## STABILITY AND VIBRATION ROBUSTNESS OF A REAL-TIME SYNTHETIC DISPERSION INTERFEROMETER

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## **Motivation**

#### Static pressure measurement

- Hull-mounted pressure port
- Measurement within aerodynamic influence
  - Extensive calibration required
- Risk of undetected sensor failure (icing)
  - R. Jäckel et al., Flow. Meas. Instrum. 81 (2021)
  - Y. Cao et al., Aerosp. Sci. Technol. 75, 353-385 (2018)

#### **Optical measurement**

- Detection of sensor failure
  - Active emission of radiation
- Measurement of  $p_0$  outside of boundary layer



#### Aeronautical application reqs.

- $\Delta p \approx 30 \text{ Pa}$ •
- Bandwidth ~ 30 Hz •
- Structural vibrations

## Interferometric approach



#### **Principle** Ciddor equation $\Delta n \propto \Delta p$ **Refractive index** Interferometric measurement of $\Delta n$ n = n(p, T, rh, $\eta_{CO2}$ ) **Classic Michelson interferometer** PD Fully sensitive to mechanical $\Delta \varphi$ Interferometric $n(\lambda,p,T,rh)$ BS measurement $\Delta \phi \propto \Delta n$ Probe Ref.

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 $\cdot [n(\lambda_{2\omega}, p) - n(\lambda_{\omega}, p)] \cdot l$ 

 $\Delta \varphi =$ 

Related publications:

- V.P. Drachev, Meas Tech 33, 1125–1127 (1990)
- F. Brandi et al., Opt. Lett. **32**, 2327-2329 (2007)

## Synthetic Dispersion Interferometer (SDI)



#### Setup

- Two-color heterodyne measurement of  $n(\lambda, p, T, rh)$ 
  - cw DPSS laser with intracavity SHG
- Acousto-optic modulator (AOM) generates ref.
  - 1<sup>st</sup> diffraction order of  $\lambda_1$  collinear with 2<sup>nd</sup> diffraction order of  $\lambda_2$

#### Related publications:

- J. Irby et. al., Rev. Sci. Instrum. **70**, 699 (1999)
- D.-G. Lee et al., Rev. Sci. Instrum. 92, 033536 (2021)
- H. Uittenbosch et al., Opt. Express **31**, 6356-6369 (2023)



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## **SDI – digital demodulation**





# Field programmable gate array (FPGA)-based digital demodulation $f_s = 15.625 \text{ MHz}$

#### Concept

- Real-time IQ demodulation
  - RedPitaya STEMlab 125-14
- $\frac{f_s}{4}$  at root of CIC filter
- Output bandwidth ~488 kHz
- $\Delta \phi = \phi_2 2 \cdot \phi_1$ 
  - Digital "frequency doubling"
- Output values
  - $\Delta \phi$ ,  $\phi_1$ ,  $\phi_2$ ,  $z_1$  and  $z_2$



## **Mechanical and long-term stability**

#### Questions

- Do vibrations cancel out?
- Does drift become an issue without stabilization?

Μ



DPSSL

## **Vibration suppression**



RM



- Piezoelectric adjuster induces vibrations of retroreflector as  $A_0 \cdot \sin(2\pi f_v \cdot t)$
- AM of  $\Delta \phi(t)$ ,  $\phi_1(t)$  and  $\phi_2(t)$  at  $f_v$  obtained via IQ-demodulation

## **Vibration suppression**



RM



- Non-common phase errors in probe arm:
  - mod. of  $\Delta \phi$  suppressed by several orders of magnitude
  - mod. of  $\Delta \phi$  uncorrelated with respect to  $\phi_1$  and  $\phi_2$

## Long-term stability



#### Exp. setup

- Ambient pressure meas.
  - $p_0 = 0.955 \cdot 10^5 \text{ Pa}$
- Piezoresistive ref. sensor
  - Keller Series 33X (10 Hz)
- -2.386 mPa/s linear drift
  - Electronics (cables, PLL, etc.)
- $\left|\Delta p_{Ref.} \Delta p_{SDI}\right| \le 159 \text{ Pa}$ 
  - $\delta\Delta\phi \leq 0.48$  rad
- Single-Arm DI

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- $\delta \Delta \phi \leq 0.5$  rad after correction over 48 hours
- K.J. Brunner et al., JINST 14, P11016 (2019)



## **Summary**



## **Optical, contact-free variometer in aviation**

- Self-diagnosis capability
- Measurement outside of aerodynamic influence
- Low optical power (eye-safety)
- Closed beam-path

### Outlook

- Laboratory proof-of-concept
  - Opt. Express **31**, 6356-6369 (2023)
- Simple setup with good prospect for integration
- Lower  $\Delta p$  required
  - Reduction of system noise
  - Optimization of interference fringes



## Thank you for your attention!

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