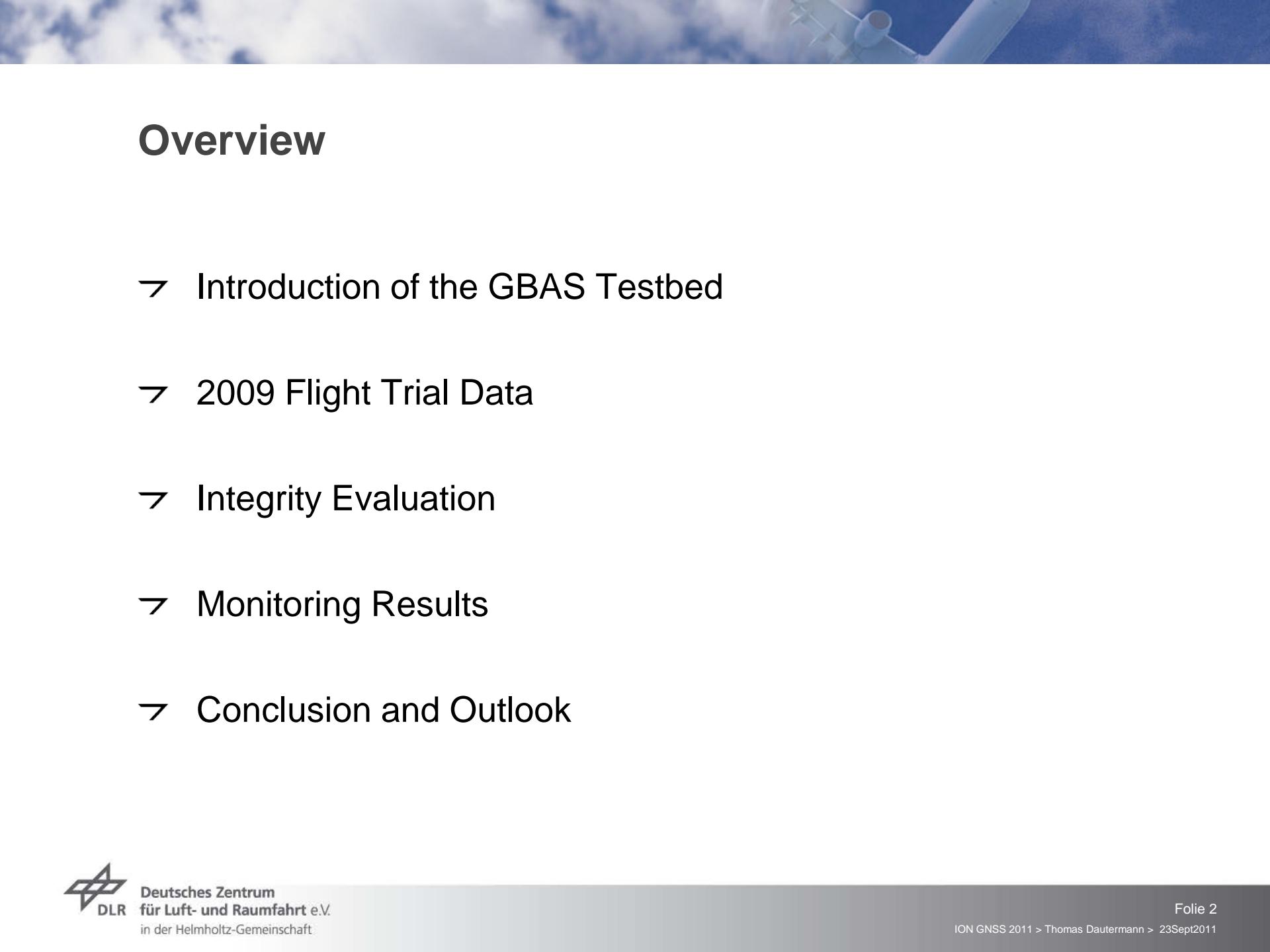


# **GAST-D Monitoring Results from Post-processed Flight Trial Data: A Performance Evaluation of DLR's GBAS Testbed**

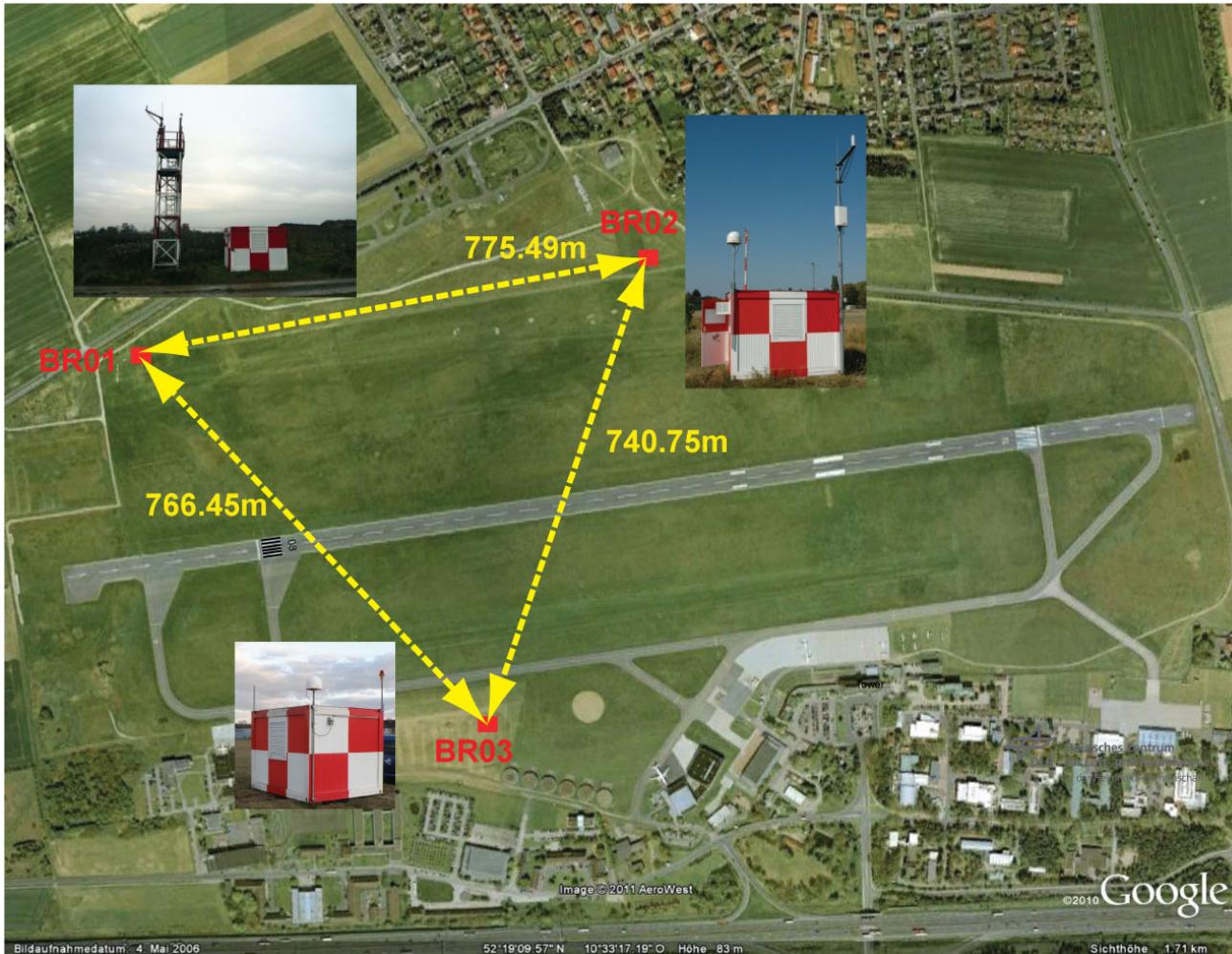
**Thomas Dautermann, Michael Felux, Anja Grosch, Boubeker Belabbas**



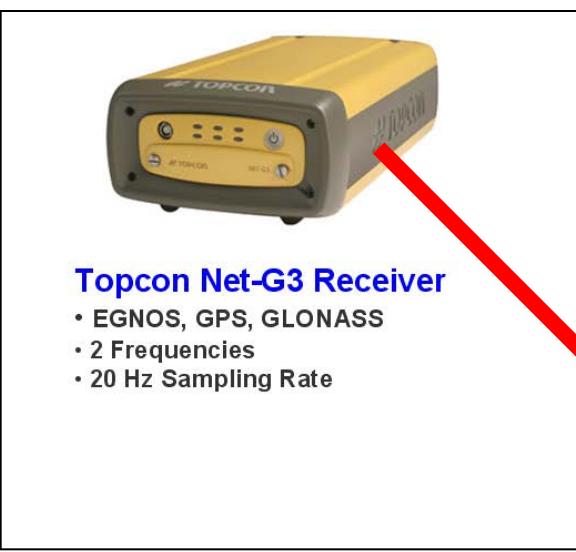
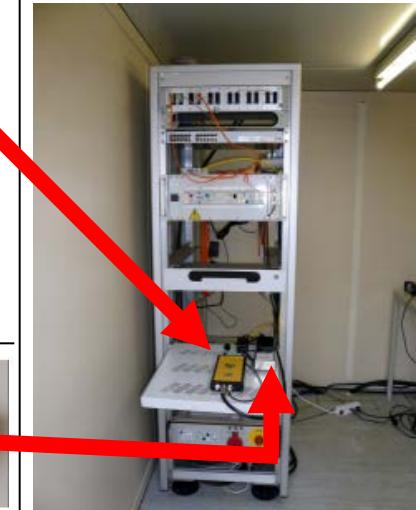
# Overview

- ↗ Introduction of the GBAS Testbed
- ↗ 2009 Flight Trial Data
- ↗ Integrity Evaluation
- ↗ Monitoring Results
- ↗ Conclusion and Outlook

# The DLR GBAS Testbed



# Ground Subsystem Hardware

<p>Outside Container</p> 	 <p><b>LEICA AR 25</b></p>  <p><b>Topcon Net-G3 Receiver</b></p> <ul style="list-style-type: none"><li>• EGNOS, GPS, GLONASS</li><li>• 2 Frequencies</li><li>• 20 Hz Sampling Rate</li></ul>	<p>Inside Container</p> 
	<p><b>External Clock</b> TEMEX Low Cost &amp; Profile Frequency Rubidium Standard (LPFRS) Improves short time stability</p> 	

# Airborne Subsystem Hardware



## Topcon Net-G3 Receiver

- EGNOS, GPS, GLONASS
- 2 frequencies
- 20 Hz data sampling
- local data recording

Real time data transfer to ground processing facility via TCP/IP

## VFW 614 ATTAS

### “Advanced Technologies Testing Aircraft System”

Approach Speed 90knots (44 m/s)

Flight Technical Error Autopilot  $\sigma < 50 \text{ m}$



# Airborne Subsystem Hardware

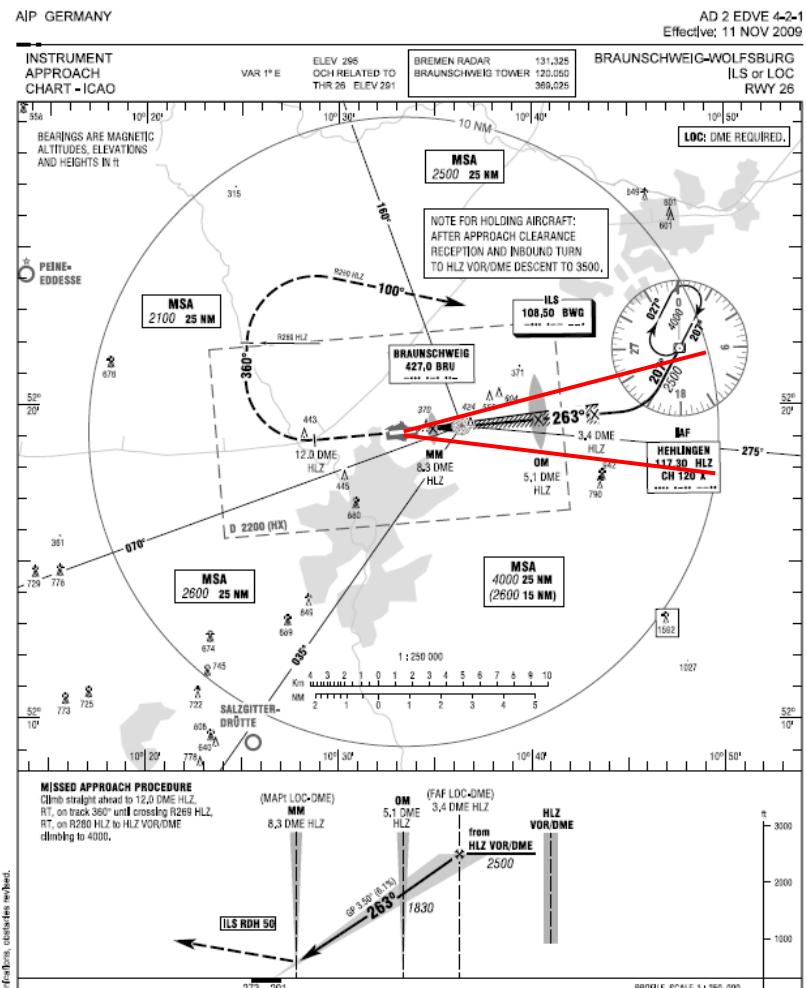


flugzeugbilder.de // Copyright by Kais Chabani (www.eddk-spotters.de,vu) // 10-September-2004 // U2R // 1095009615

# Flight Trial Statistics and Setup

- ↗ Guidance through ILS
  - ↗ GBAS Service Area and PAR
  - ↗ Total of 30 approaches
  - ↗ Evaluation based on DO253C

Date	No. approaches
2009/11/16	4
2009/11/26	1
2009/11/27	4
2009/12/07	6
2009/12/11	6
2009/12/14	2
2009/12/16	7



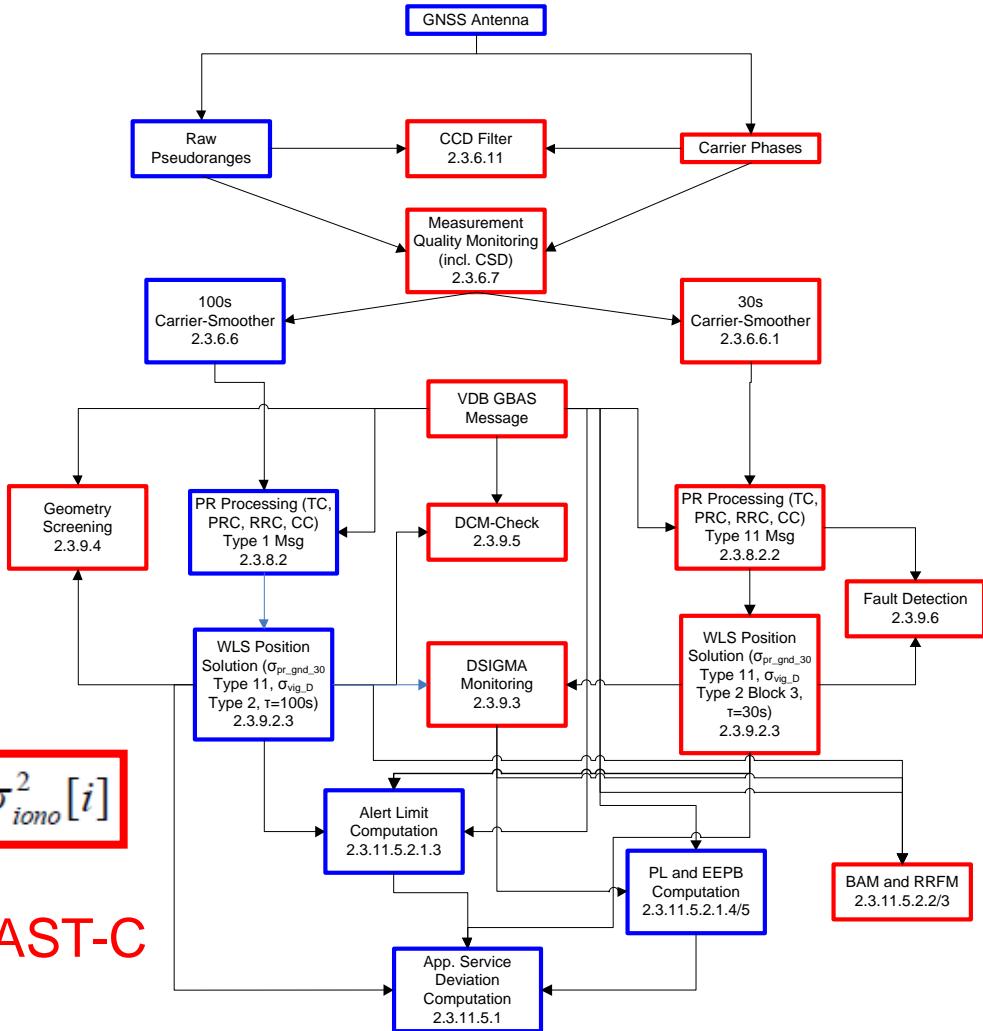
# Airborne Architecture

- ↗ Additional Monitors Implemented
- ↗ Geometry Screening in accordance with ATTAS FTE  $\sigma - S_{\text{vert}} < 4$
- ↗ Nominal Protection Levels GAST-C vs. GAST-D

$$VPL_{Apr\_H0} = K_{ffmd} \sqrt{\sum_{i=1}^N s_{Apr\_vert,i}^2 \sigma_i^2} + D_V$$

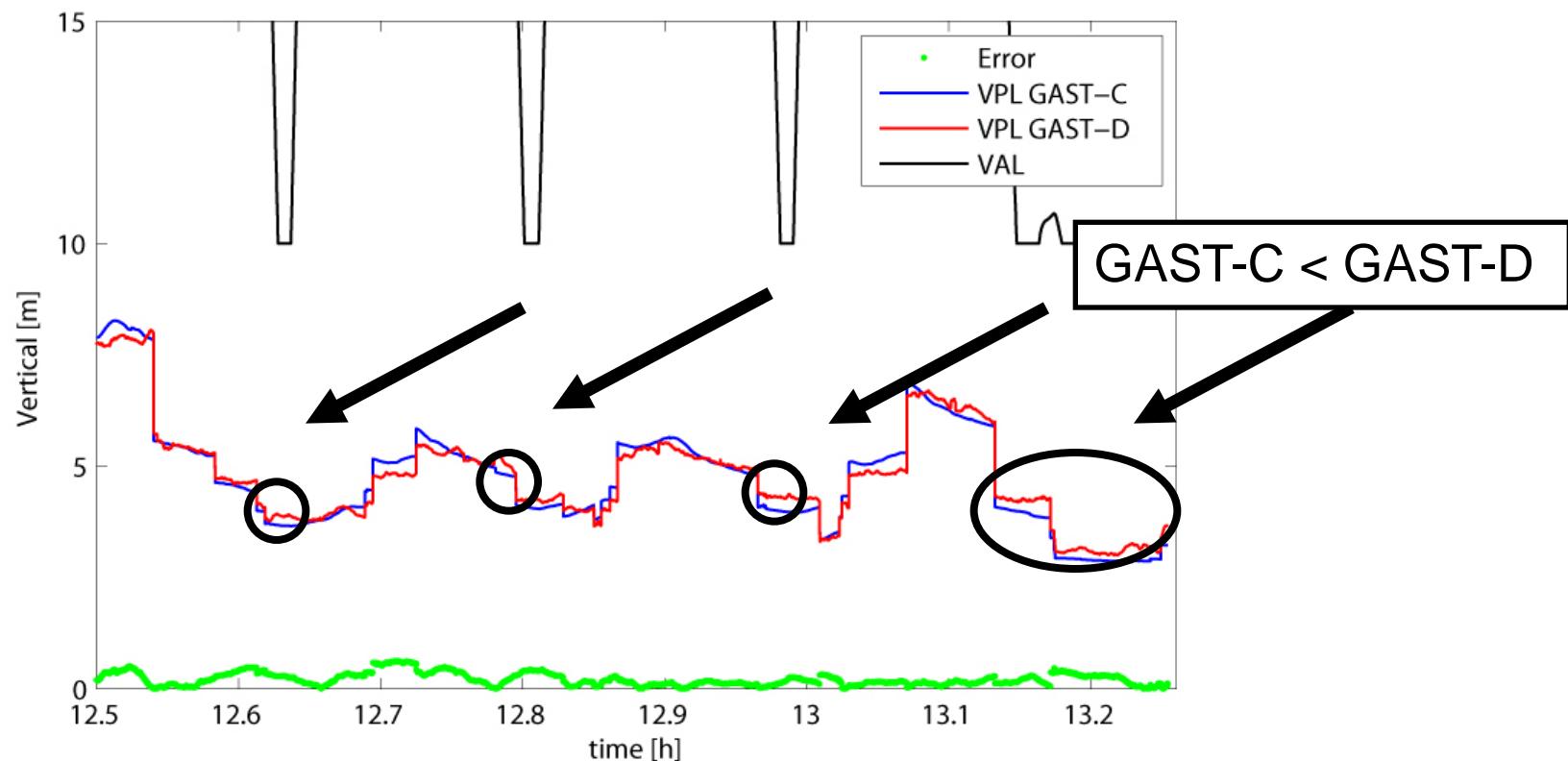
$$\sigma_i^2 = \sigma_{pr\_gnd\_x}^2[i] - \sigma_{tropo}^2[i] + \sigma_{pr\_air}^2[i] - \sigma_{iono}^2[i]$$

GAST-C < GAST-D    GAST-D < GAST-C



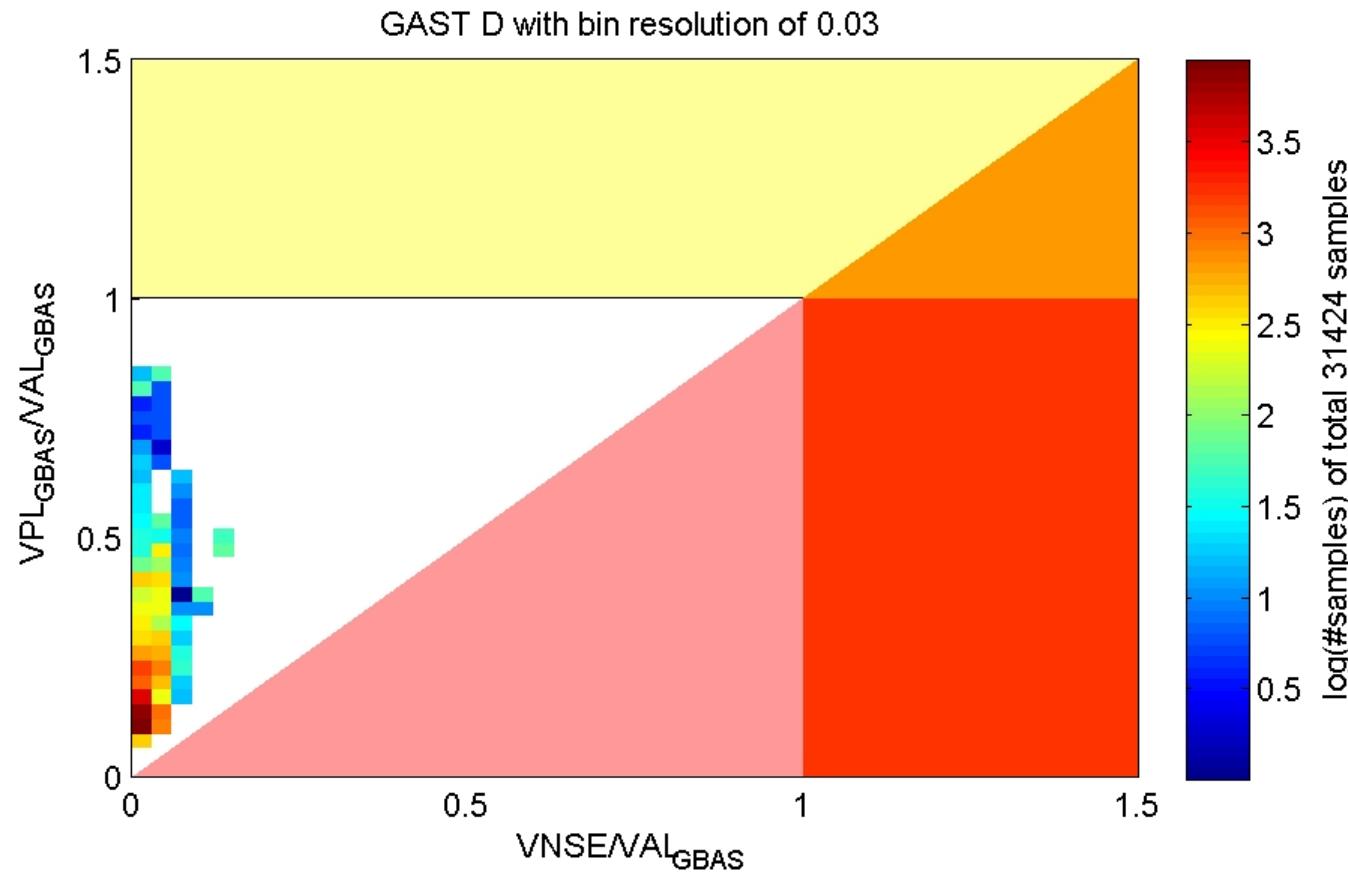
# Protection Level Behavior

- ↗ Levels GAST-C vs. GAST-D
- ↗ Nov. 27 2009



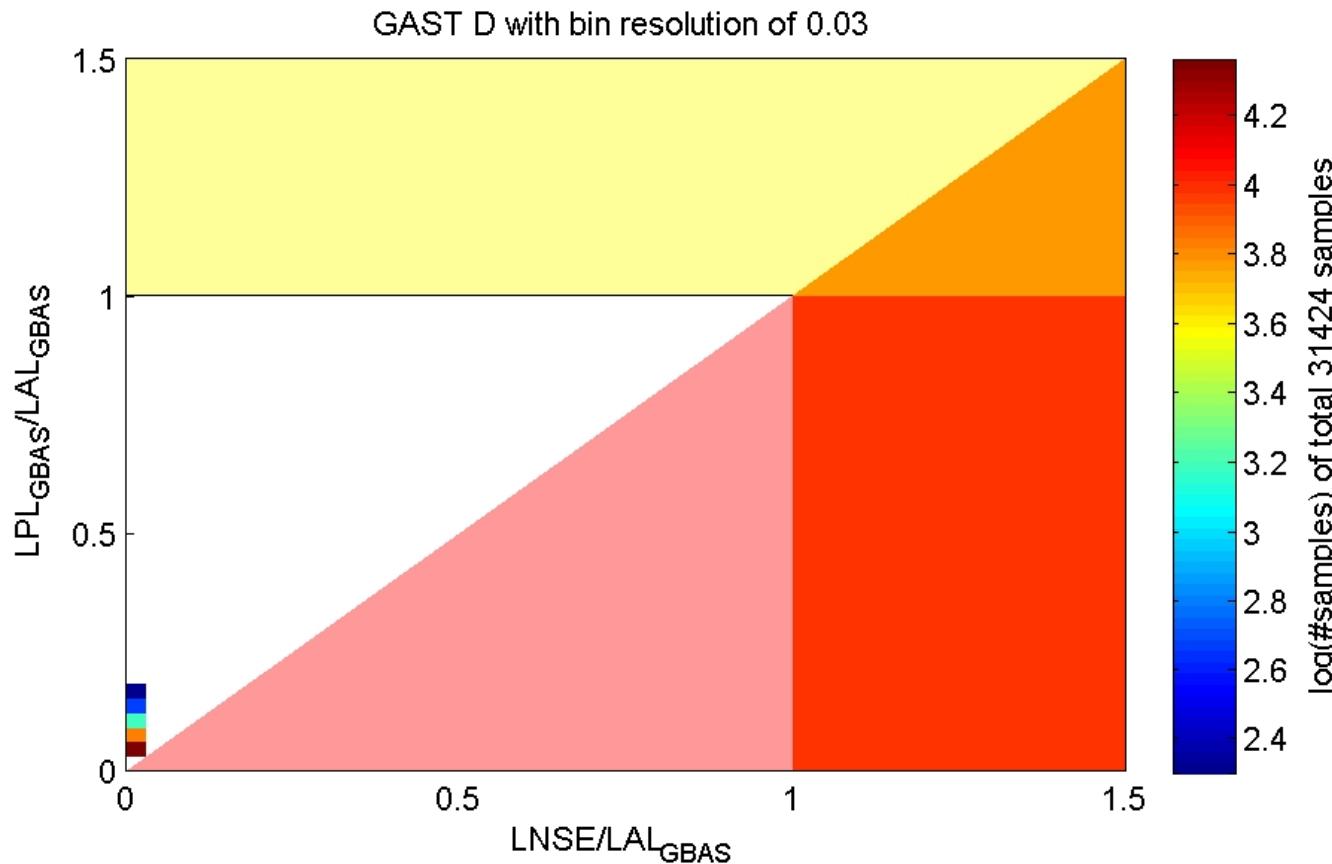
# Integrity Evaluation (Stanford Diagram)

- Service area, all approaches

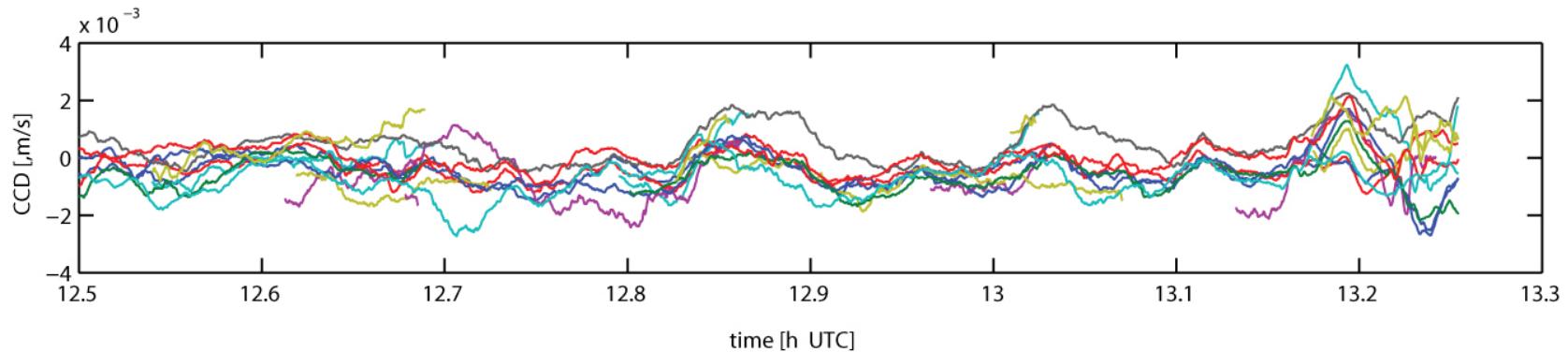


# Integrity Evaluation (Stanford Diagram)

- Service area, all approaches



# Code Carrier Divergence Monitor - Nov. 27 2009



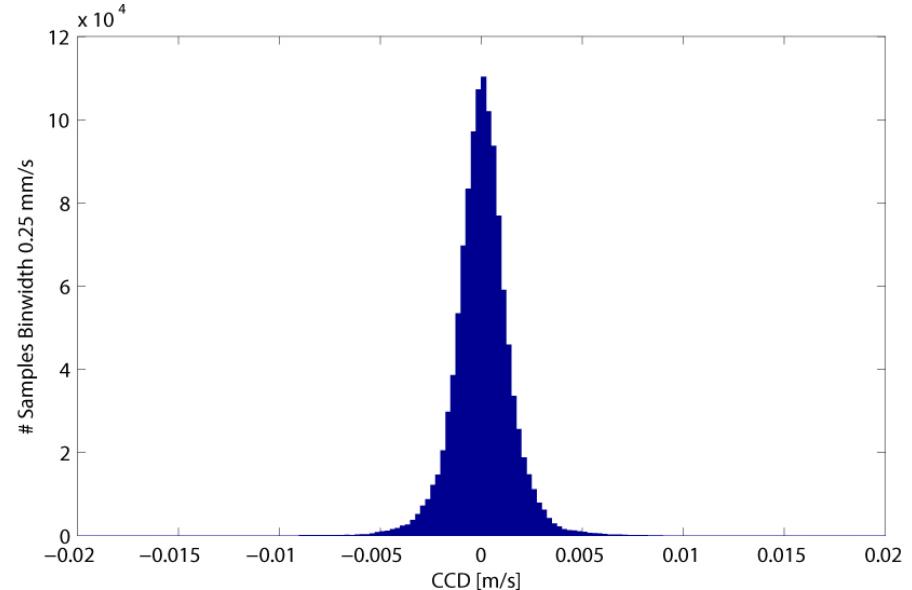
- ↗ Two step filter

$$Z_n = (1-\alpha)Z_{n-1} + \alpha \Delta CMC_n$$

$$D_n = (1-\alpha)D_{n-1} + \alpha Z_n$$

$$\alpha = 0.5 \text{ s}/100 \text{ s} = 1/200$$

- ↗ Threshold 12.5 mm/s
- ↗ Threshold is in mm in DO253C



# Differential Correction Magnitude Check - Nov. 27 09

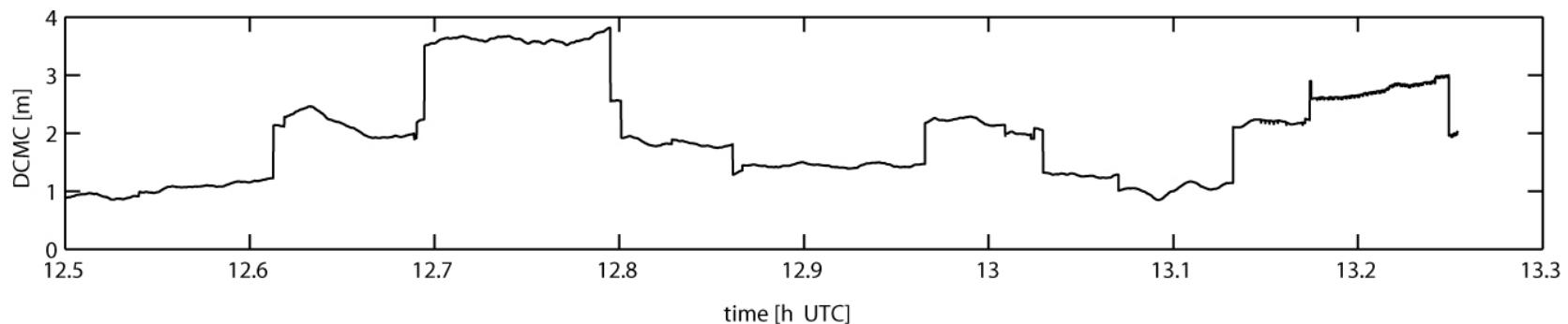
- Differential correction magnitude in position domain

$$\delta PR_i = PRC_i + RRC_i(t - t_{apl}) + TC_i$$

$$\vec{x} = S \delta PR$$

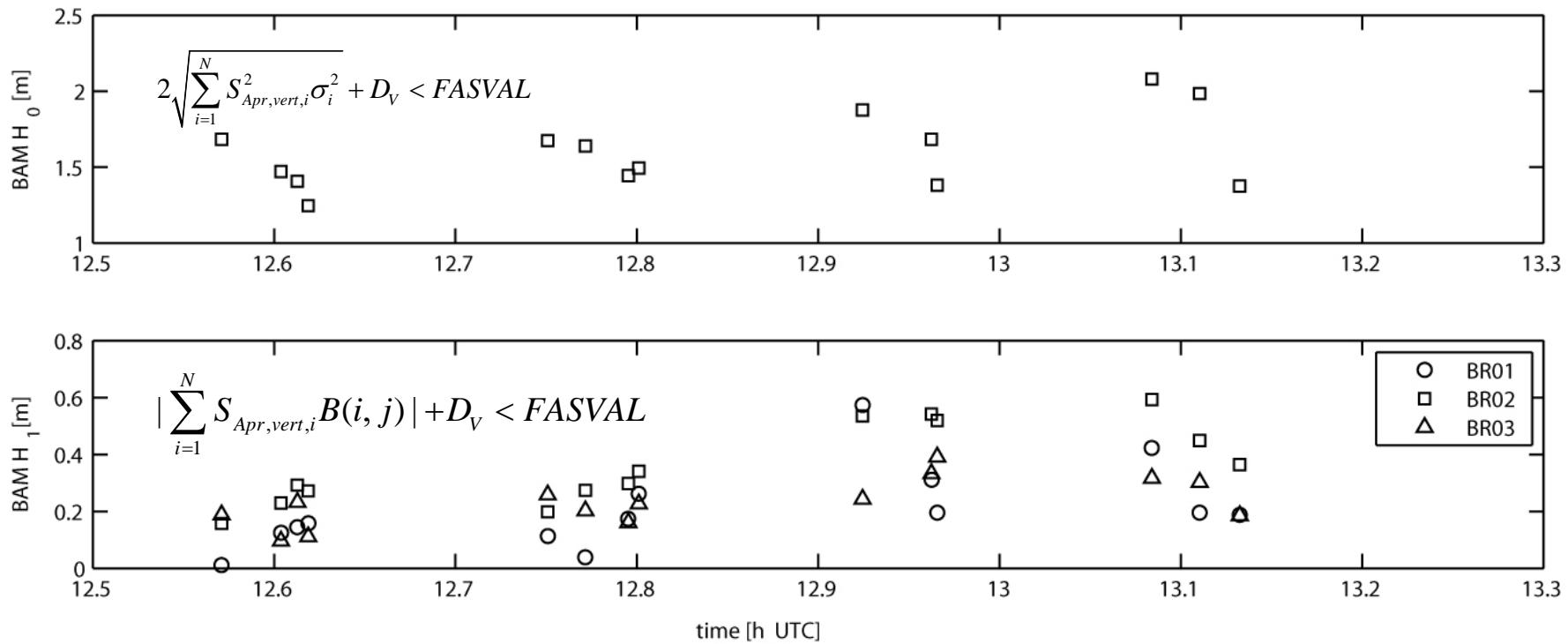
$$DCM_H = \sqrt{x_1^2 + x_2^2}$$

- In DO253C with satellite clock bias
- Threshold 200m



# Bias Approach Monitor

- Compares 66% position uncertainty and B-Values in position domain to FASVAL (10m) when transitioning to PAR or geometry change occurs



# Reference Receiver Fault Monitor - Nov. 27 2009

- ↗ B-values mapped into position domain

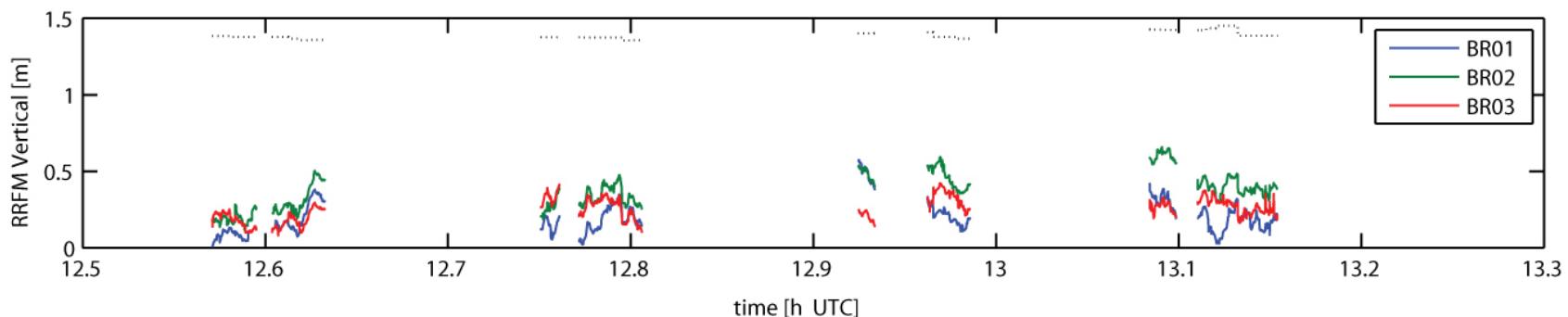
$$\left| \sum_{i=1}^N S_{Apr,vert,i} B(i,j) \right| + D_V < T_{B,air,vert}$$

$$T_{B,air,vert} = K_{ffd,B} \sqrt{\sigma_{B_{vert}}^2 + \sigma_{D_V}^2}$$

$$\left| \sum_{i=1}^N S_{Apr,lat,i} B(i,j) \right| + D_L < T_{B,air,lat}$$

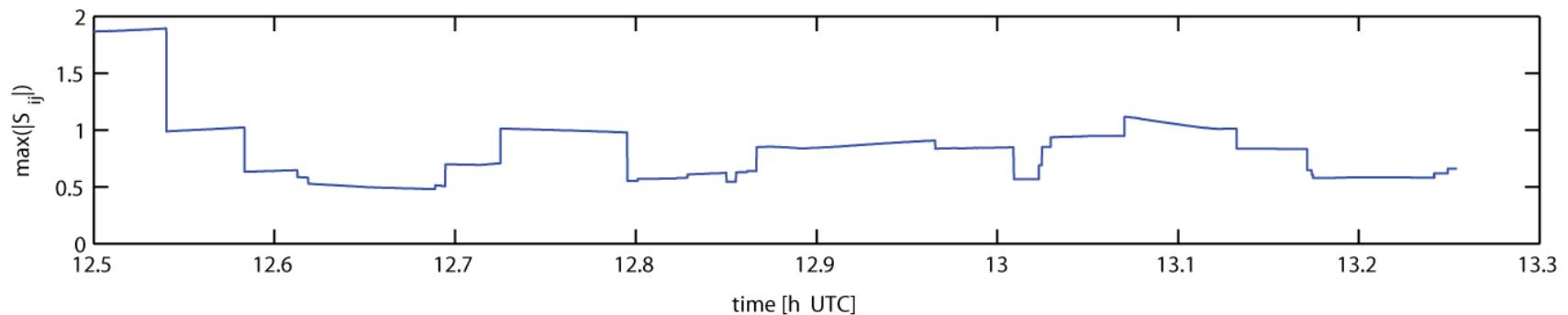
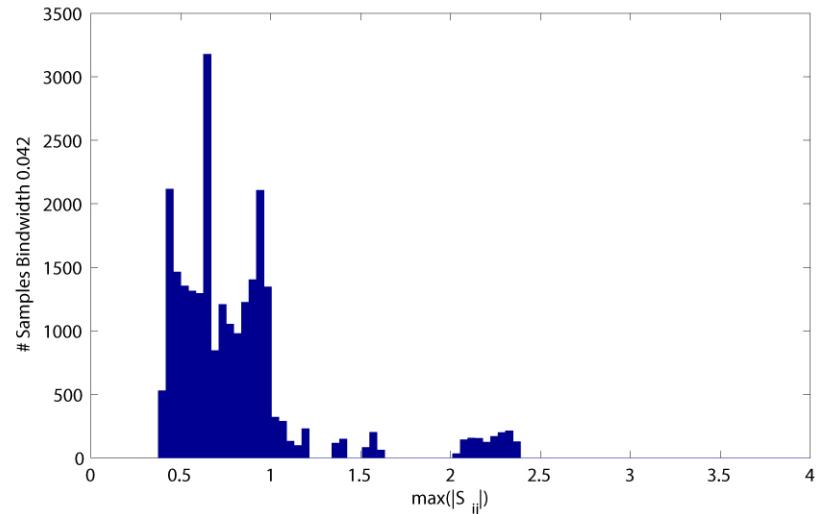
$$T_{B,air,lat} = K_{ffd,B} \sqrt{\sigma_{B_{lat}}^2 + \sigma_{D_L}^2}$$

- ↗  $K_{ffd,B}=5$
- ↗ Only while inside PAR



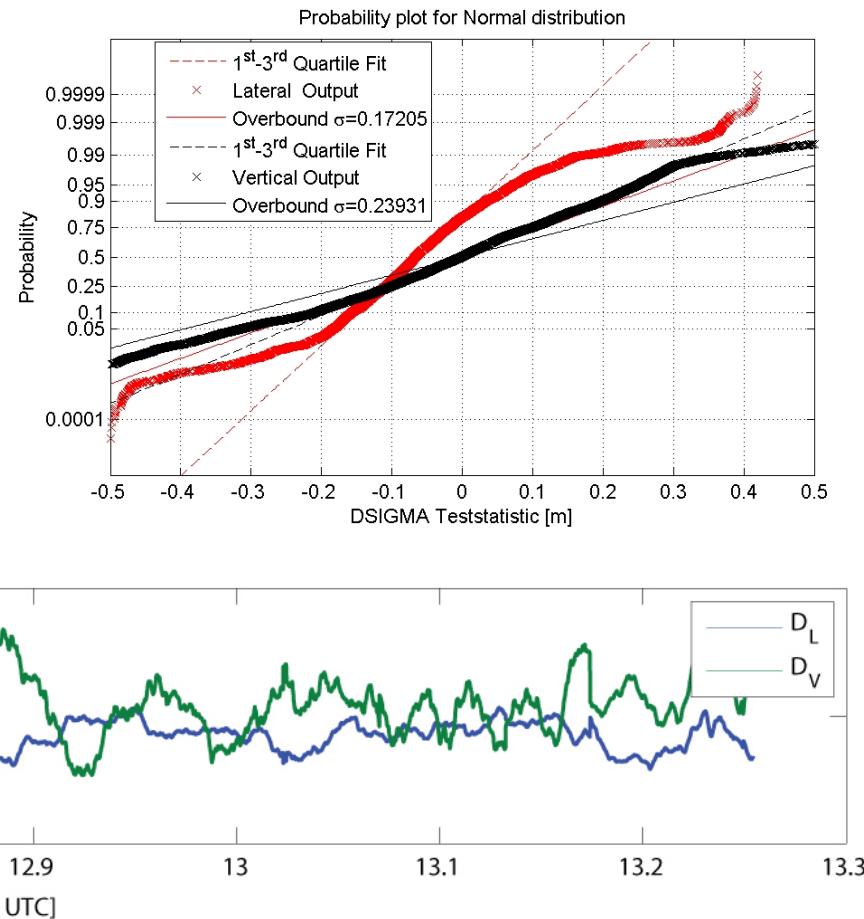
# Maximum Element of Pseudoinverse

- ↗ Geometry needs to be screened to avoid positioning with maximum undetectable range error of 1.5m
- ↗ Here, limited to 4 but could be increased according to FTE
- ↗ Maximum  $S_{ij}$  observed during all flight trials was 2.43

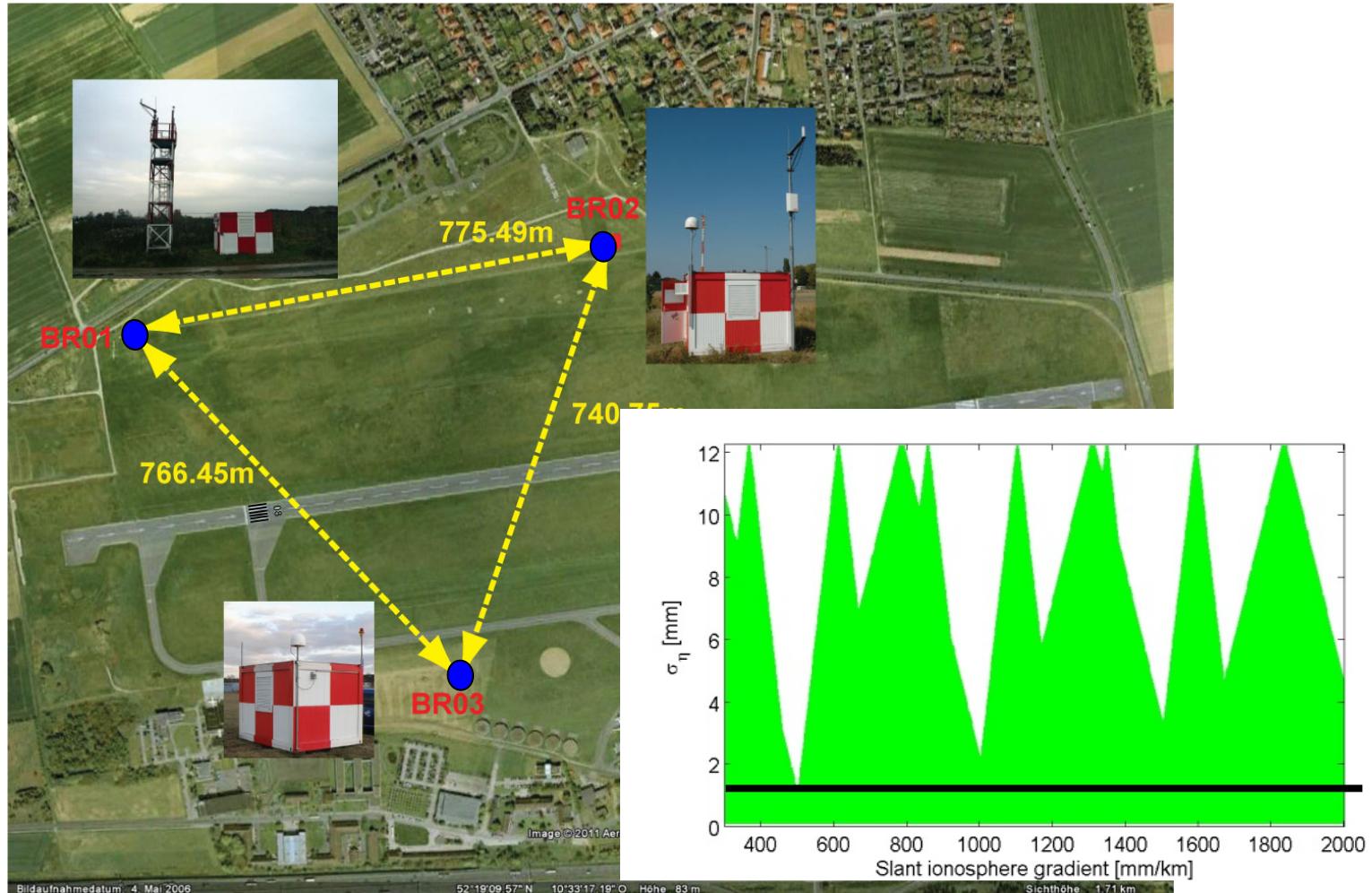


# DSIGMA Monitor Statistics ( $D_V$ -Vertical)

- Difference between 30s and 100s smoothed position
- Murph and Harris (2006):  $\sigma=0.22\text{m}$
- Additional Ionosphere monitor required -> Double Difference Phase

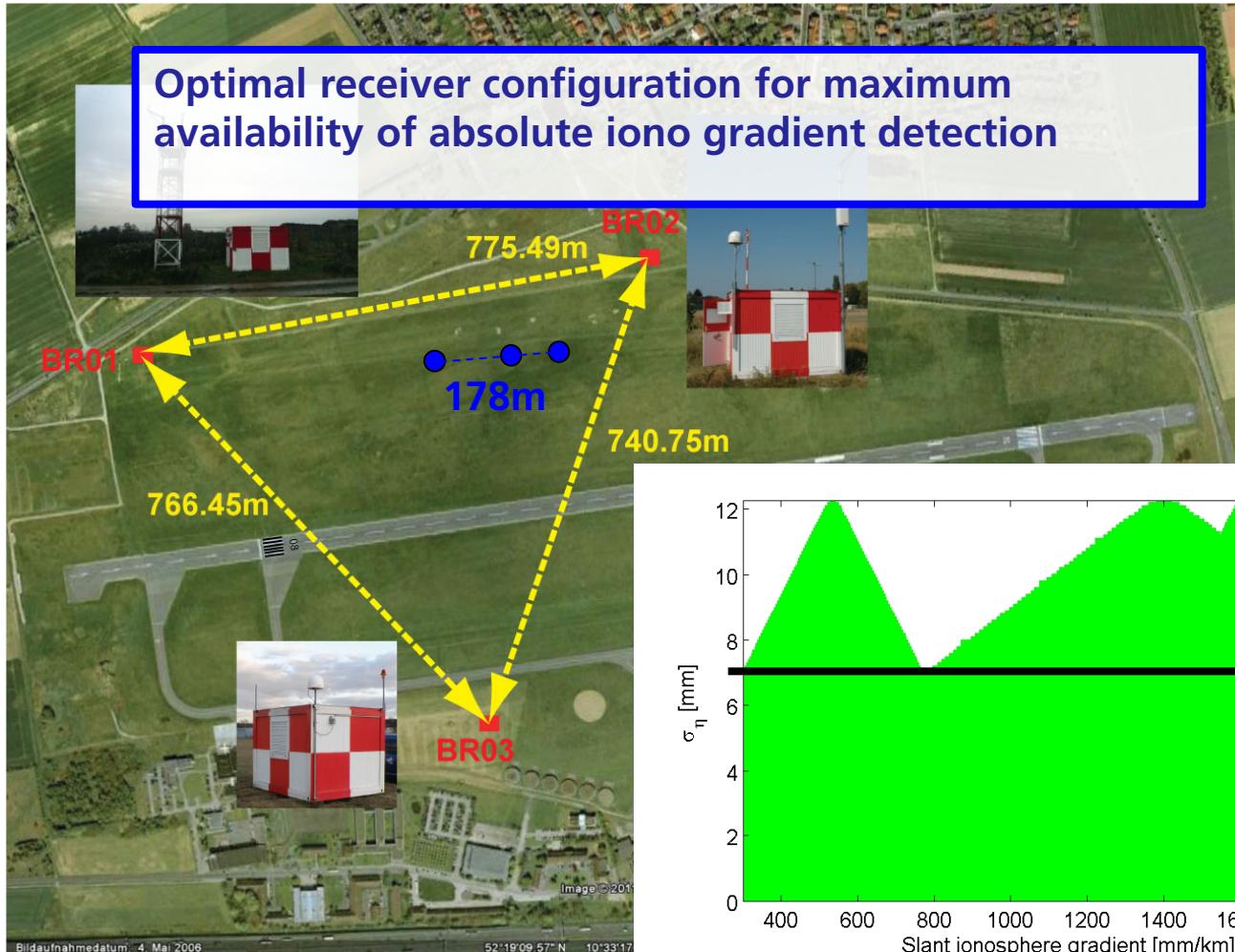


# Optimal absolute iono gradient monitoring network

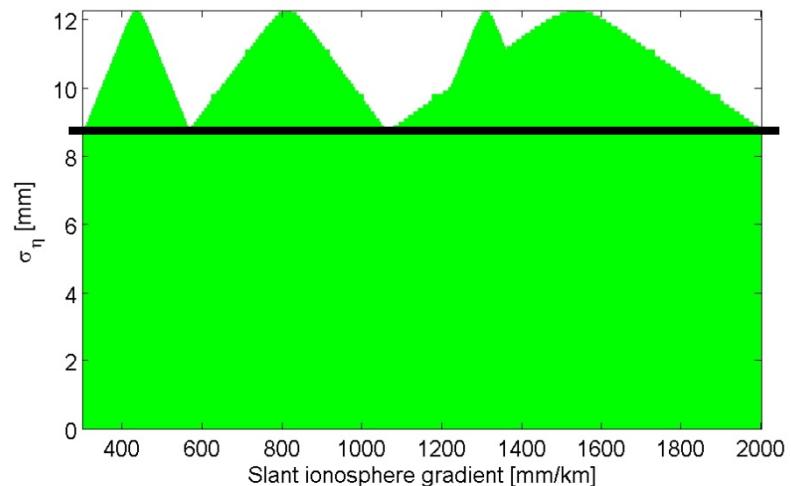
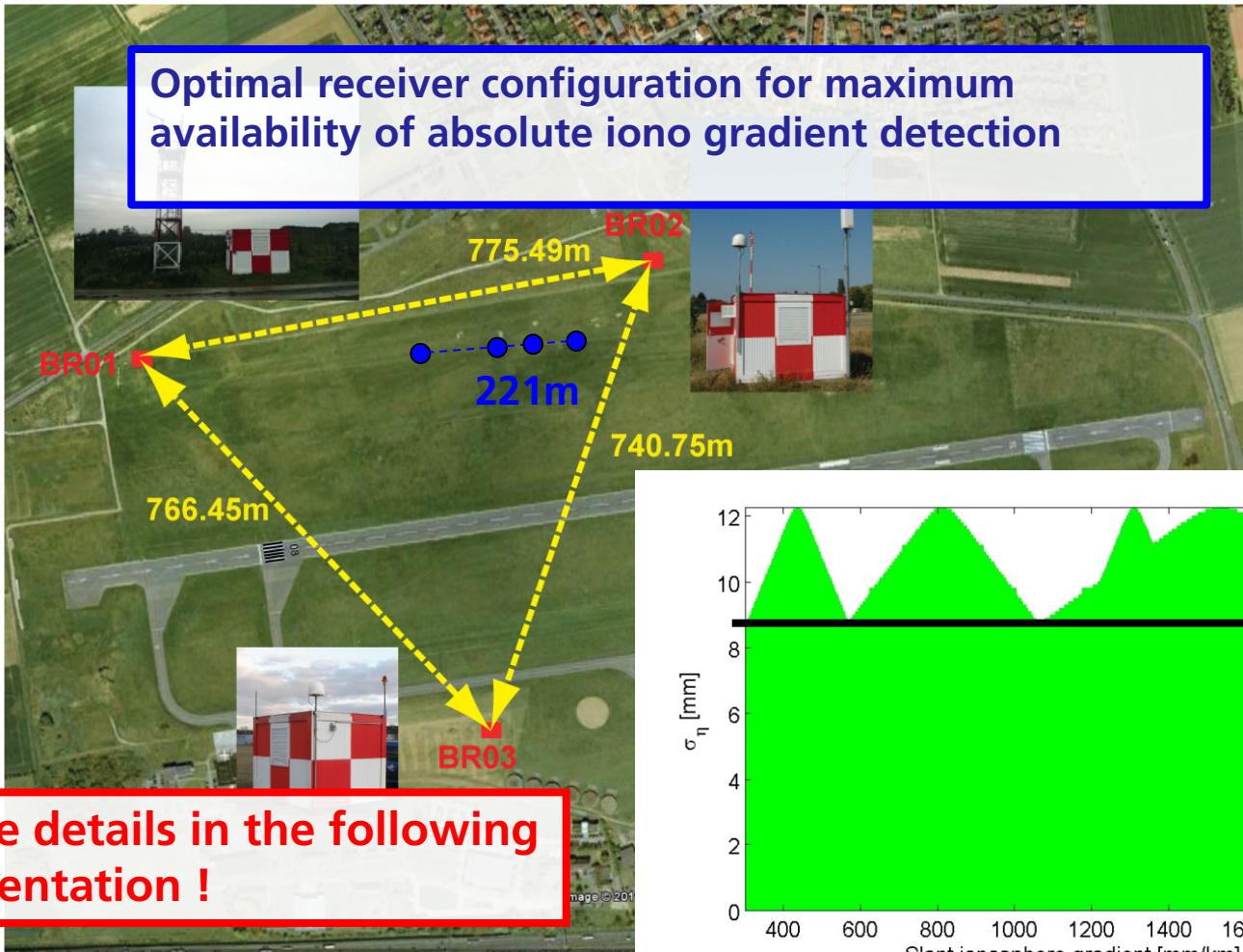


$\sigma_\eta$  is phase noise of receiver & antenna

# Optimal absolute iono gradient monitoring network



# Optimal absolute iono gradient monitoring network

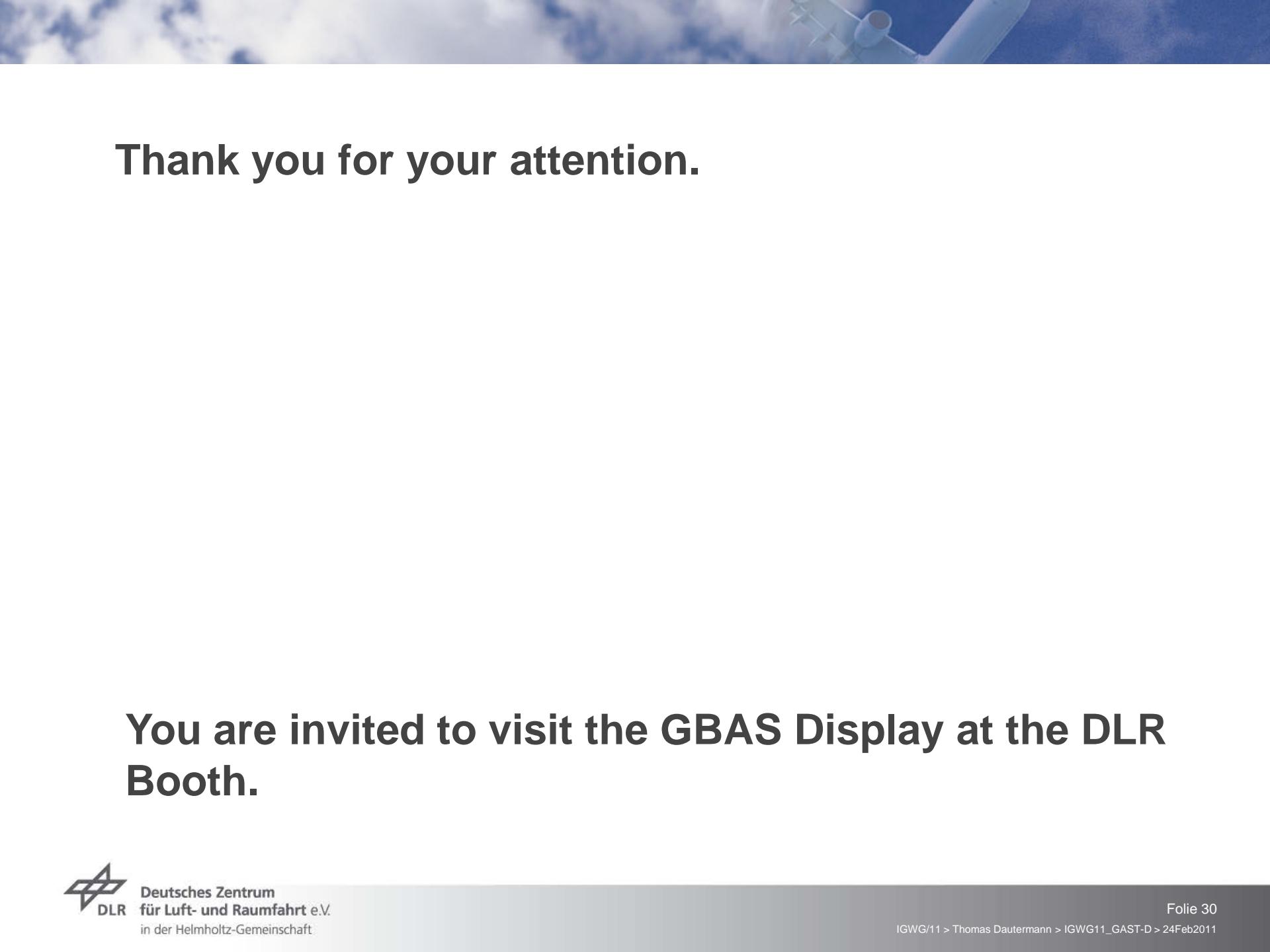


# Summary

- ↗ GAST-D capability of testbed positive
- ↗ Monitors and system performed within nominal limits

For 2011-2012:

- ↗ Real time functionality 
- ↗ Absolute ionosphere gradient monitor set up
- ↗ Initial Autoland Trials with ATTAS (VWF614) or ATRA (A320)



**Thank you for your attention.**

**You are invited to visit the GBAS Display at the DLR Booth.**