

# DLRK 2022

Active vibration suppression of wind tunnel models using piezoelectric materials

Anna Altkuckatz



**DLRK 2022**  
DEUTSCHER LUFT- UND  
RAUMFAHRTKONGRESS  
27. - 29. SEPTEMBER 2022 – DRESDEN  
„Luft- und Raumfahrt - gemeinsam forschen und nachhaltig gestalten“





FH AACHEN  
UNIVERSITY OF APPLIED SCIENCES



Institute of  
Aeroelasticity

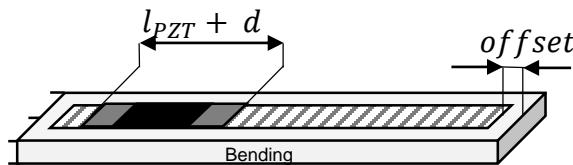
# Investigation goals



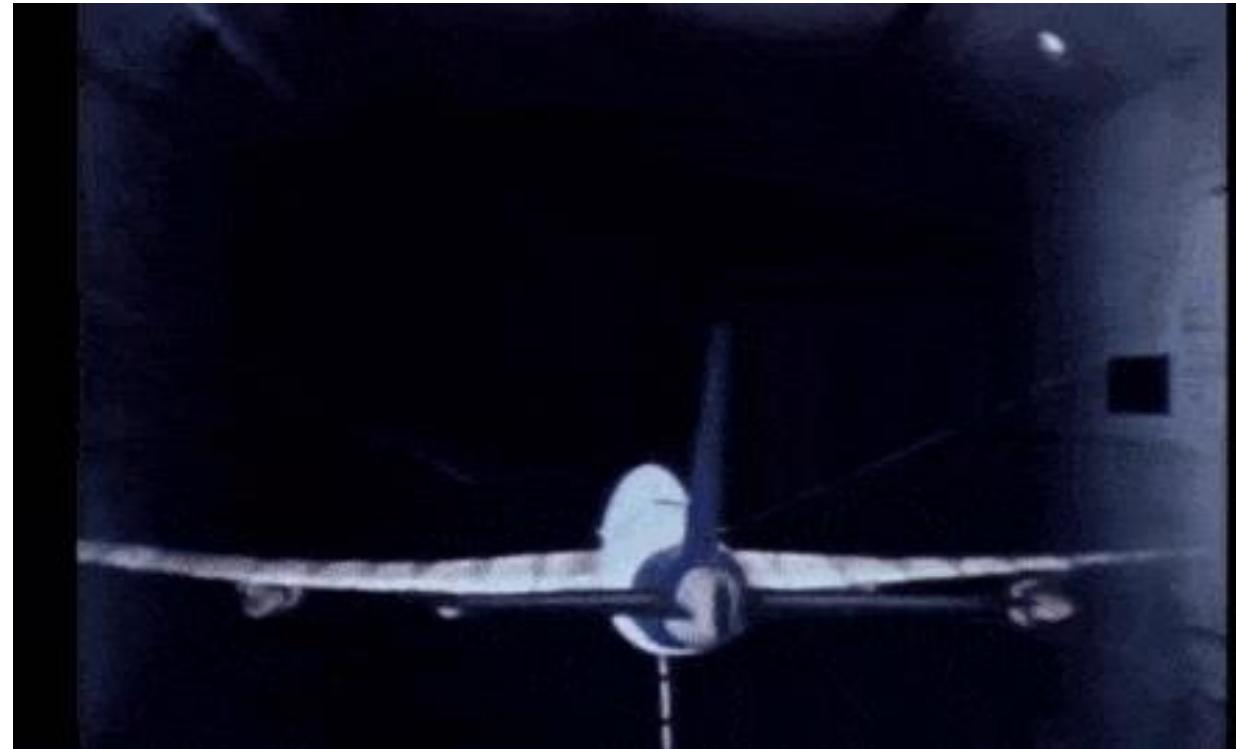
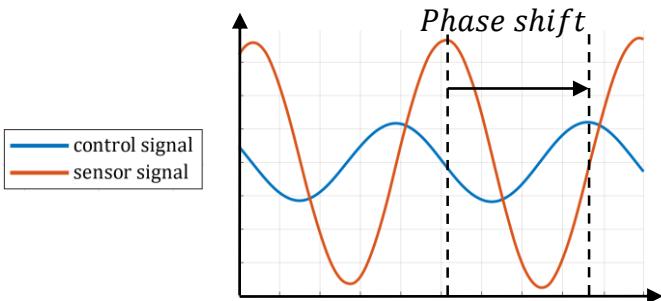
Is it possible to damp vibrations due to flutter with PZTs?



What is the optimal position & size of the PZTs?



Which control signal is required?



<https://personal.lse.ac.uk/ROBERT49/ebooks/PhilSciAdventures/lecture12.html>

# Agenda

-  Investigation goals
-  Foundations
-  Methodology
-  Validation of the methodology
-  Application of the methodology
-  Summary and Future application ideas

# Agenda



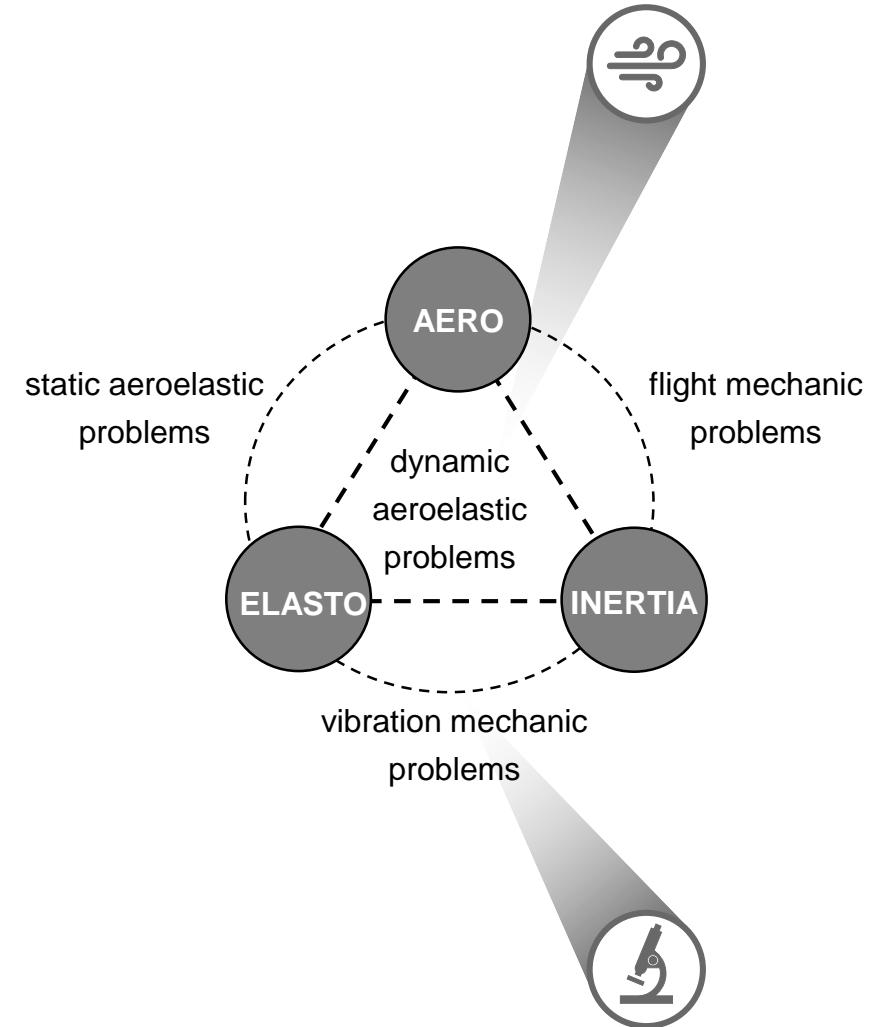
-  Investigation goals
-  Foundations
-  Methodology
-  Validation of the methodology
-  Application of the methodology
-  Summary and Future application ideas

# Foundations

Application of the methodology

## Aeroelasic problem

- Aeroelastic triangle of forces

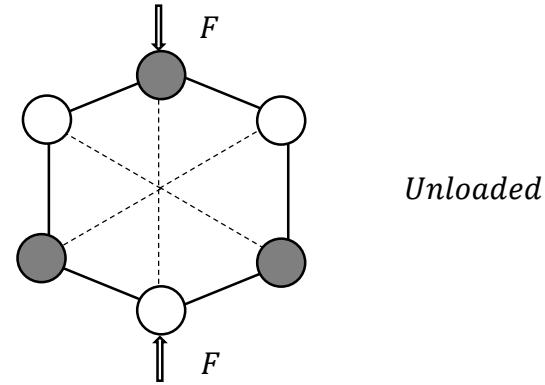


Validation of the methodology

## Aeroelastic problem

- Aeroelastic triangle of forces

## Piezoelectric materials

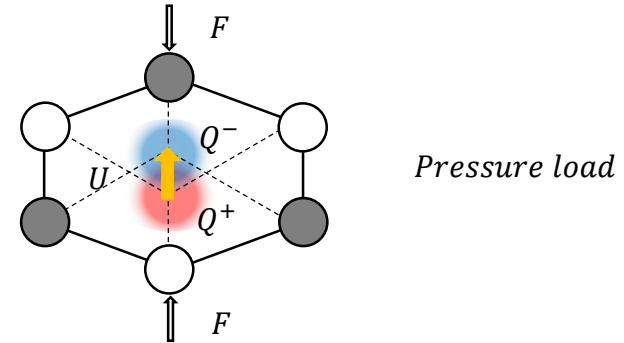


○  $Si^+$   
●  $O^-$

## Aeroelastic problem

- Aeroelastic triangle of forces

## Piezoelectric materials



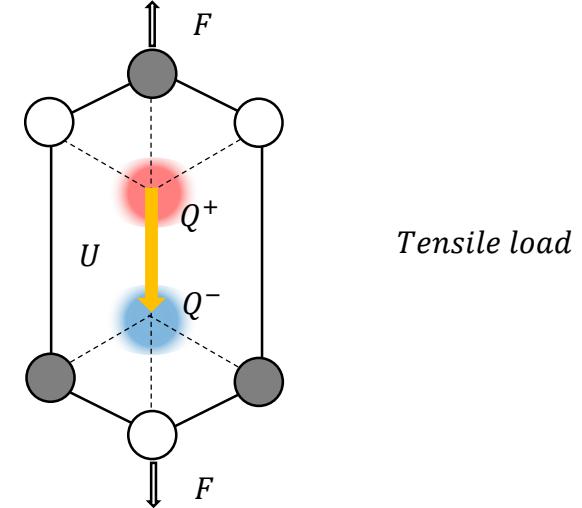
Pressure load

○  $Si^+$   
●  $O^-$

## Aeroelastic problem

- Aeroelastic triangle of forces

## Piezoelectric materials

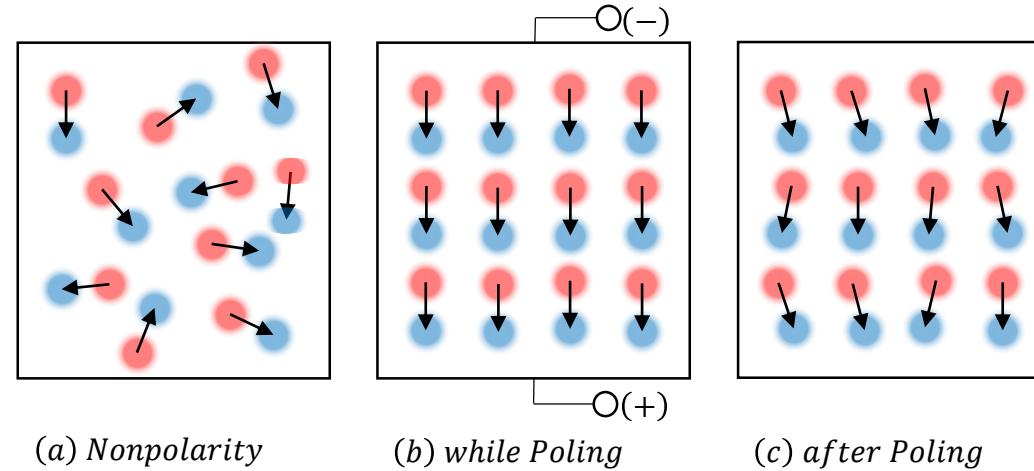


○  $Si^+$   
●  $O^-$

## Aeroelasic problem

- Aeroelastic triangle of forces

## Piezoelectric materials



○  $Si^+$   
●  $O^-$



## Aeroelastic problem

- Aeroelastic triangle of forces

## Piezoelectric materials

- Direct piezoelectric effect
- Inverse piezoelectric effect

Direct piezoelectric effect:

Sensor



$$P = d * T = e * S$$

Inverse piezoelectric effect:

Actuator



$$S = d * E$$

$P$  := polarisation

$d, e$  := piezoelectric coefficients

$T$  := mechanical stress

$E$  := electric field strength

$S$  := deformation



## Aeroelastic problem

- Aeroelastic triangle of forces

## Piezoelectric materials

- Direct piezoelectric effect
- Inverse piezoelectric effect
- Coupled equations

$$P = d * T = e * S$$

$$S = d * E$$



$$S = s^E * T + d^t * E$$

$$D = d * T + \epsilon * E$$

$\epsilon$  := permittivity

$s^E$  := inverse of stiffness

$D$  := electric displacement field

superscript " $t$ " := transposition

$P$  := polarisation

$d, e$  := piezoelectric coefficients

$T$  := mechanical stress

$E$  := electric field strength

$S$  := deformation



# Agenda



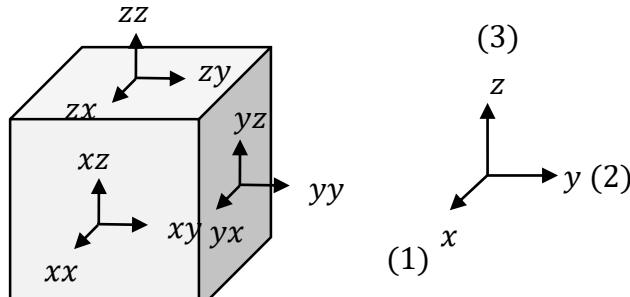
-  Investigation goals
-  Foundations
-  **Methodology**
-  Validation of the methodology
-  Application of the methodology
-  Summary and Future application ideas

# Methodology

## Modelling of structure

$$S = s^E T + d^t E$$

$$D = dT + \epsilon E$$



$$\begin{Bmatrix} S_1 \\ S_2 \\ S_3 \\ S_4 \\ S_5 \\ S_6 \end{Bmatrix} = \begin{bmatrix} s_{11} & s_{12} & s_{13} & 0 & 0 & 0 \\ s_{21} & s_{22} & s_{23} & 0 & 0 & 0 \\ s_{31} & s_{32} & s_{33} & 0 & 0 & 0 \\ 0 & 0 & 0 & s_{44} & 0 & 0 \\ 0 & 0 & 0 & 0 & s_{55} & 0 \\ 0 & 0 & 0 & 0 & 0 & s_{66} \end{bmatrix} \begin{Bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \\ T_6 \end{Bmatrix}$$

$\epsilon :=$  permittivity

$s^E :=$  inverse of stiffness

$D :=$  electric displacement field

*superscript "t" := transposition*

$P :=$  polarisation

$d, e :=$  piezoelectric coefficients

$T :=$  mechanical stress

$E :=$  electric field strength

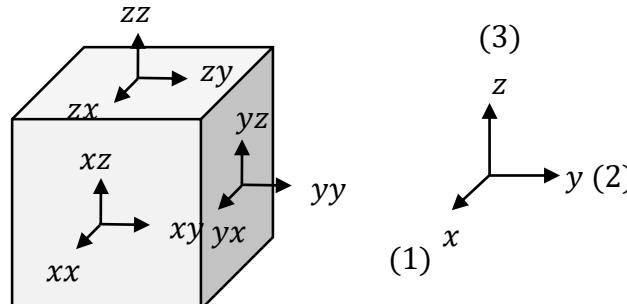
$S :=$  deformation (dimensionless)

# Methodology

## Modelling of structure

$$S = s^E T + d^t E$$

$$D = dT + \epsilon E$$



$$\begin{Bmatrix} S_1 \\ S_2 \\ S_3 \\ S_4 \\ S_5 \\ S_6 \\ D_1 \\ D_2 \\ D_3 \end{Bmatrix} = \begin{bmatrix} s_{11} & s_{12} & s_{13} & 0 & 0 & 0 & 0 & 0 & d_{31} \\ s_{21} & s_{22} & s_{23} & 0 & 0 & 0 & 0 & 0 & d_{32} \\ s_{31} & s_{32} & s_{33} & 0 & 0 & 0 & 0 & 0 & d_{33} \\ 0 & 0 & 0 & s_{44} & 0 & 0 & 0 & d_{24} & 0 \\ 0 & 0 & 0 & 0 & s_{55} & 0 & d_{15} & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & s_{66} & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & d_{15} & 0 & \epsilon_{11} & 0 & 0 \\ 0 & 0 & 0 & d_{24} & 0 & 0 & 0 & \epsilon_{22} & 0 \\ d_{31} & d_{32} & d_{33} & 0 & 0 & 0 & 0 & 0 & \epsilon_{33} \end{bmatrix} \begin{Bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \\ T_6 \\ E_1 \\ E_2 \\ E_3 \end{Bmatrix}$$

$\epsilon$  := permittivity

$s^E$  := inverse of stiffness

$D$  := electric displacement field

superscript "t" := transposition

$P$  := polarisation

$d, e$  := piezoelectric coefficients

$T$  := mechanical stress

$E$  := electric field strength

$S$  := deformation (dimensionless)

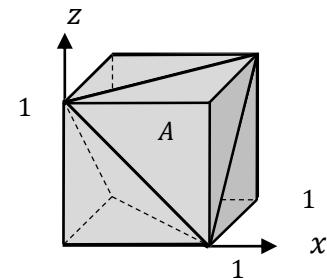
# Methodology

## Modelling of structure

$$S = s^E T + d^t E$$

$$D = dT + \epsilon E$$

## Setting up and solving PDEs



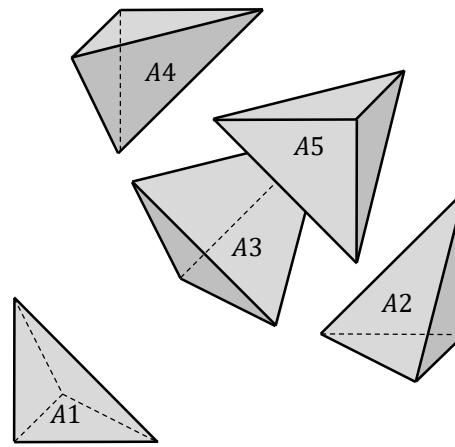
# Methodology

## Modelling of structure

$$S = s^E T + d^t E$$

$$D = dT + \epsilon E$$

## Setting up and solving PDEs



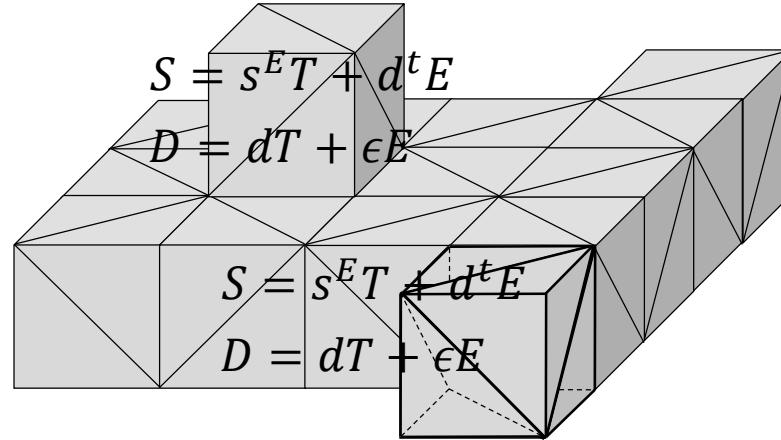
# Methodology

## Modelling of structure

$$S = s^E T + d^t E$$

$$D = dT + \epsilon E$$

## Setting up and solving PDEs



# Methodology

## Modelling of structure

$$S = s^E T + d^t E$$

$$D = dT + \epsilon E$$

## Setting up and solving PDEs

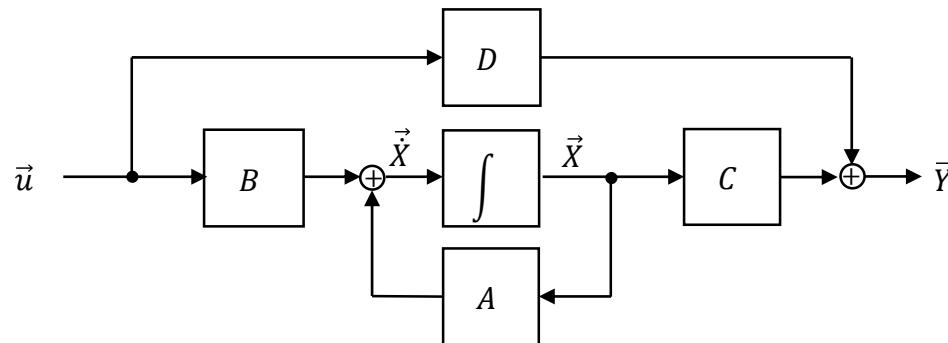
## State-space representation of FEM model

$$[M]_{gen}\{\ddot{q}\} + [D]_{gen}\{\dot{q}\} + [C]_{gen}\{q\} = \{F\}_{gen} + p\{Q_{1V}\}_{gen}$$



$$\{\dot{X}\} = [A]\{X\} + [B]\{u\}$$

$$\{Y\} = [C]\{X\} + [D]\{u\}$$



$$m_{ij} := [M]_{gen} = [\phi]^t [M] [\phi]$$

$$c_{ij} := [C]_{gen} = [\phi]^t [C] [\phi]$$

$$d_{ij} := [D]_{gen} = [\phi]^t [D] [\phi]$$

$$\{F\}_{gen} = [\phi]^t \{F\}$$

generalized mass matrix

generalized stiffness matrix

generalized damping matrix

generalized force vector



# Methodology

## Modelling of structure

$$S = s^E T + d^t E$$

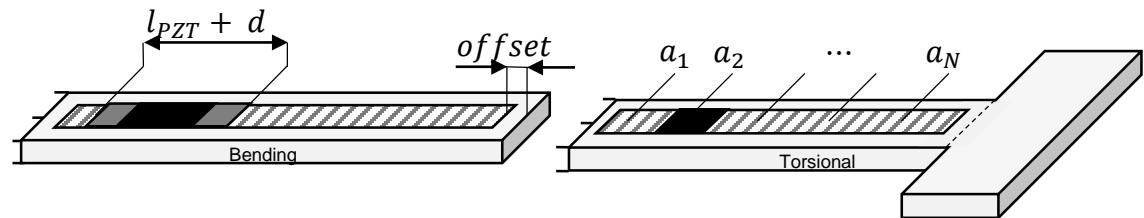
$$D = dT + \epsilon E$$

## Setting up and solving PDEs

## State-space representation of FEM model

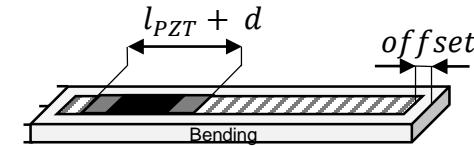
## Position optimization

- Two different bending beams for position optimization analysis



$a :=$  position PZT  
 $l_{PZT} :=$  length PZT  
 $d :=$  PZT growth rate  
 $N :=$  number of positions

# Methodology



## Modelling of structure

$$S = s^E T + d^t E$$

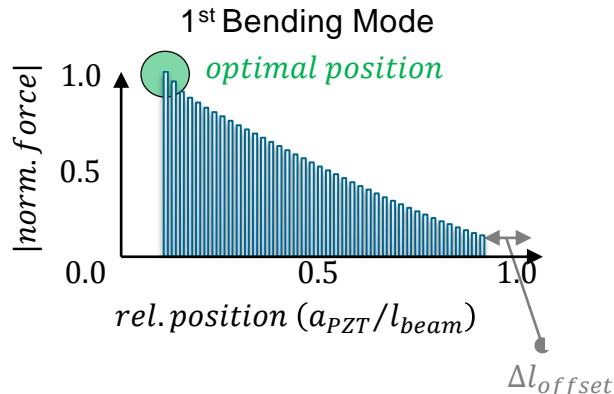
$$D = dT + \epsilon E$$

## Setting up and solving PDEs

## State-space representation of FEM model

## Position optimization

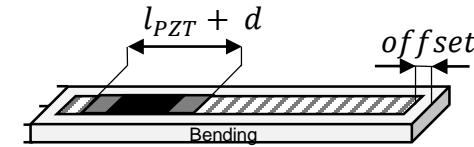
- Two different bending beams for position optimization analysis



$$\begin{aligned}l_{PZT\ min} &= l_{PZT} \\N &= 40; \\ \Delta l_{offset} &= offset + \frac{l_{PZT\ min}}{2} \\ a_{start} &= \Delta l_{offset} \\ a_{end} &= l_{beam} - \Delta l_{offset}\end{aligned}$$



# Methodology



## Modelling of structure

$$S = s^E T + d^t E$$

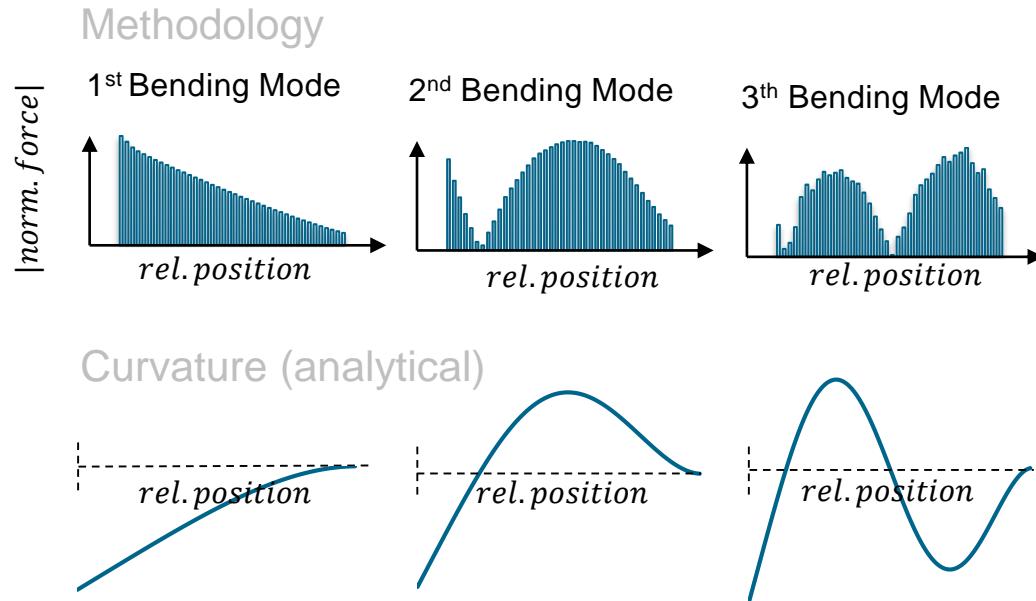
$$D = d T + \epsilon E$$

## Setting up and solving PDEs

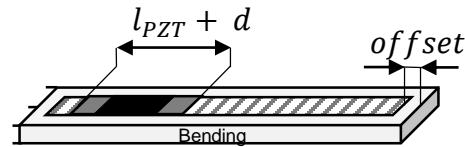
## State-space representation of FEM model

## Position optimization

- Two different bending beams for position optimization analysis



# Methodology



## Modelling of structure

$$S = s^E T + d^t E$$

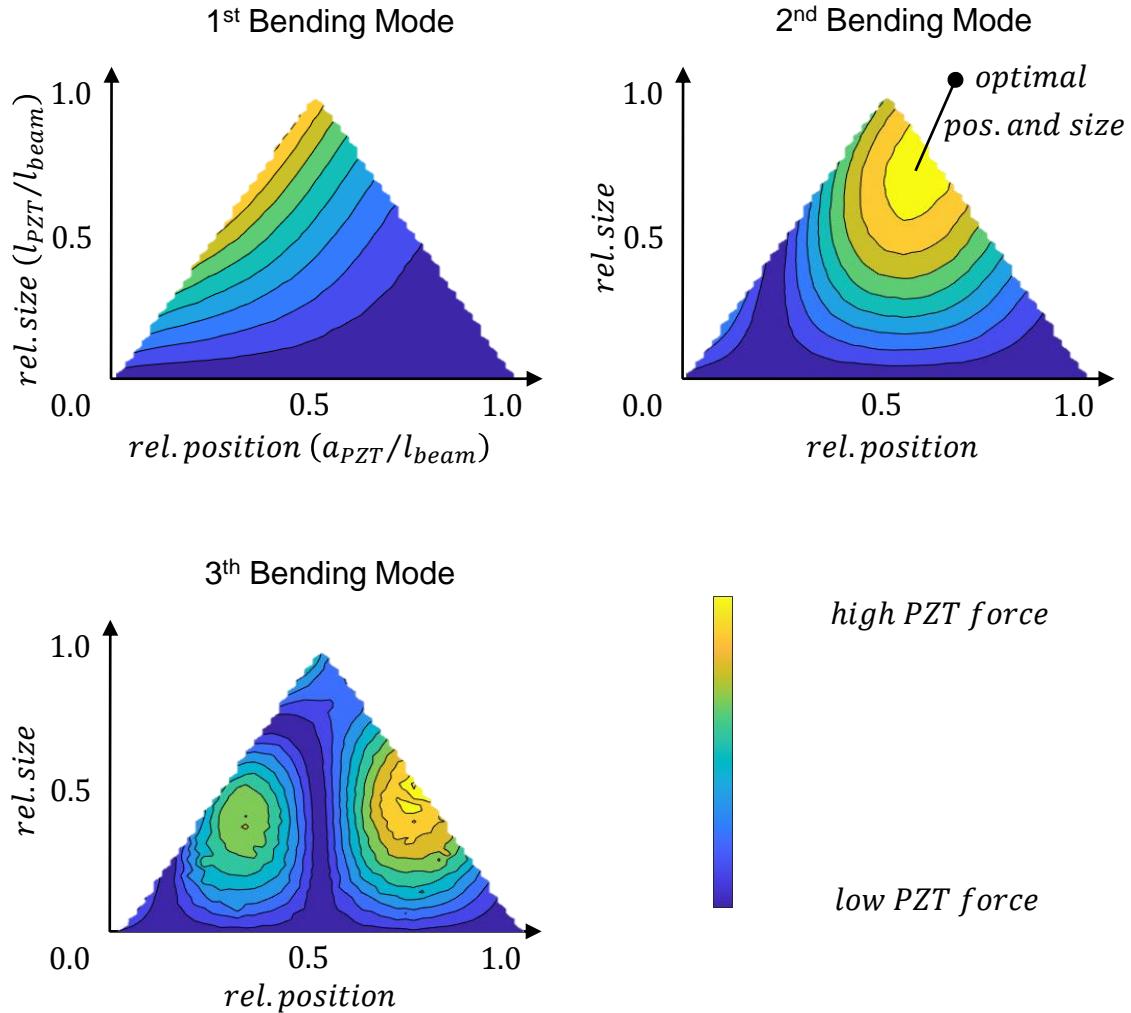
$$D = d T + \epsilon E$$

## Setting up and solving PDEs

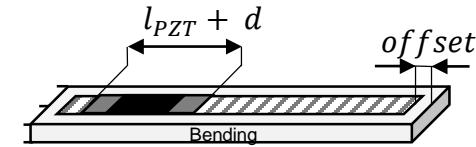
## State-space representation of FEM model

## Position optimization

- Two different bending beams for position optimization analysis



# Methodology



## Modelling of structure

$$S = s^E T + d^t E$$

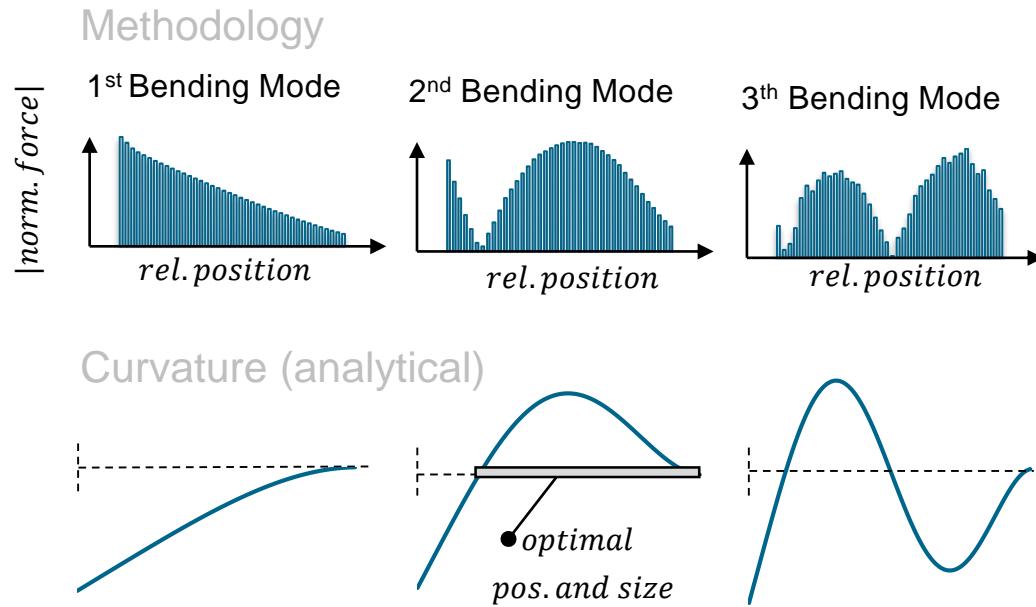
$$D = d T + \epsilon E$$

## Setting up and solving PDEs

## State-space representation of FEM model

## Position optimization

- Two different bending beams for position optimization analysis



# Methodology

## Modelling of structure

$$S = s^E T + d^t E$$

$$D = dT + \epsilon E$$

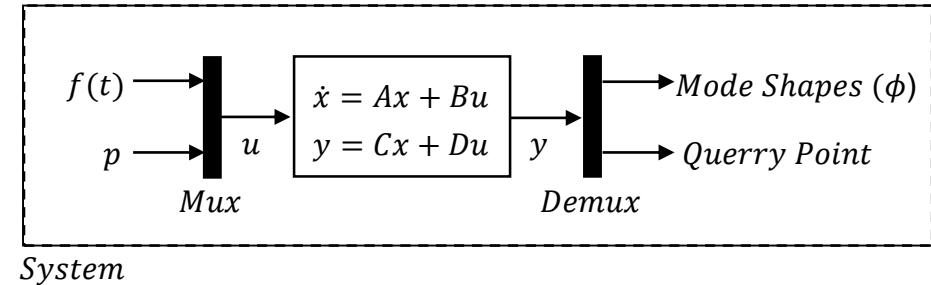
## Setting up and solving PDEs

## State-space representation of FEM model

## Position optimization

- Two different bending beams for position optimization analysis

## Design of control system using SIMULINK



# Methodology

## Modelling of structure

$$S = s^E T + d^t E$$

$$D = dT + \epsilon E$$

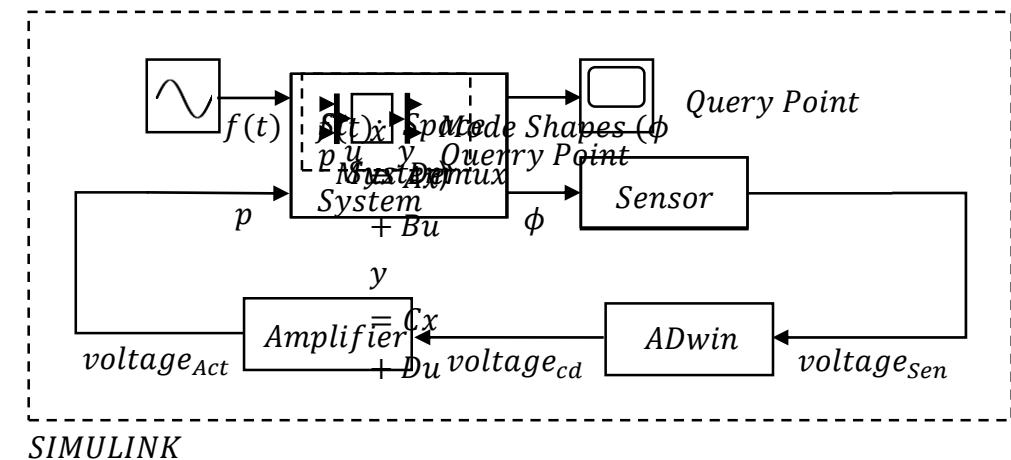
## Setting up and solving PDEs

## State-space representation of FEM model

## Position optimization

- Two different bending beams for position optimization analysis

## Design of control system using SIMULINK



SIMULINK

# Agenda

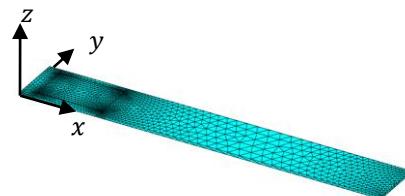


-  Investigation goals
-  Foundations
-  Methodology
-  **Validation of the methodology**
-  Application of the methodology
-  Summary and Future application ideas

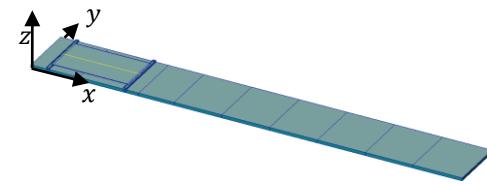
# Validation of the methodology

## Validation of structure

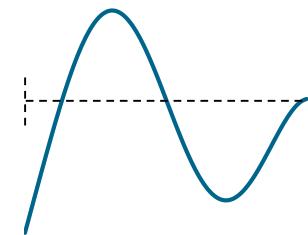
Methodology



Nastran



Analytical



# Validation of the methodology

## Validation of structure

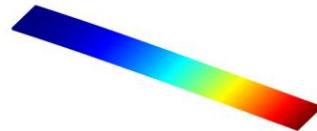
Frequency	Methodology	Nastran	Analytical
-----------	-------------	---------	------------

$f_{e_1}$  [Hz] 21.50 21.73 21.00

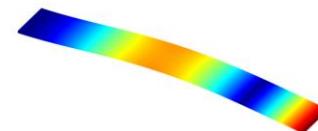
$f_{e_2}$  [Hz] 132.56 130.33 131.50

$f_{e_3}$  [Hz] 290.45 — —

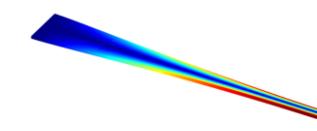
*1<sup>st</sup>Eigenmode (bending)*



*2<sup>nd</sup>Eigenmode (bending)*



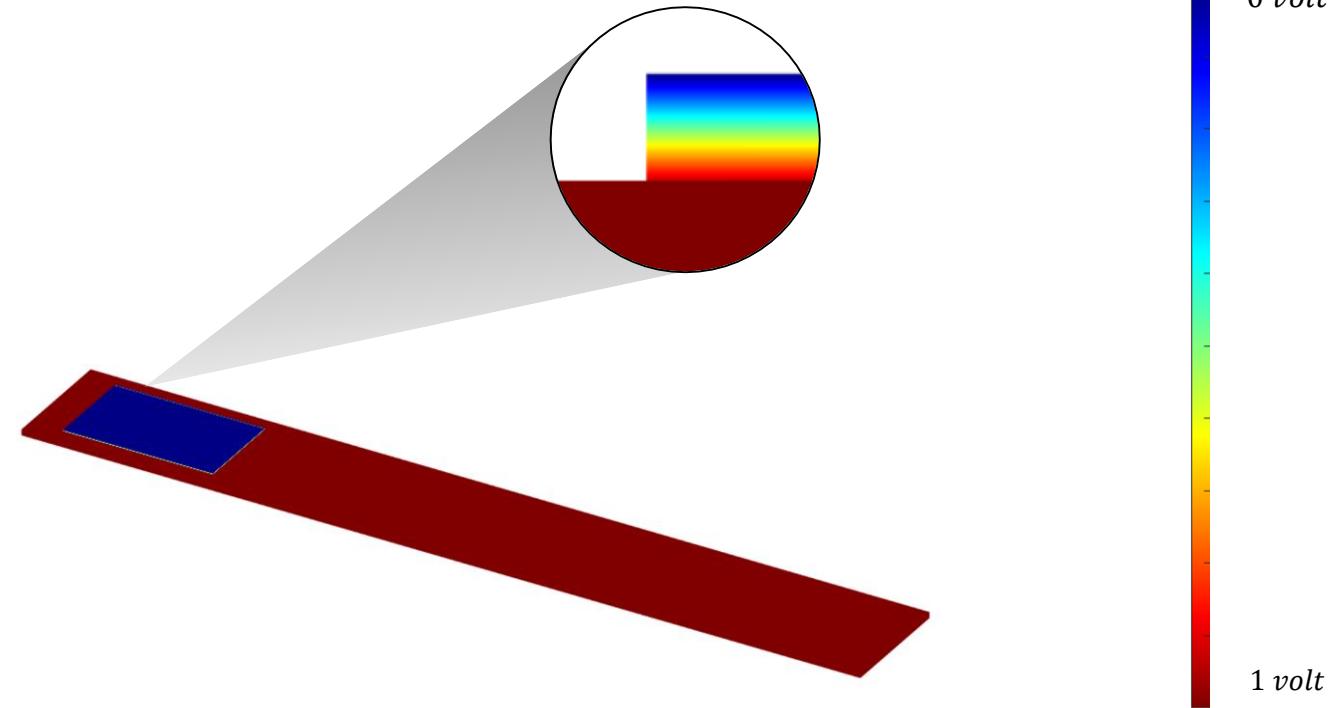
*3<sup>rd</sup>Eigenmode (torsional)*



# Validation of the methodology

Validation of structure

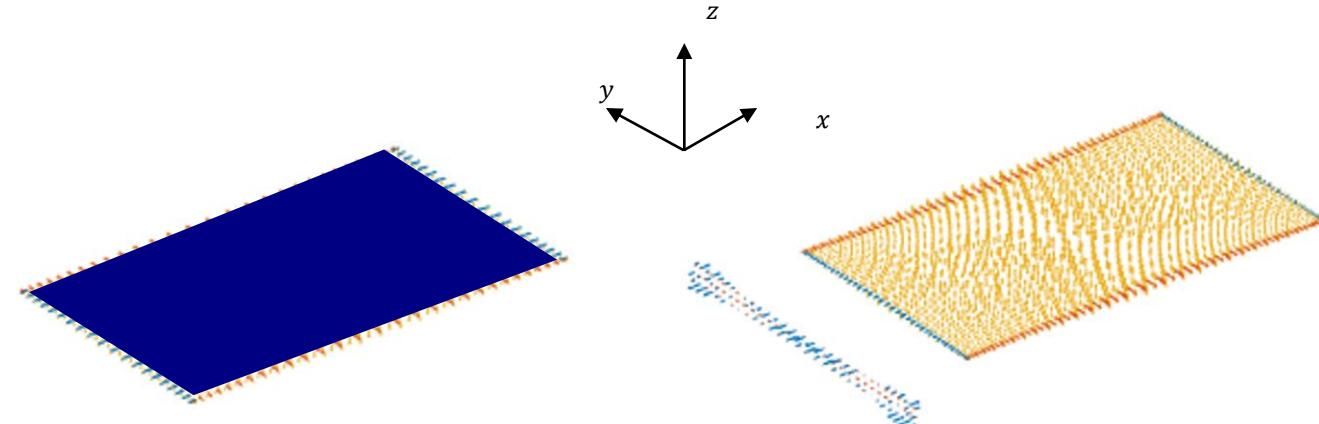
Validation of piezo effect



# Validation of the methodology

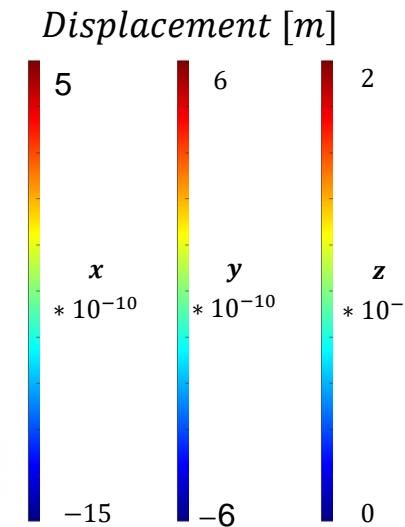
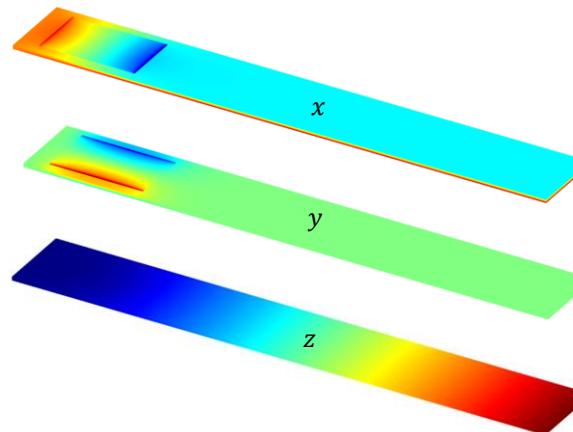
Validation of structure

Validation of piezo effect



*PZT forces*

*total system forces*



<i>direction i</i>	$\sum_i F_n$ [N]
$x$	$3.62 * 10^{-6}$
$y$	$1.42 * 10^{-6}$
$z$	-12.38

$x$  – direction forces

$y$  – direction forces

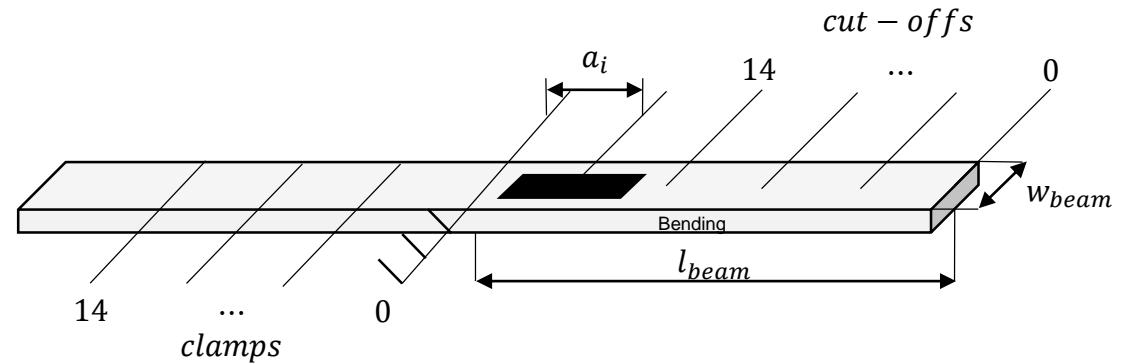
$z$  – direction forces

# Validation of the methodology

Validation of structure

Validation of piezo effect

Validation of position optimization



# Validation of the methodology

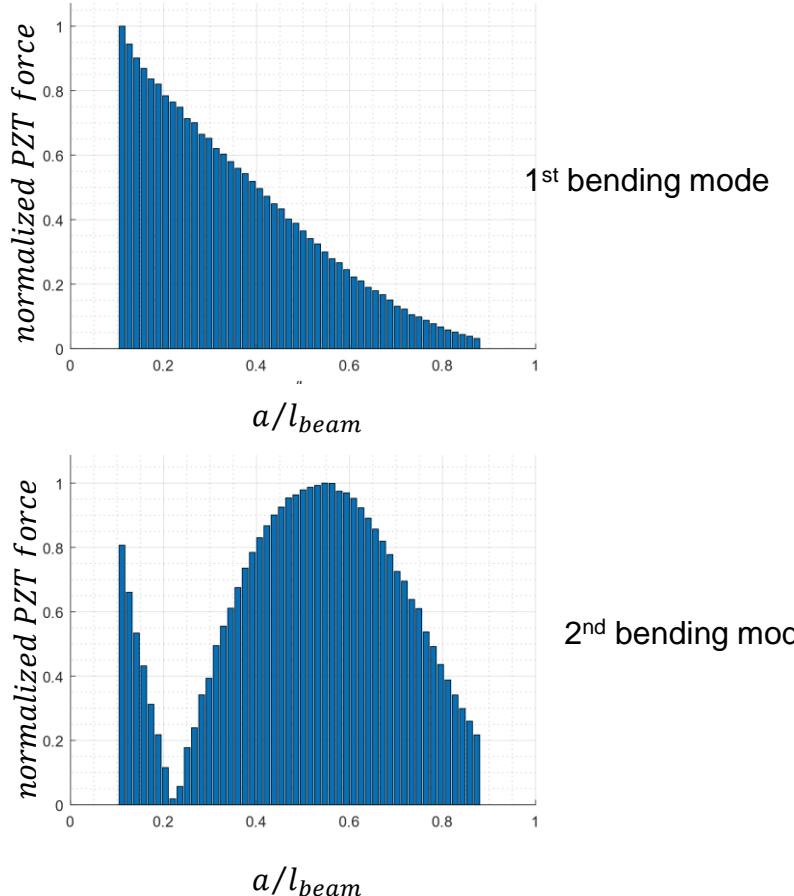


Validation of structure

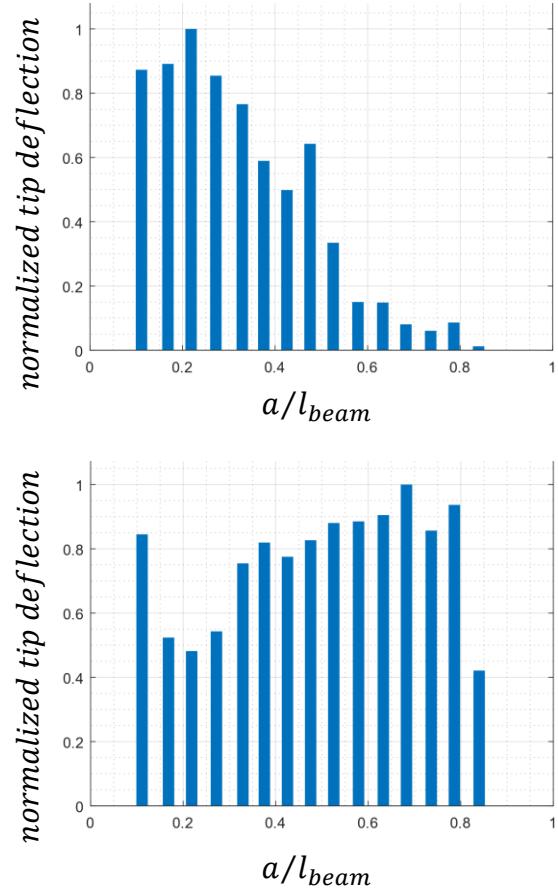
Validation of piezo effect

Validation of position optimization

Simulation



Experiment



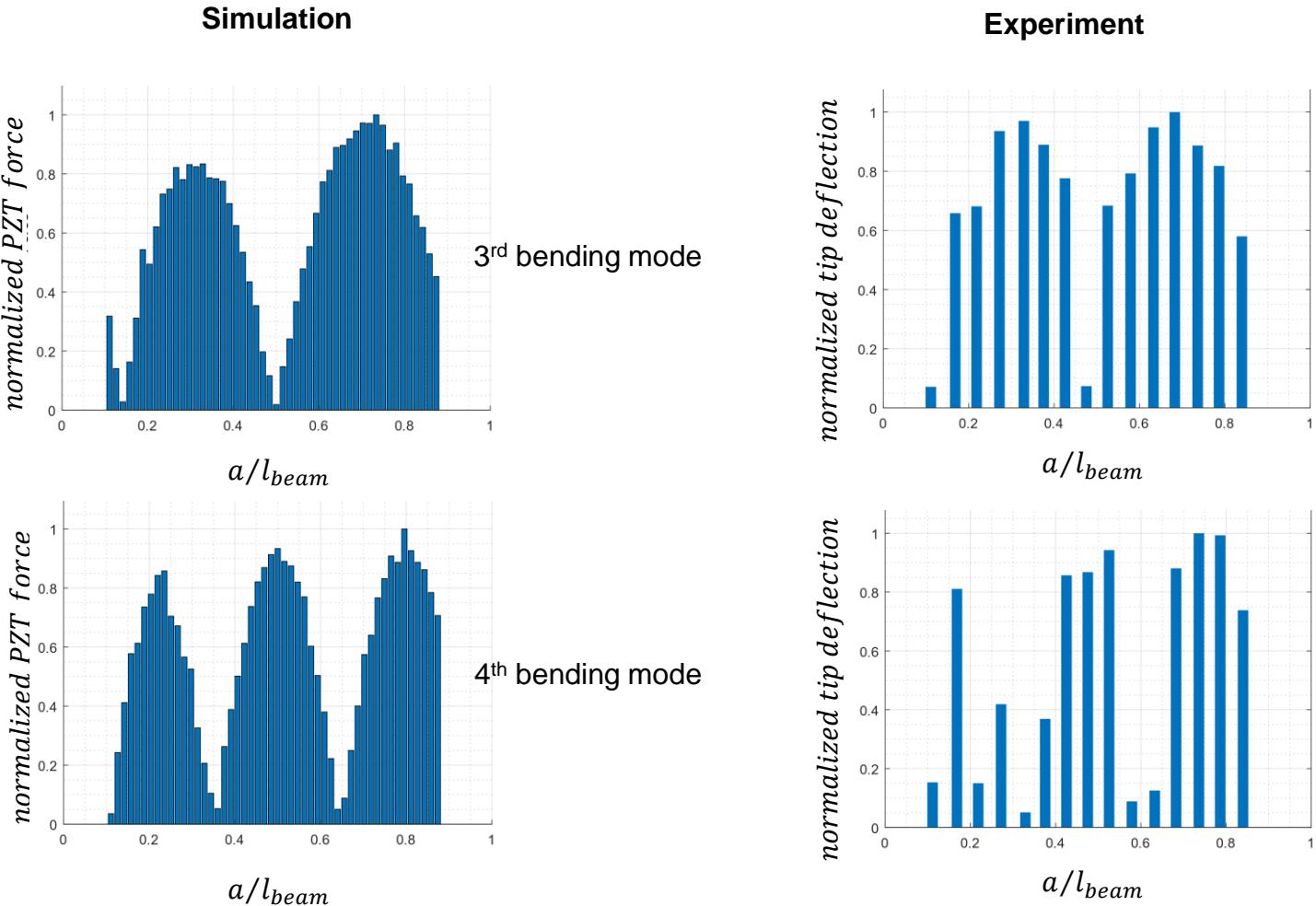
# Validation of the methodology



Validation of structure

Validation of piezo effect

Validation of position optimization



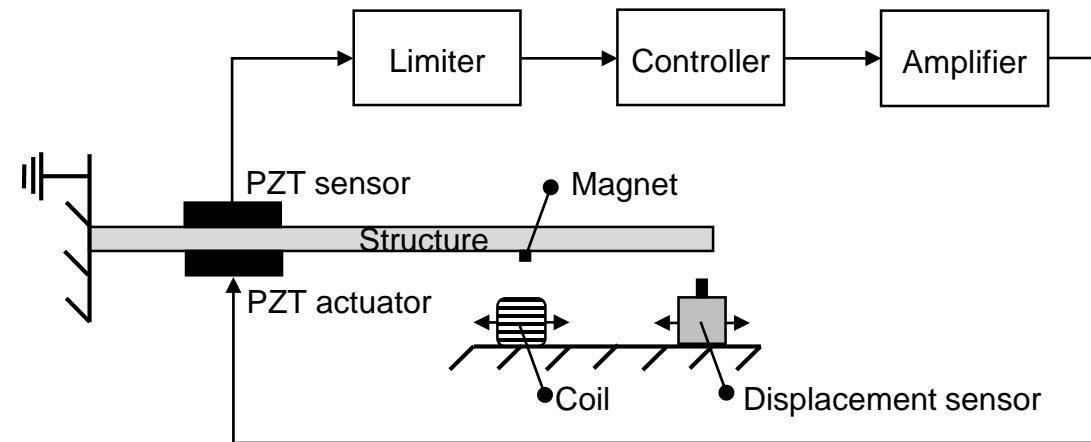
# Agenda



-  Investigation goals
-  Foundations
-  Methodology
-  Validation of the methodology
-  **Application of the methodology**
-  Summary and Future application ideas

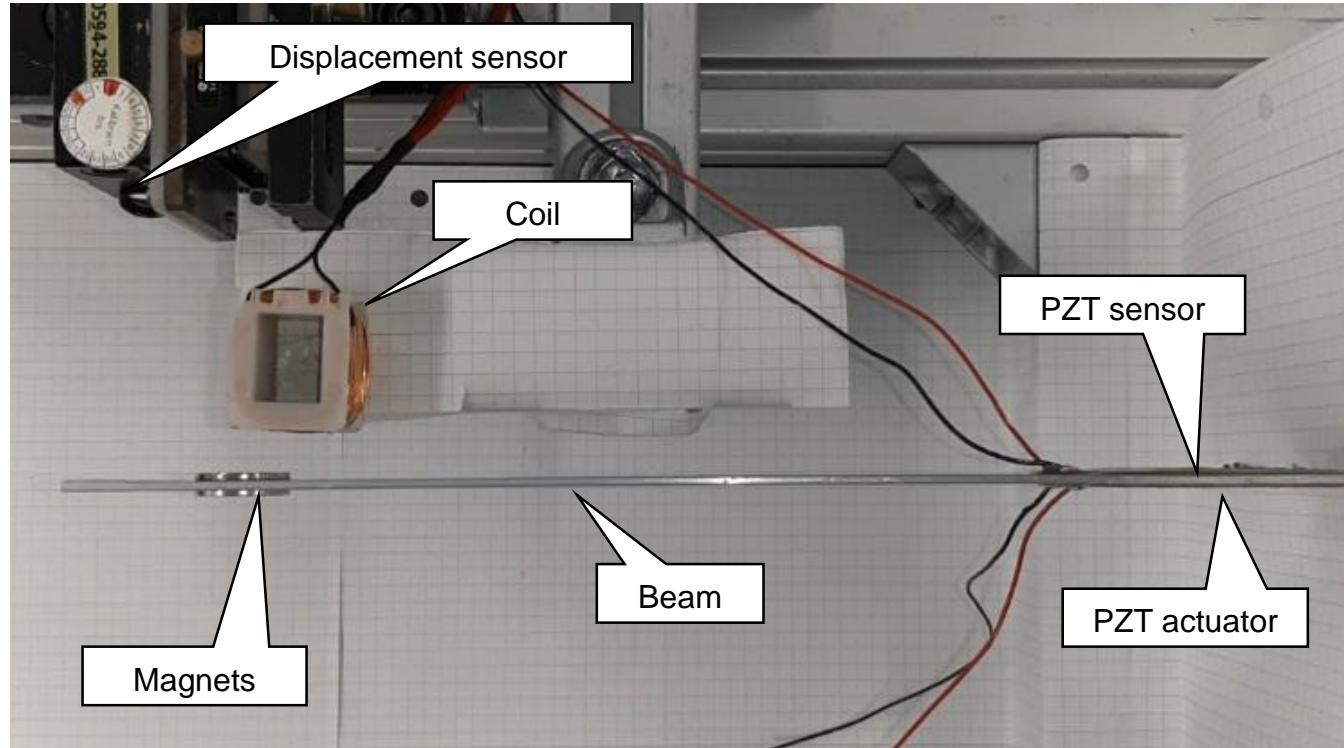
# Application of the methodology

## Test Setup



# Application of the methodology

## Test Setup



# Application of the methodology

## Test Setup

## Pre-Windtunnel tests

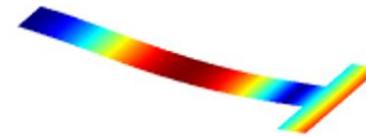
1<sup>st</sup> Mode (bending)

$$f_1 = 4.22 \text{ Hz}$$



2<sup>nd</sup> Mode (bending)

$$f_2 = 29.29 \text{ Hz}$$



3<sup>rd</sup> Mode (torsional)

$$f_3 = 30.01 \text{ Hz}$$



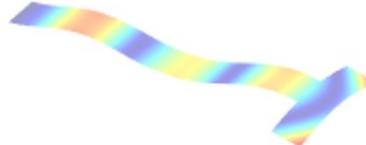
4<sup>th</sup> Mode (bending)

$$f_4 = 91.37 \text{ Hz}$$



5<sup>th</sup> Mode (bending)

$$f_5 = 181.42 \text{ Hz}$$



6<sup>th</sup> Mode (torsional)

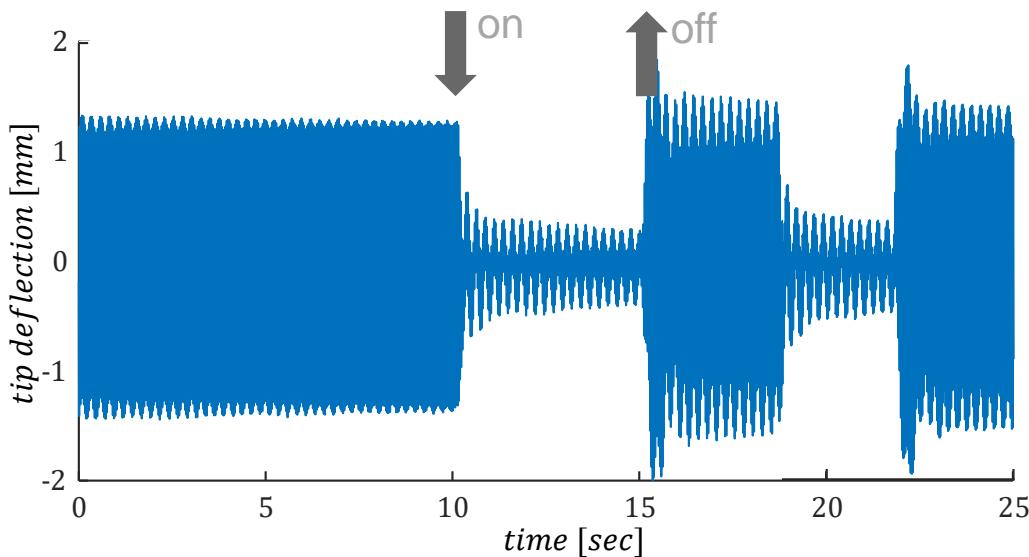
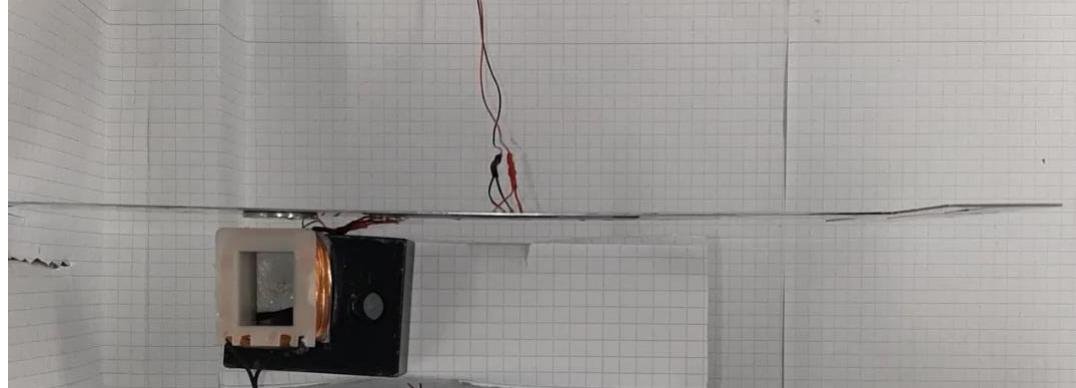
$$f_6 = 188.20 \text{ Hz}$$



# Application of the methodology

## Test Setup

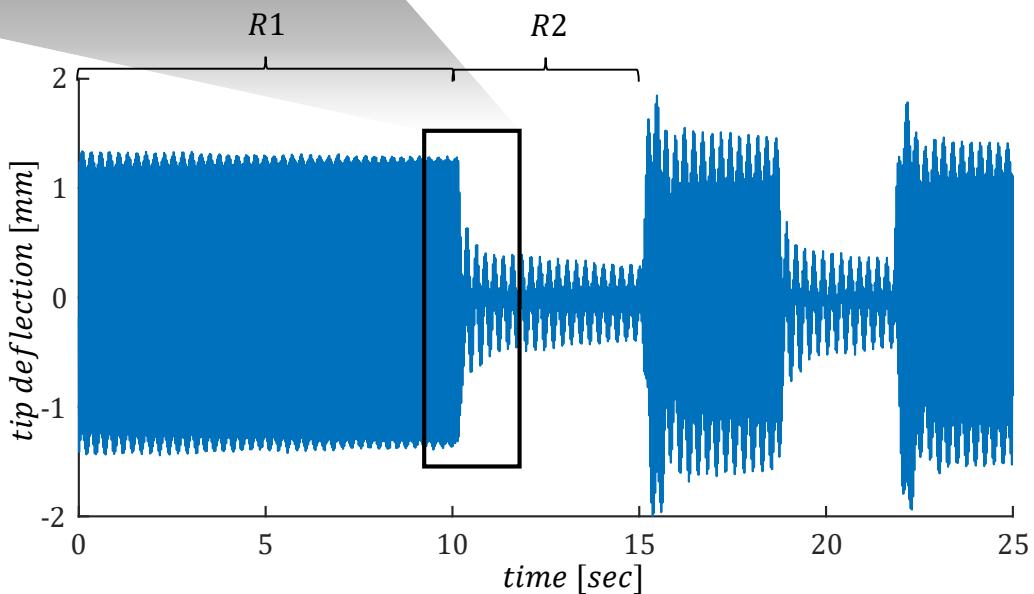
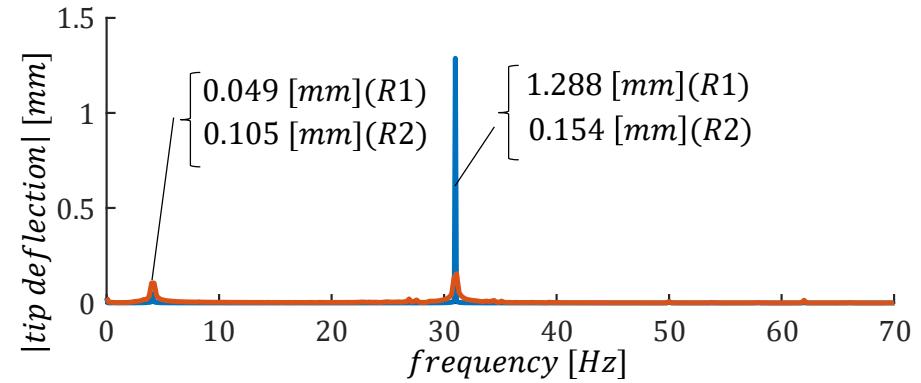
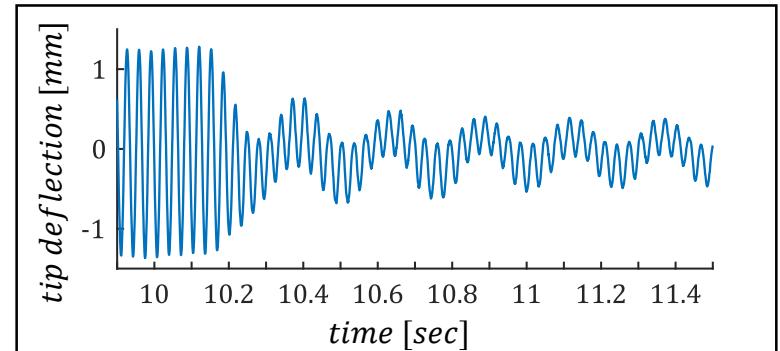
## Pre-Windtunnel tests



# Application of the methodology

## Test Setup

## Pre-Windtunnel tests

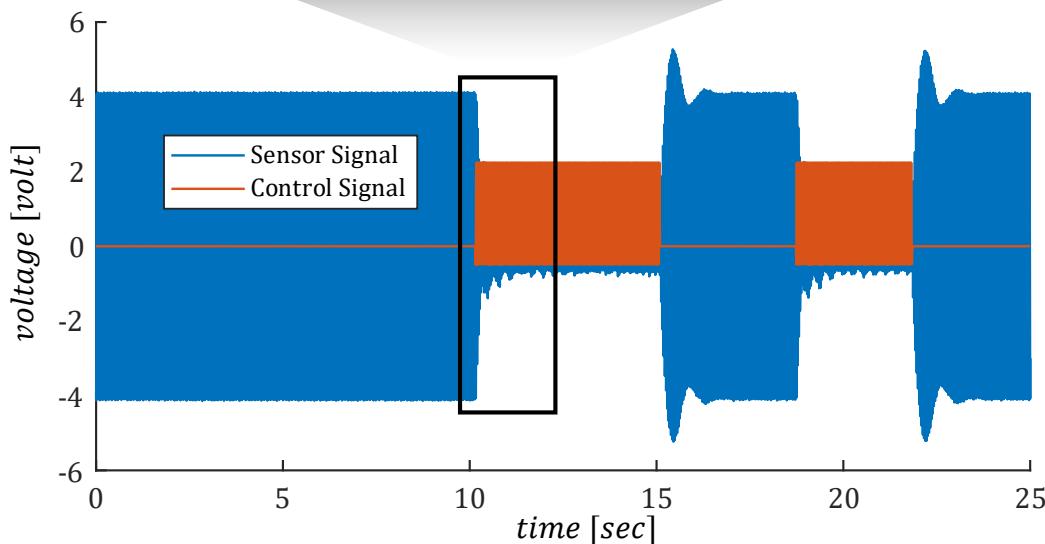
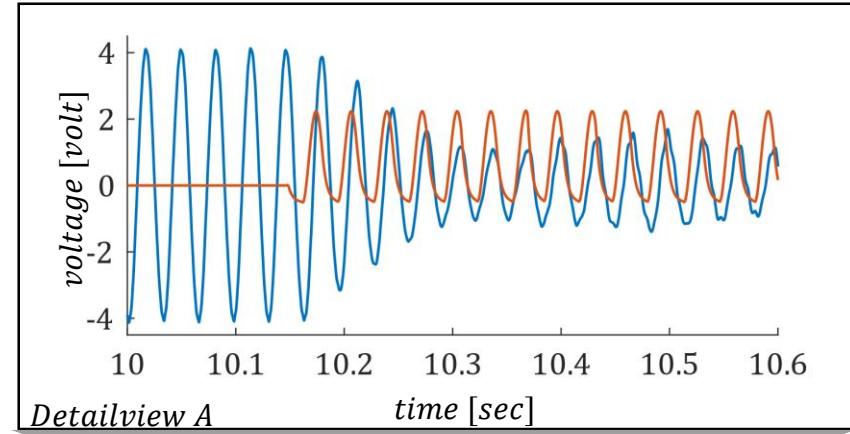


R1  
R2

# Application of the methodology

## Test Setup

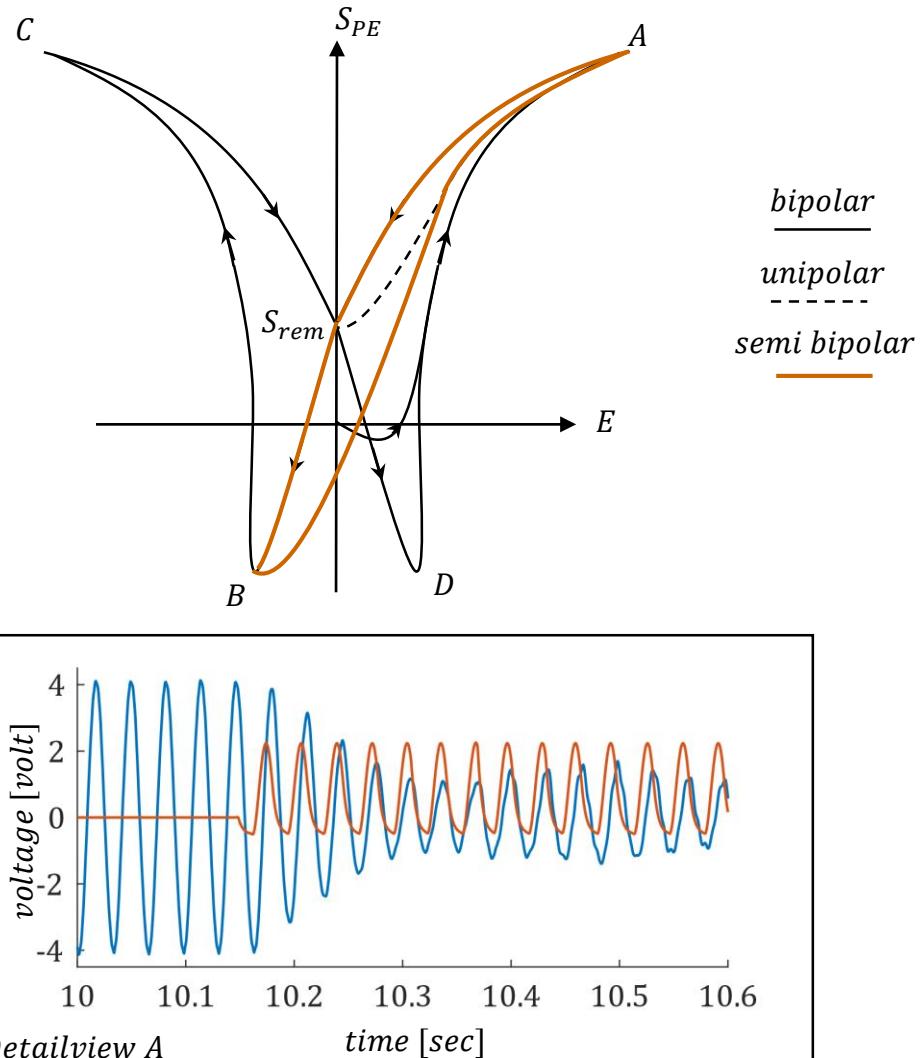
## Pre- Windtunnel tests



# Application of the methodology

## Test Setup

## Pre- Windtunnel tests

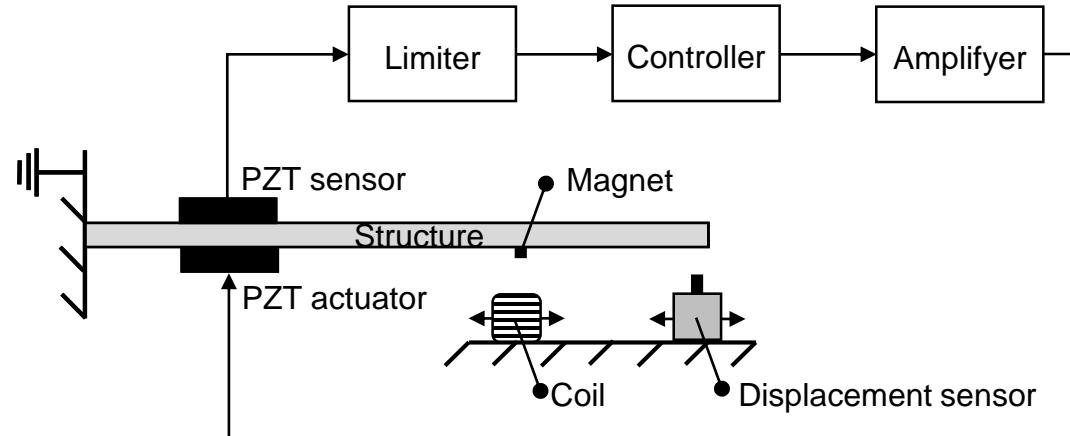


# Application of the methodology

## Test Setup

## Pre-Windtunnel tests

## Windtunnel test

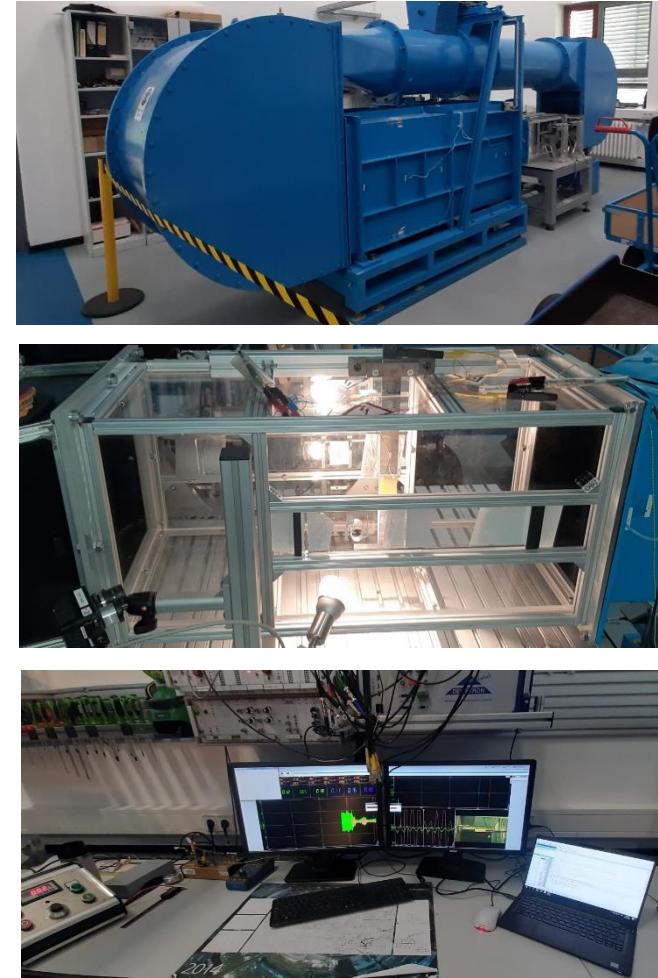
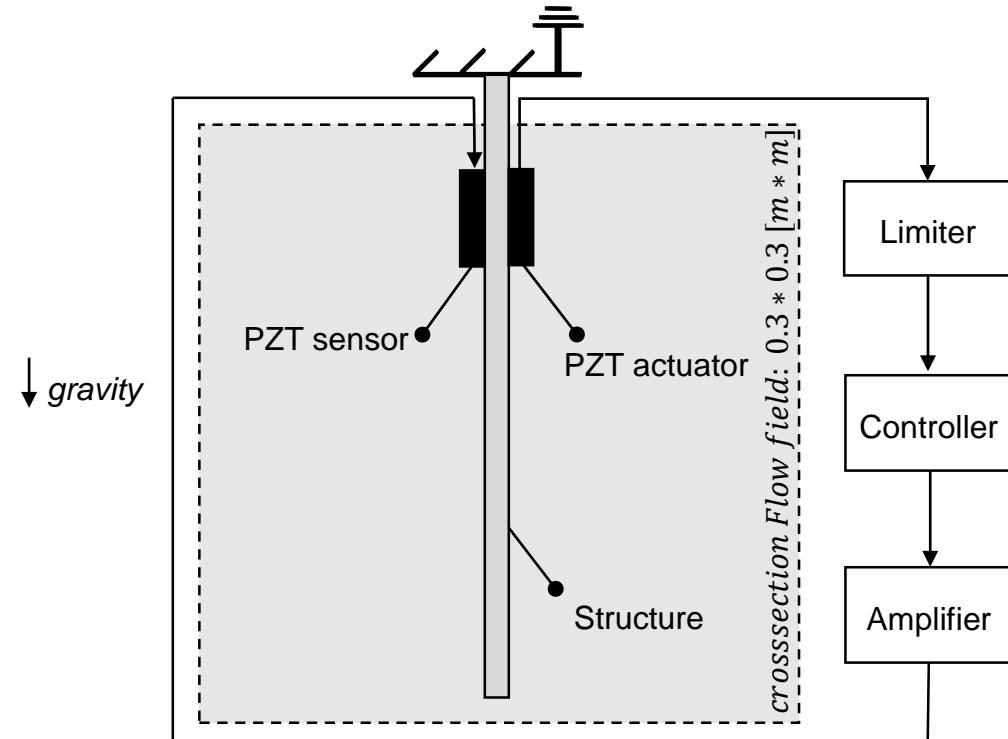


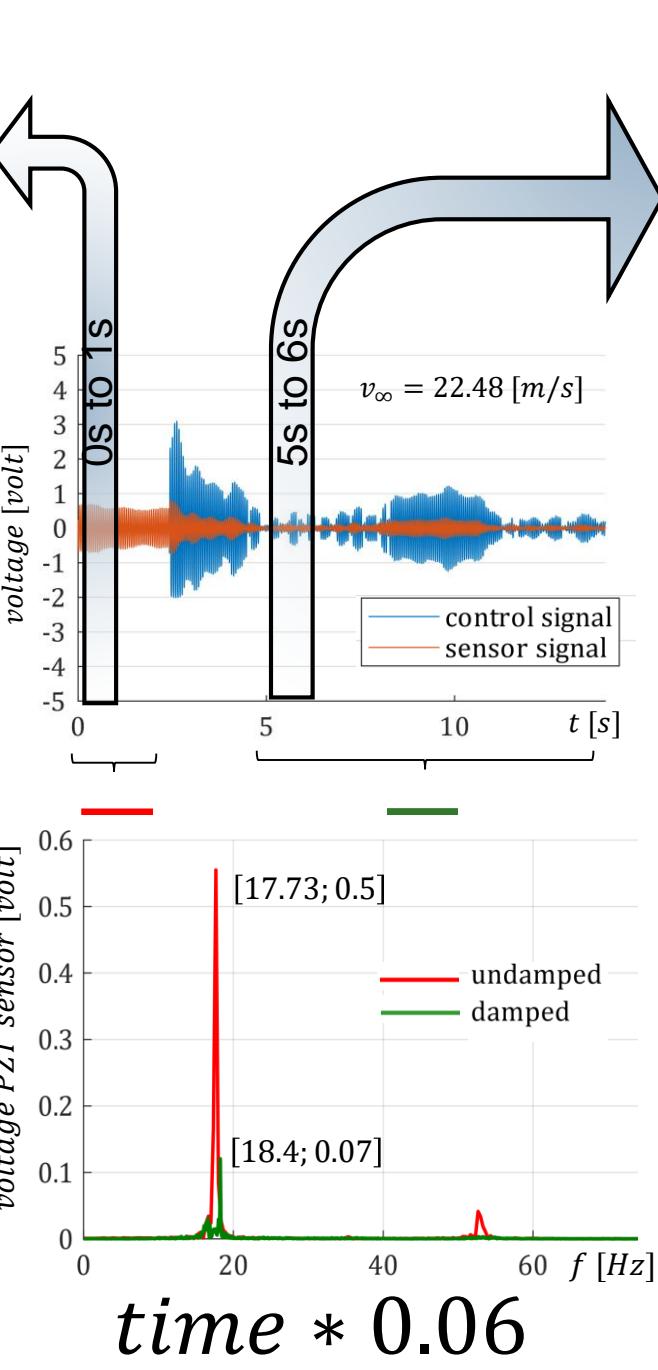
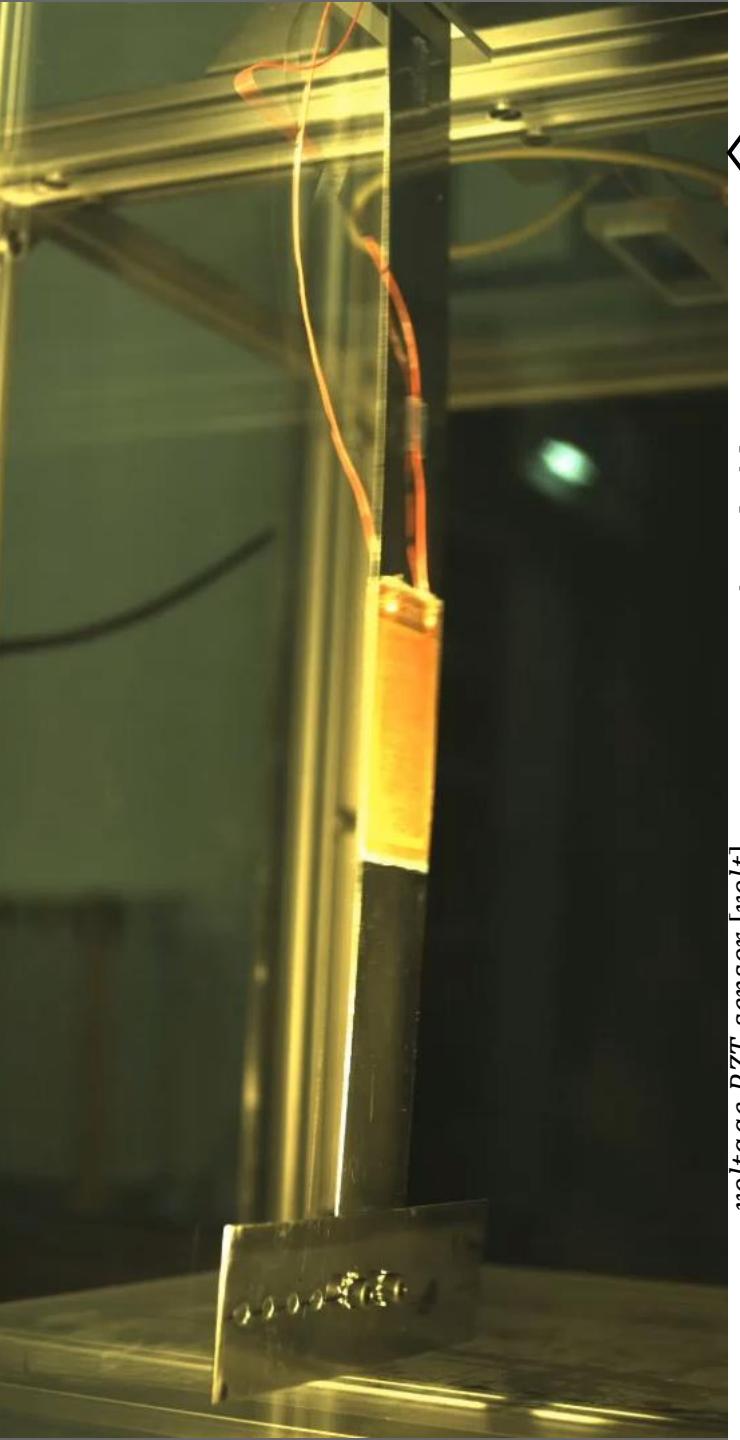
# Application of the methodology

## Test Setup

## Pre-Windtunnel tests

## Windtunnel test



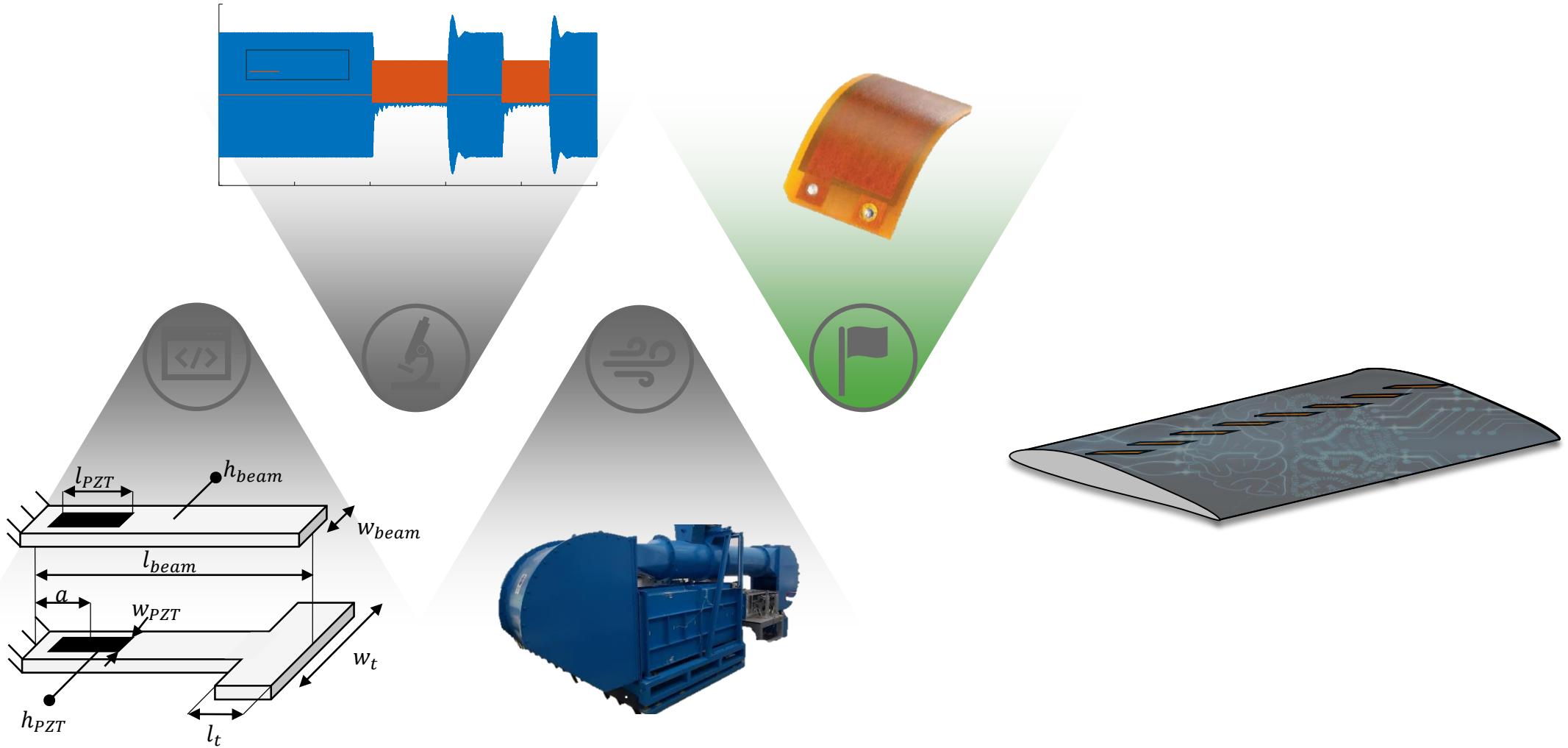


# Agenda



-  Investigation goals
-  Foundations
-  Methodology
-  Validation of the methodology
-  Application of the methodology
-  **Summary and Future application ideas**

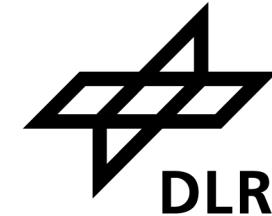
# Summary and Future application ideas



# Thank you for your attention!



**DLRK 2022**  
DEUTSCHER LUFT- UND  
RAUMFAHRTKONGRESS  
27. - 29. SEPTEMBER 2022 – DRESDEN  
„Luft- und Raumfahrt - gemeinsam forschen und nachhaltig gestalten“



**Institute of  
Aeroelasticity**

# Questions ?



AE @ [LinkedIn](#)

Anna Altkuckatz, Institute for Aeroelasticity, 29. Sep. 2022

**M. Sc. Anna Altkuckatz**

German Aerospace Center (DLR)

Institute of Aeroelasticity | Aeroelastic Experiments | Bunsenstr. 10 | 37073 Goettingen

Telephone: +49 (0)551-709-2752 | E-Mail: [Anna.Altkuckatz@dlr.de](mailto:Anna.Altkuckatz@dlr.de)



AE Homepage