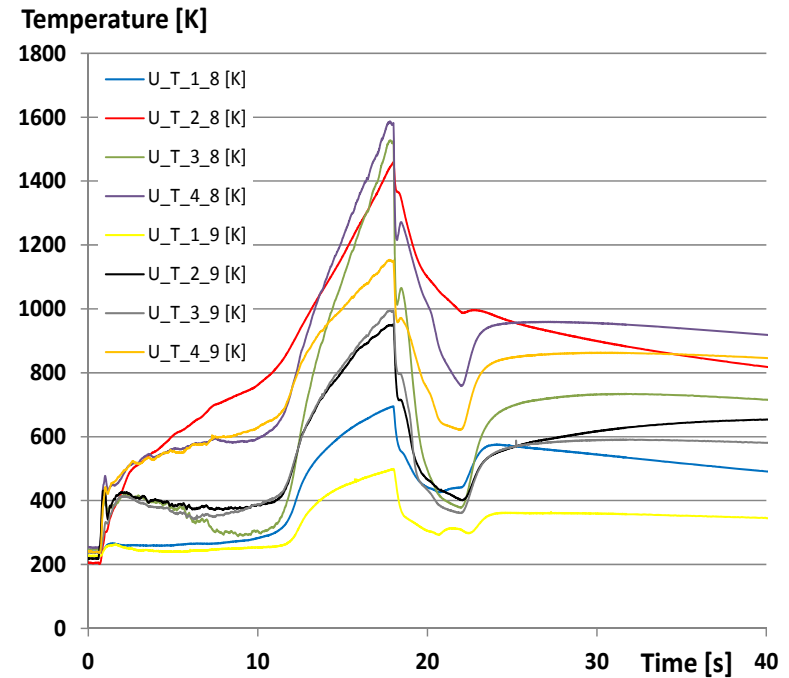
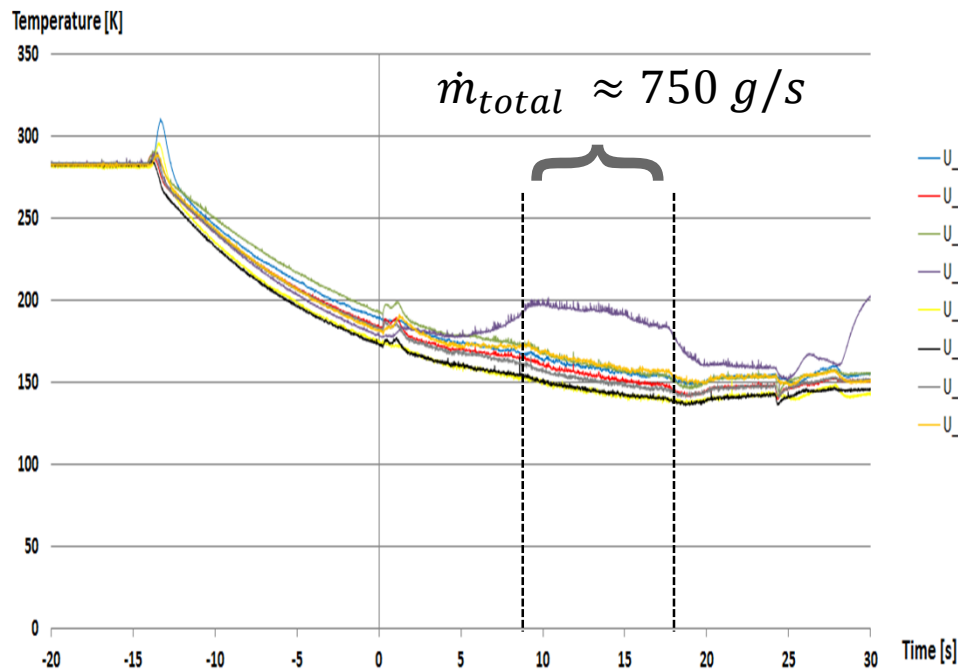
O/F = 5.5; $\tau = 6.72\%$; $p_c \approx 55$ bar



Cooling turned off

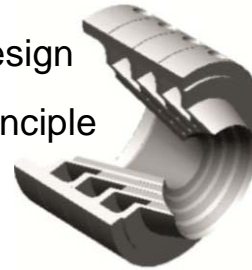
O/F = 2.0

Max. $T_{surface} \cong 1800$ K



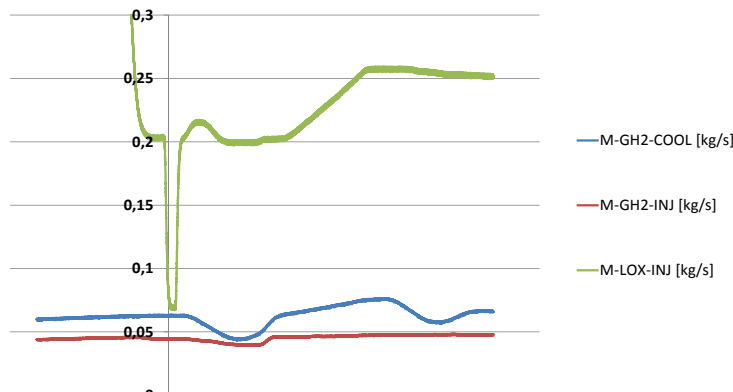
CMC injector („Cone Injector“)

Design principle

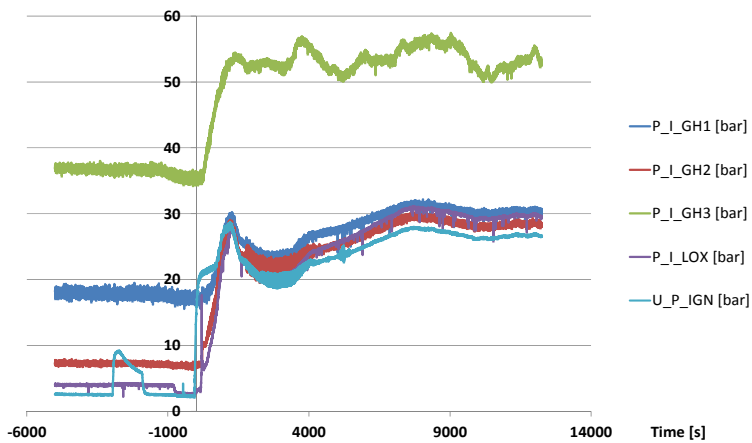


Features, goals, results

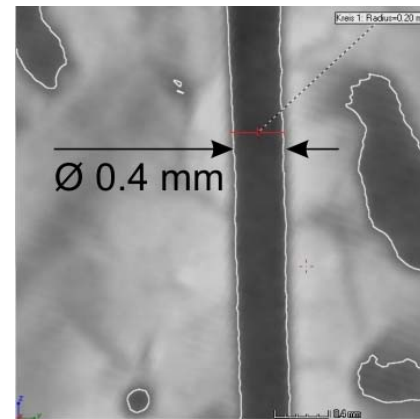
DLR - Cone Injector test campaign 'IZ2' - MASS FLOW CURVES



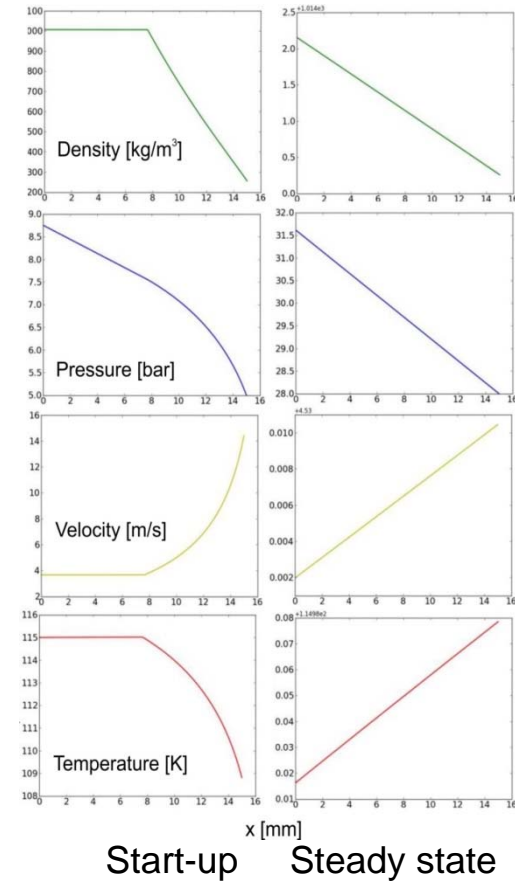
DLR - Cone injector test campaign 'IZ2' - PRESSURE CURVES



Demonstrator



Channel morphology



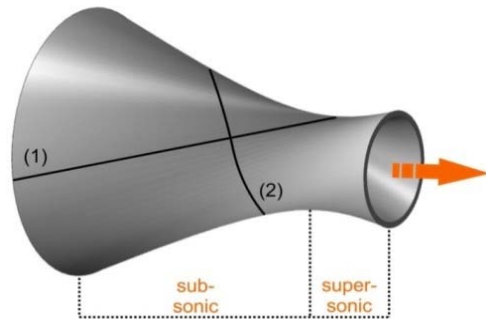
Flow design

Initially successful hotruns, P6.1, Dec 2013

Mechanical design

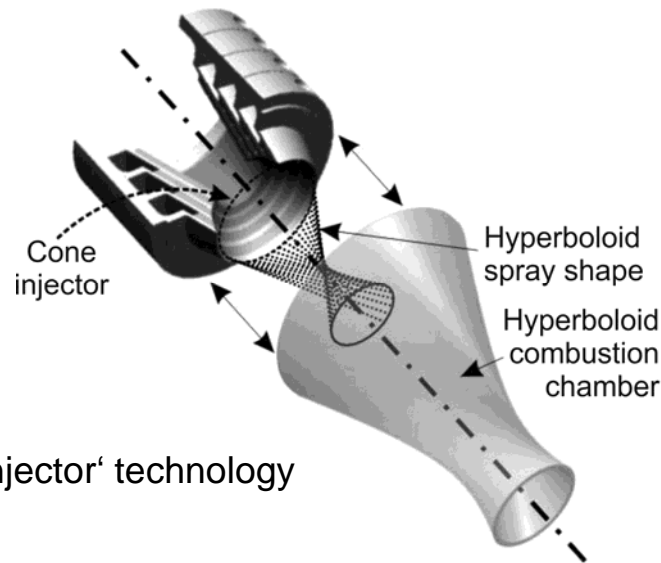


Hyperboloid chamber contour – Orbital propulsion size



Hyperboloid chamber design

Perfectly combined with 'cone injector' technology

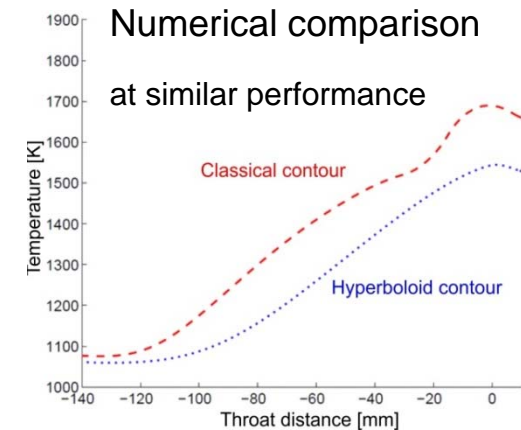


Hyperboloid geometry

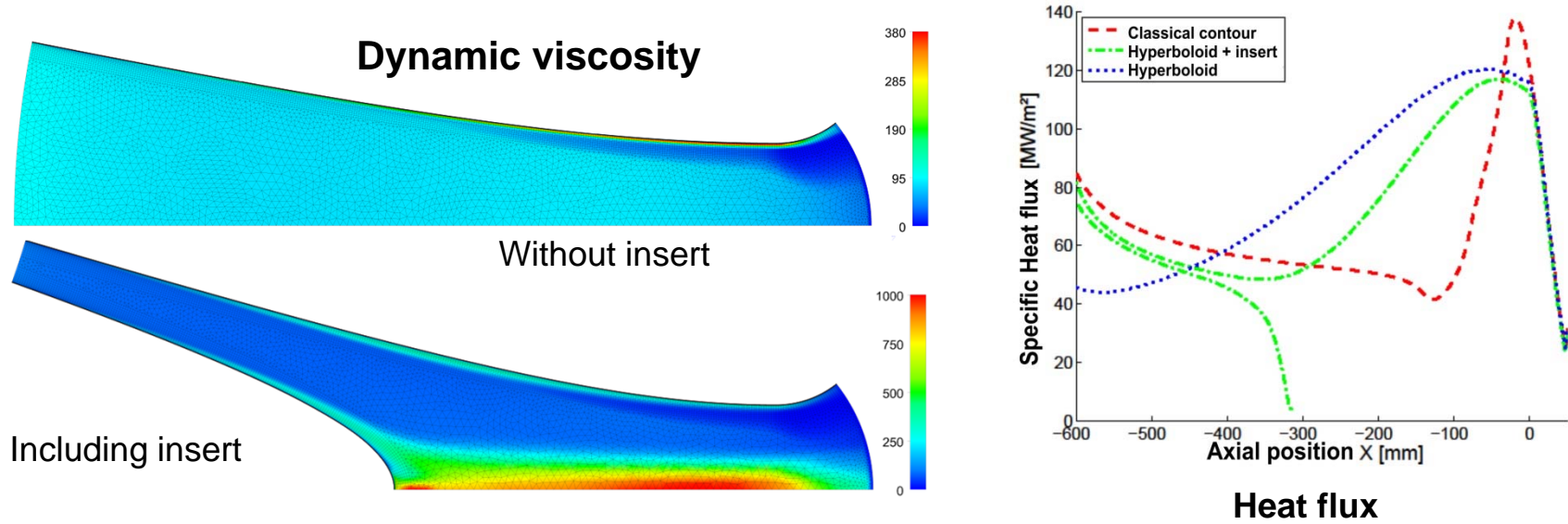
$$\frac{x^2}{a^2} + \frac{y^2}{b^2} - \frac{z^2}{c^2} = 1$$

Comparison referred to typical 500 N class

- Advantages for
 - film cooling
 - transpiration cooling
- Composite affine structure manufacturing (winding technique)



Hyperboloid chamber contour – Comparison VINCI size



Contour	Mass flow [kg/s]	Total heat flux [MW]	Specific heat flux [MW/m ²]
Classical	43	16	55
Hyperboloid without insert	42	16	56
Hyperboloid including insert	43	27	52

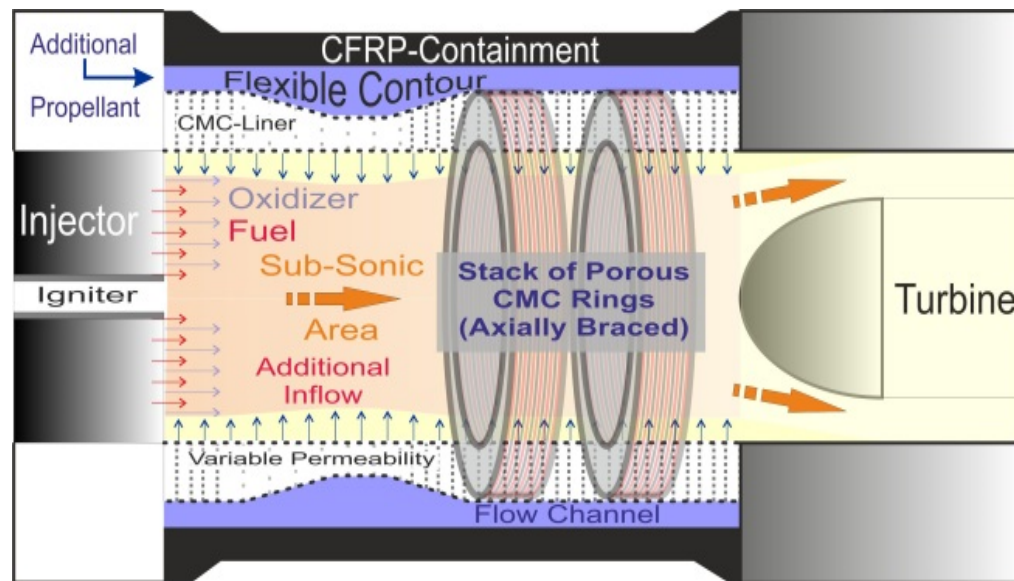
Performance



Future potential - Preburner

Features

- Standard injector technology concerning ...
 - functional design
 - mixture ratio
- Propellant overhead injected through chamber wall
- Long life and light weight structures, similar to CMC thrust chamber design



Application principle
(oxide CMCs for ox-rich systems)



Further activities

- ALM / SLM technology for injector systems
- CMC components for hybrid propulsion systems
- Paraffin / N₂O: Hybrid thruster
- CMC thrust chamber for an ADN orbital propulsion system
- Investigations on alternative propellants for CMC high performance thrust chamber application
 - LOX / LCH₄
 - LOX / kerosene



Summary

- The transpiration cooled CMC thrust chamber principle could be demonstrated successfully
 - a simplified and de-coupled design principle has been proven
 - no critical material degradation under efficient operation, considering scaling aspects
 - mechanically safe structures
- First firing tests of the ceramic ‚cone injector‘ concept successful and promising
- Adequate hybrid mechanical interfaces demonstrated
- New hyperboloid thrust chamber contour numerically validated

Outlook

- CMC application potential for ADN thruster (orbital propulsion)
- CMCs principally interesting for hybrid propulsion systems
- Preburner application (in particular ox-rich)
- Up-coming SLM technology
- Alternative propellants



Thank you for your attention!

