

Momentum Predictability and Heat Accumulation in Laser-based Space Debris Removal

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German Aerospace Center (DLR), Institute of Technical Physics

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Tuesday, March 27



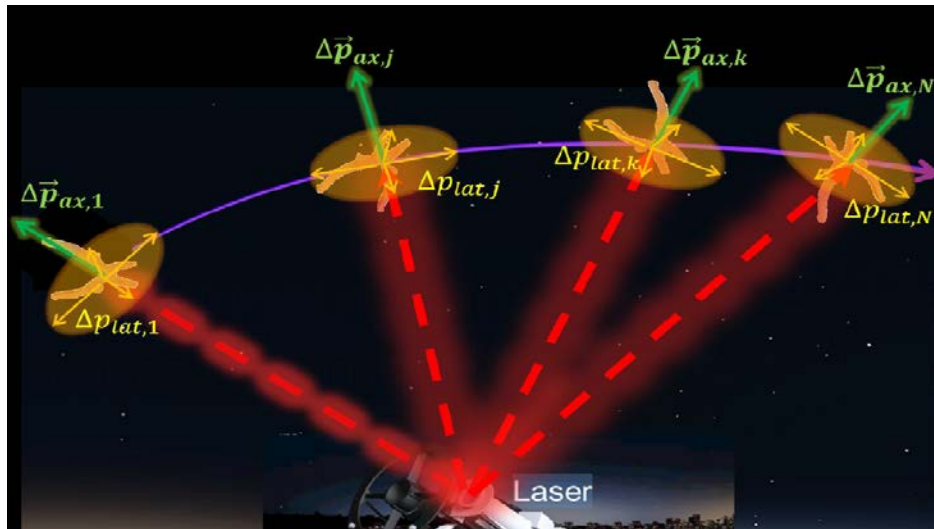
Knowledge for Tomorrow



Motivation

Momentum Scatter

- Irregularly shaped targets
- Random target orientation
- Unknown target material



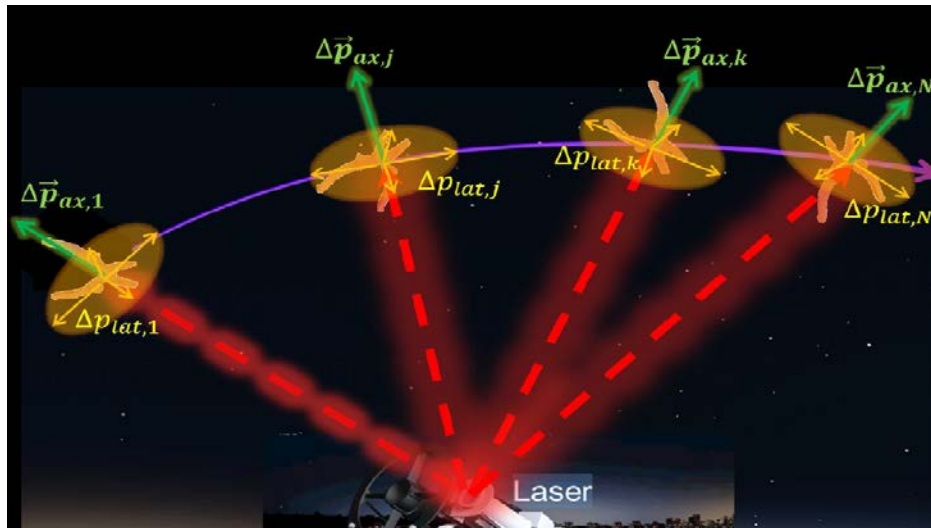
Impulse components in repetitive laser irradiation



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Impulse components in repetitive laser irradiation

Heat Accumulation

- Thermal stress
- Droplet ejection
- Target Melting



Molten aluminum target after repetitive laser irradiation



Thermal constraints ...

Heat Accumulation in Laser Ablation

- Residual heat for metals: $\eta_{res} = \frac{Q_{heat}}{E_L} \approx 15 \dots 25 \%$



Thermal constraints ...

Heat Accumulation in Laser Ablation

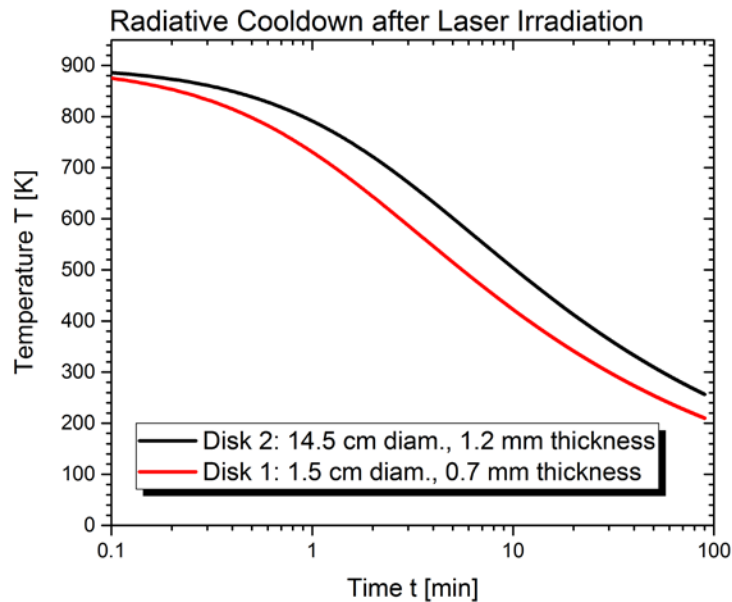
- Residual heat for metals: $\eta_{res} = \frac{Q_{heat}}{E_L} \approx 15 \dots 25 \%$
- Almost neglected in debris removal research
- Adressed in: Schall, Acta Astronaut. **24**: 343 (1991)
- Melting of flat targets: „Debris Compactor“



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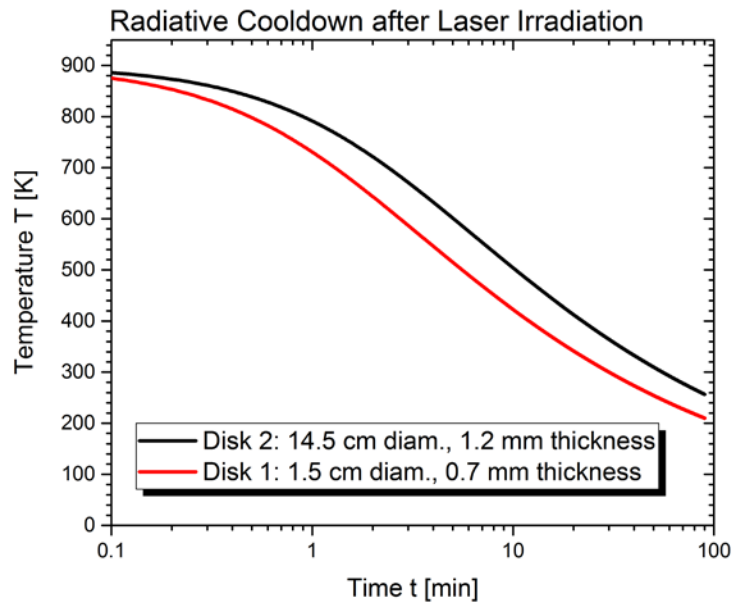
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Thermo-Mechanical Coupling Coefficient c_{tm}

- How much momentum can be transferred, taking into account for the residual heat?

$$c_{tm} = \frac{\Delta p}{Q_{heat}} \left(= \frac{\Delta p}{\eta_{res} E_L} = \frac{c_m}{\eta_{res}} \right)$$

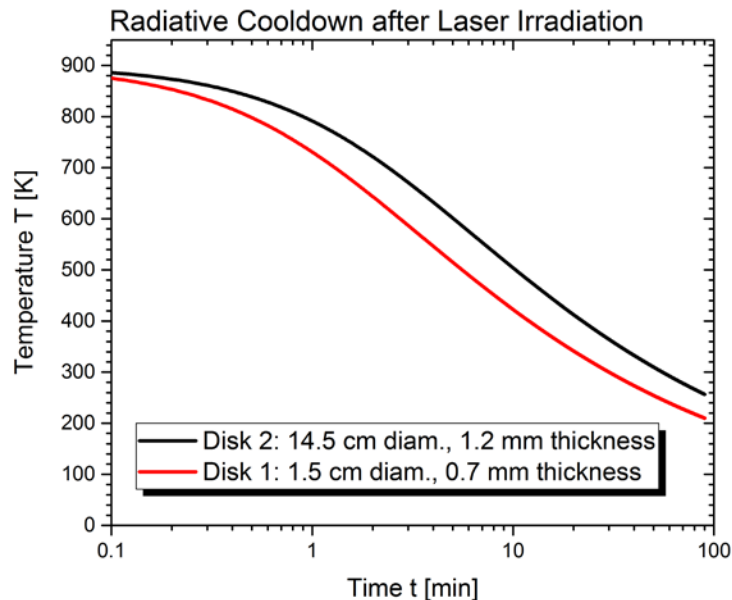
Scharring et al.,
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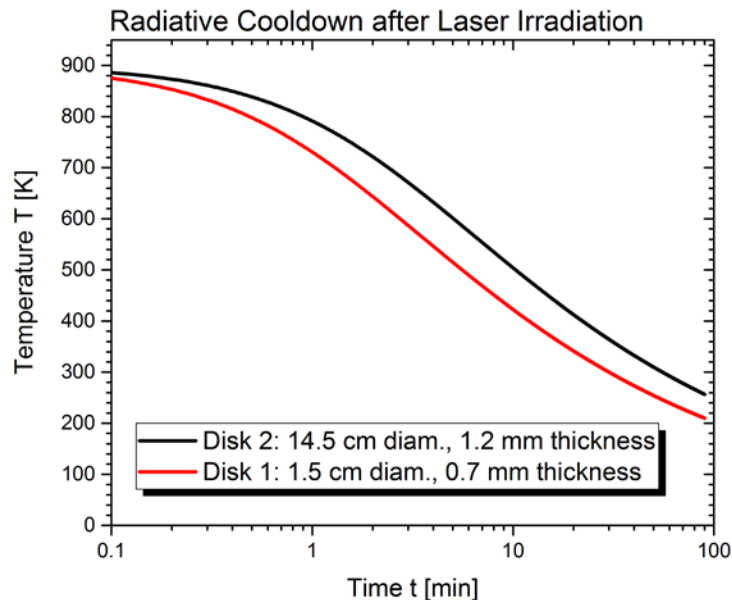
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- Maximum momentum transfer:

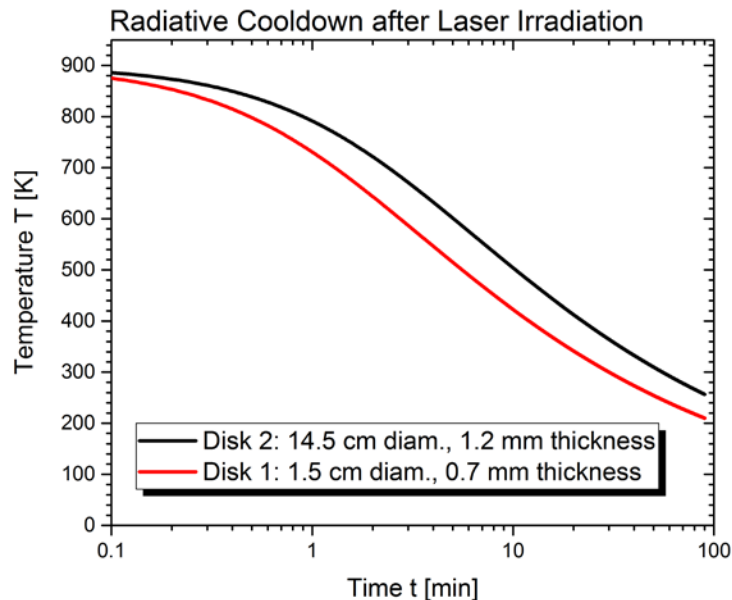
$$\Delta p_{max} = c_{tm} \cdot c_p \cdot m \cdot (T_m - T_0)$$



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- Maximum velocity increment:

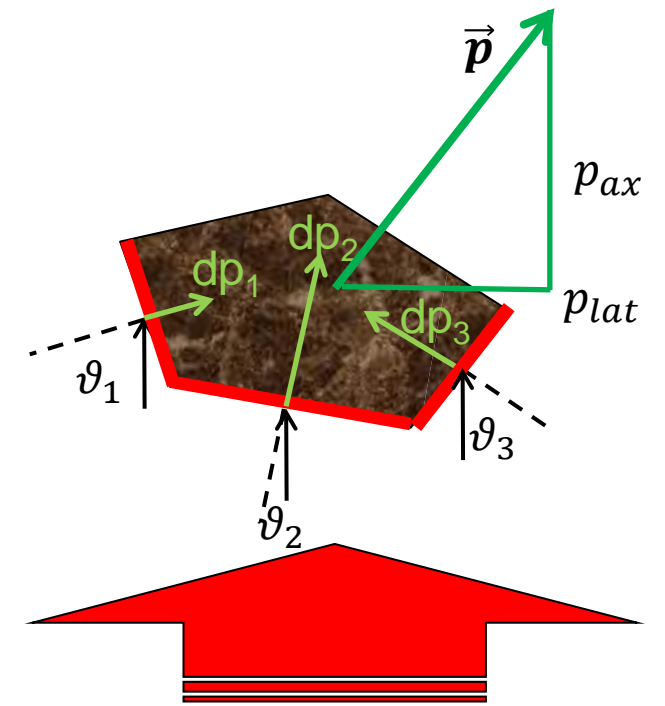
$$\Delta v_{max} = \frac{c_m}{\eta_{res}} \cdot c_p \cdot (T_m - T_0)$$



... and Momentum Prediction

Area-matrix concept $\vec{p} = c_m \Phi_L \vec{k} \cdot \underline{G}$

Liedahl et al., *Adv. Space Res.* 52(5): 895 – 915 (2013)



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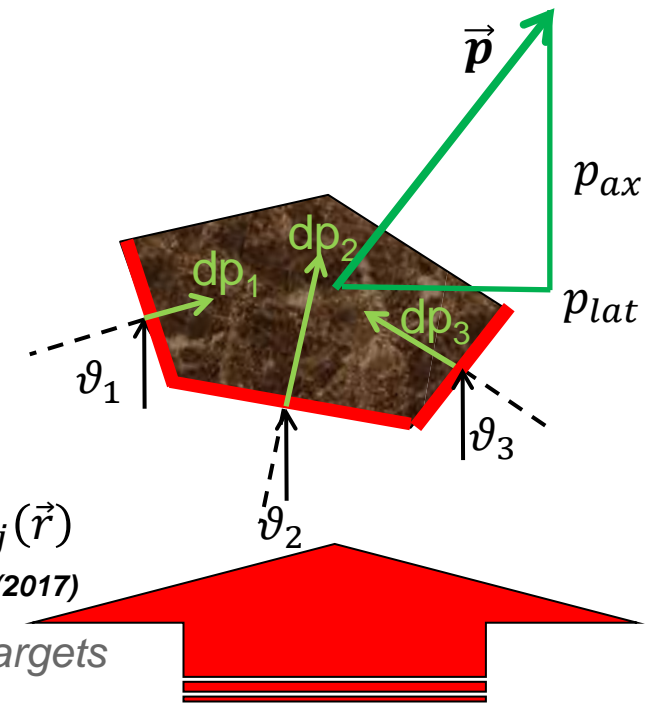
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EXPEDIT

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EXamination Program for irrEgularly shaped debris Targets



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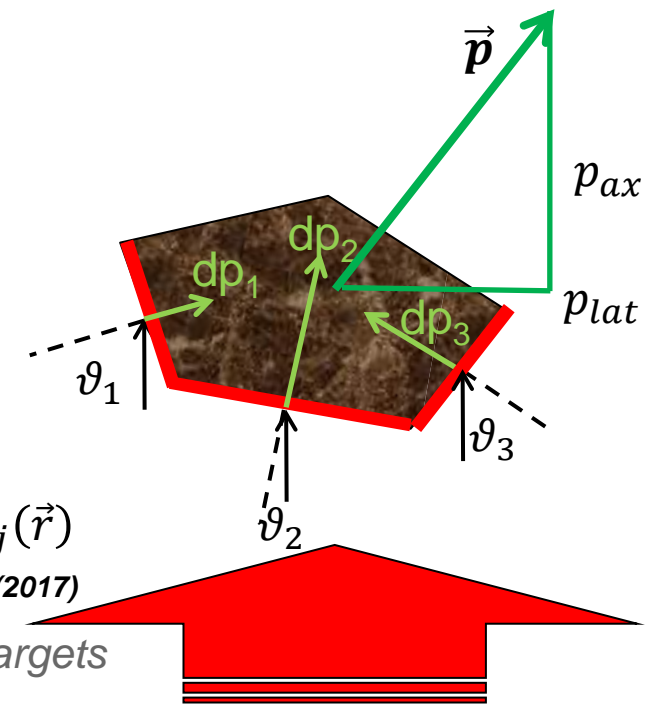
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Discretization of **Laser** $\Phi = \Phi(\vec{r})$

Raytracing of Gaussian beam profile: Nvidia Optix, GPU

Discretization of **Matter**

Finite surface elements (obj files)

Discretization of **Interaction**

Parameter dependencies of $c_m(\Phi)$, $\eta_{res}(\Phi)$

Programming language: C++

Python wrapper for API: Monte Carlo studies, Orbital propagation



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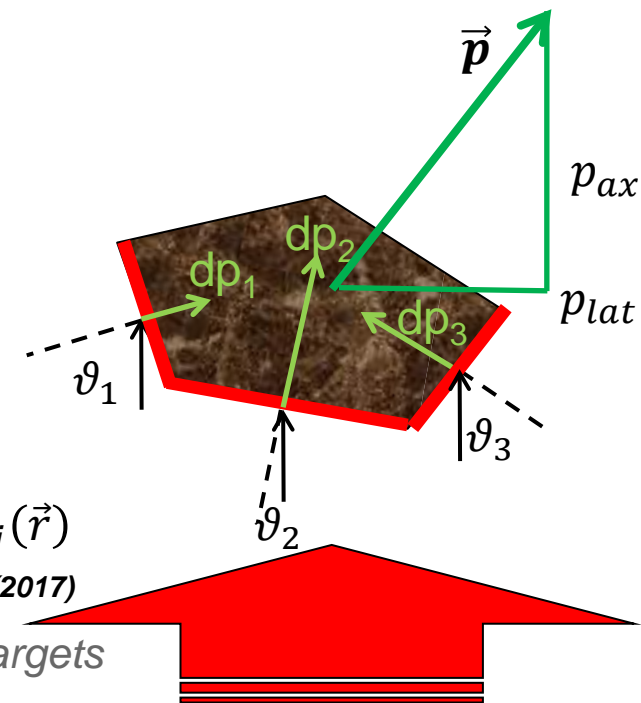
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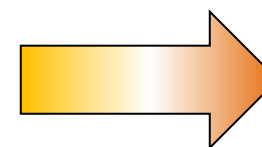
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$c_m(\Phi(\vec{r}))$
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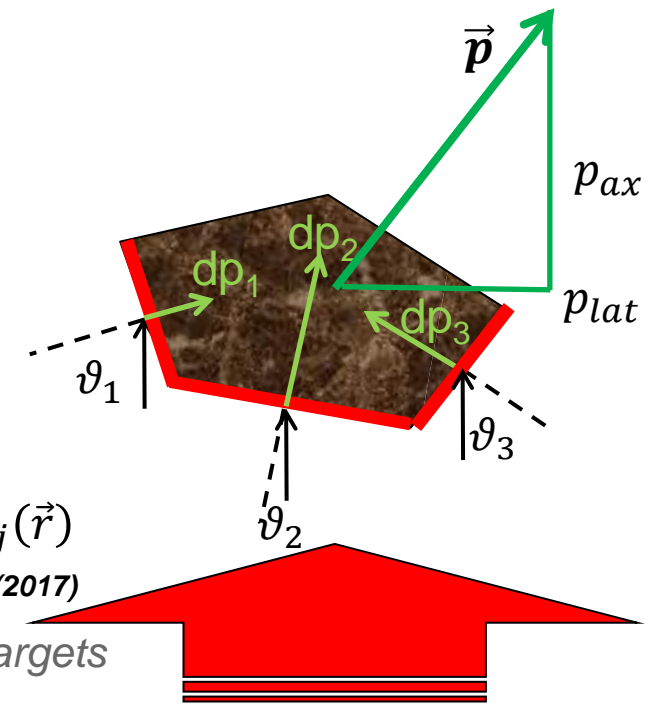
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$$c_m(\Phi(\vec{r}))$$

$$\eta_{res}(\Phi(\vec{r}))$$



Local momentum density on the surface of an irregularly shaped target. Cow model courtesy of NVidia.



Monte Carlo Study Design: Baseline Setup

Parameters

- Laser: CLEANSPACE concept

B. Esmiller et al., Appl. Opt. 53(31): 145-154 (2014)

- Pulse energy: $E_L = 25 \text{ kJ}$
- Pulse duration: $\tau = 10 \text{ ns}$
- Wavelength: $\lambda = 1064 \text{ nm}$
- Spot diameter ($1/e^2$): $d_{spot} = 66.7 \text{ cm}$
- Mean fluence: $\langle \Phi \rangle = 7.2 \text{ J/cm}^2$

- Beam Discretization:

- 0.1 mm resolution

- Monte Carlo:

- Random target orientation
- 2000 sample shots / target
- Beam center = Target CMS

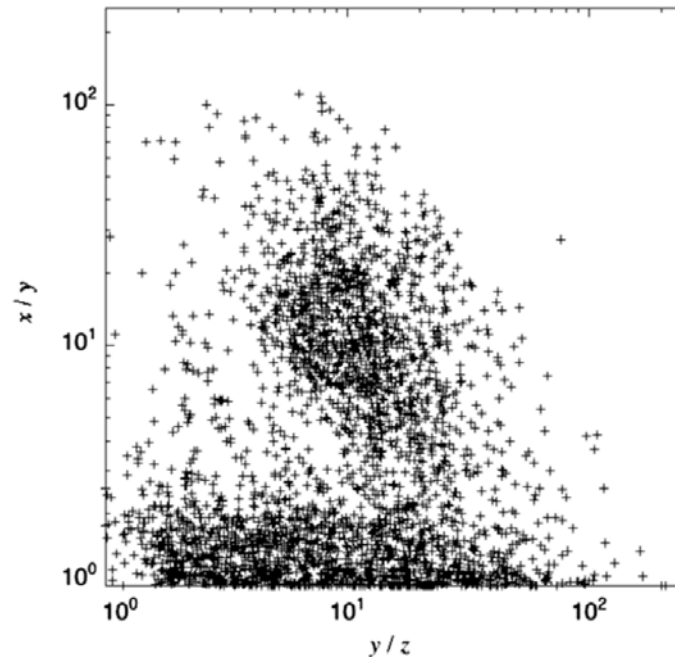


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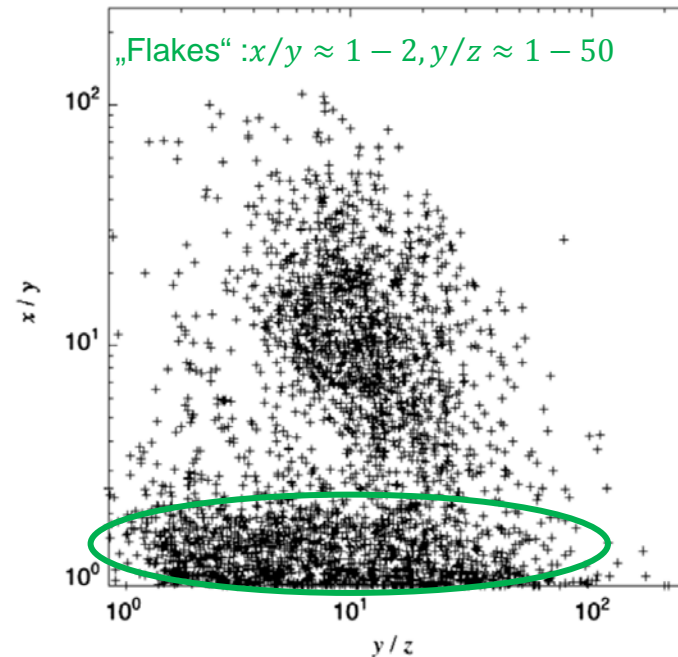


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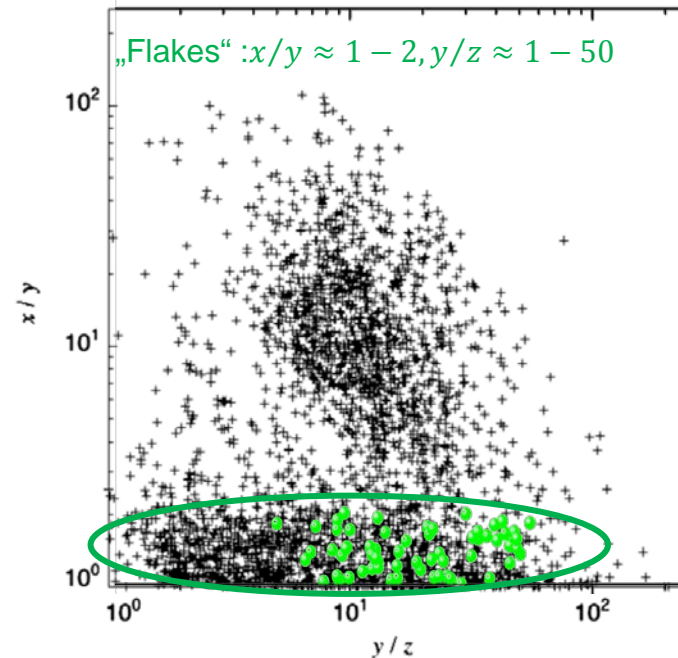
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Targets

- 100, randomly generated
- Flake-like ellipsoids
- Material: aluminium



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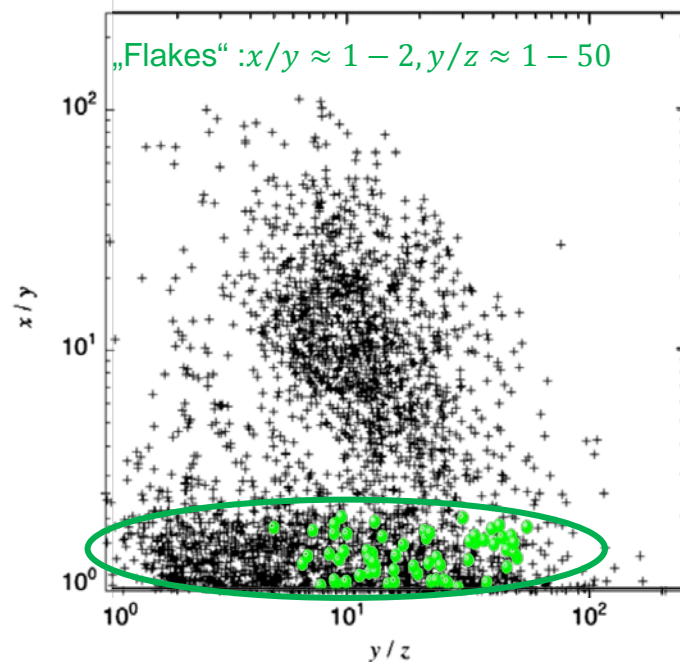
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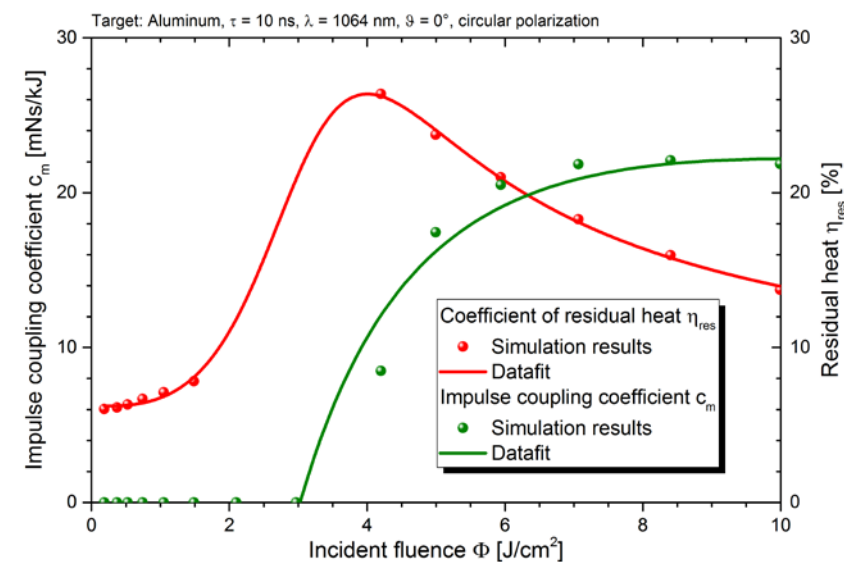
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Laser-matter Interaction

- Results from HD simulations (Polly-2T*)
- Datafit parameters → Expedit simulation



*Polly-2T code courtesy of M. Povarnitsyn, RAS Moscow.



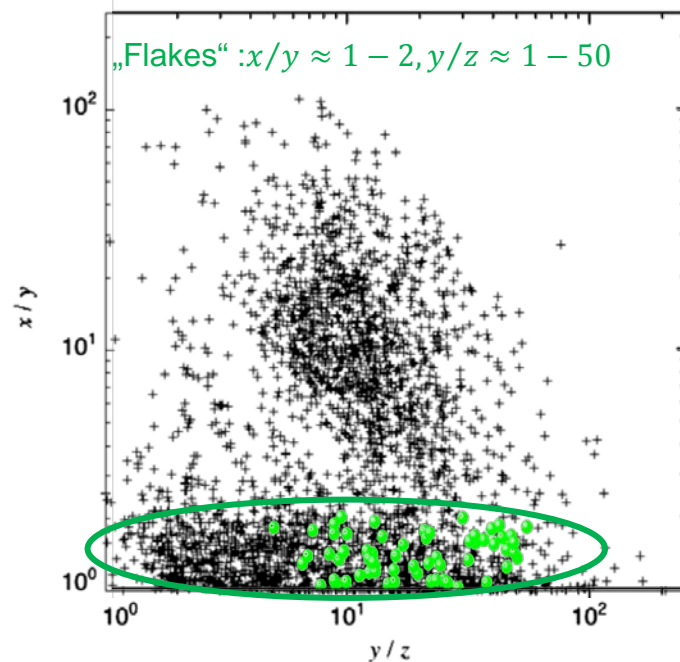
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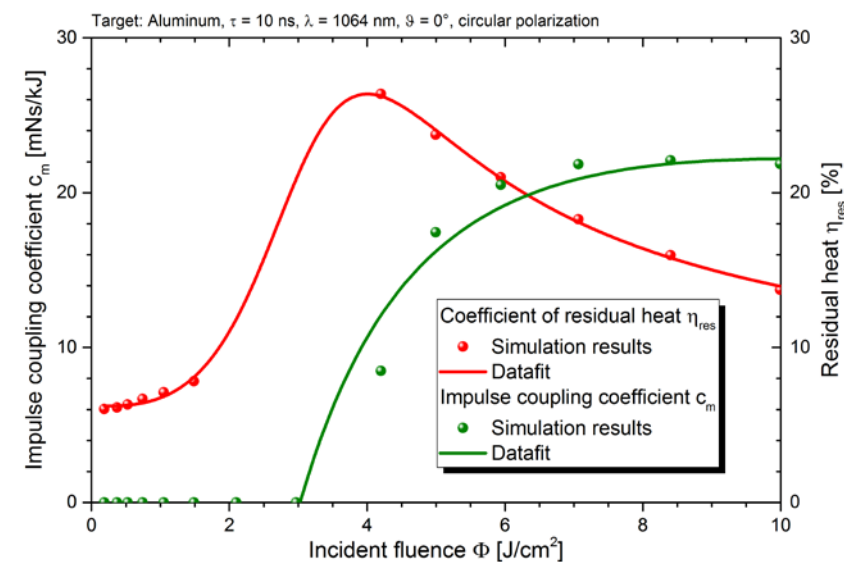
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$$c_m[mNs/kJ](\Phi) \approx \frac{\Phi - \Phi_0}{a + (\Phi - \Phi_0)} \cdot b \cdot 12.46 \cdot A^{7/16} \cdot \left(\frac{\sqrt{\tau}}{\lambda \cdot \Phi [J/cm^2]} \right)^c$$

$(\Phi > \Phi_0)$

$$\eta_{res}(\Phi) \approx \frac{a_0 + a_1 \cdot \Phi + a_2 \cdot \Phi^2}{1 + a_3 \cdot \Phi + a_4 \cdot \Phi^2 + a_5 \cdot \Phi^3}$$

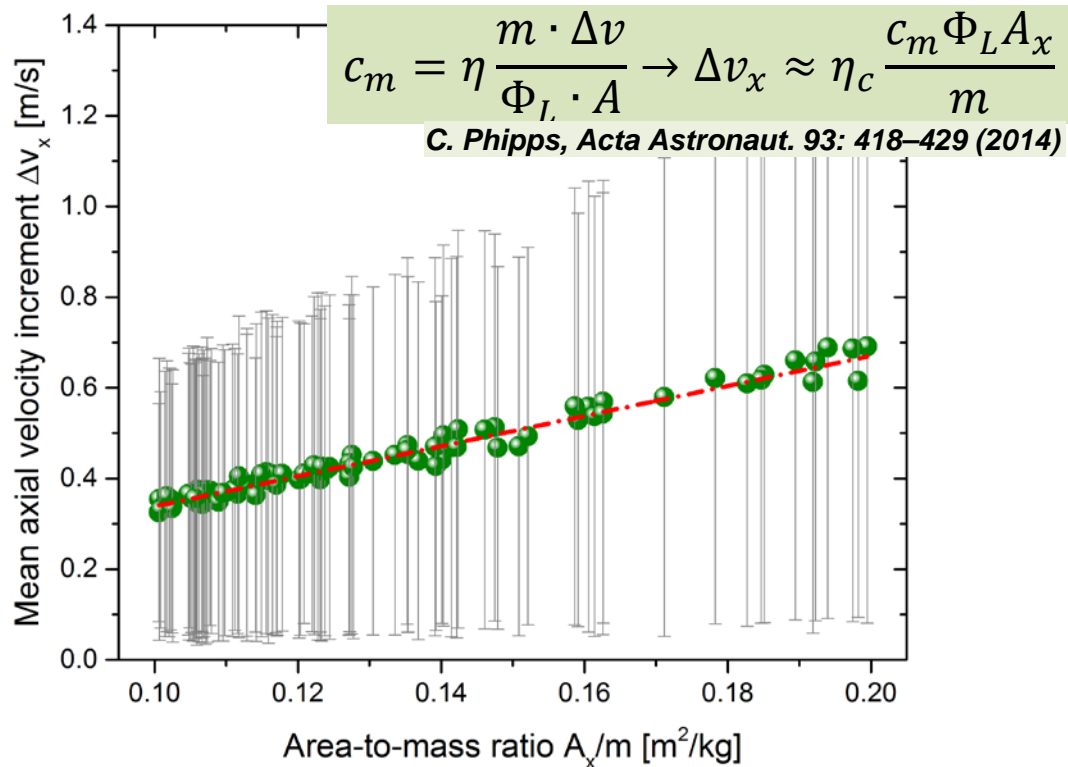


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- Gaussian laser spot profile

Monte Carlo Study: Random Target Orientation

Velocity Increment Δv



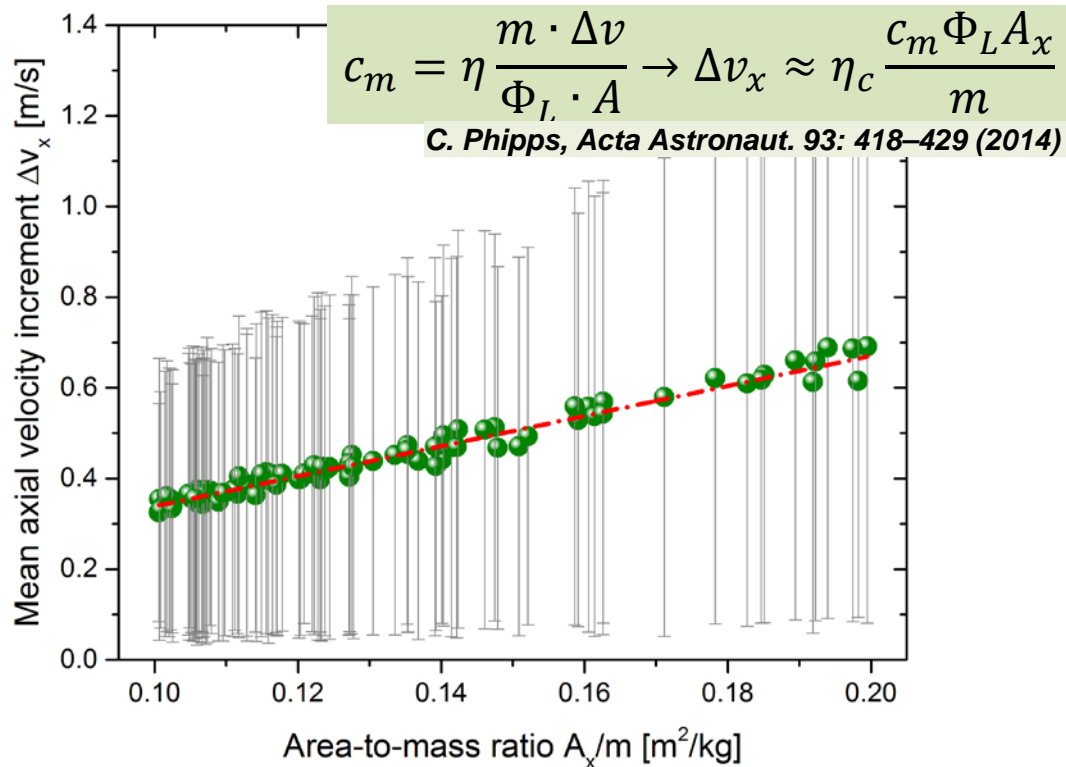
- Consideration of large momentum scatter necessary
- Collision analysis for conceivable trajectories required



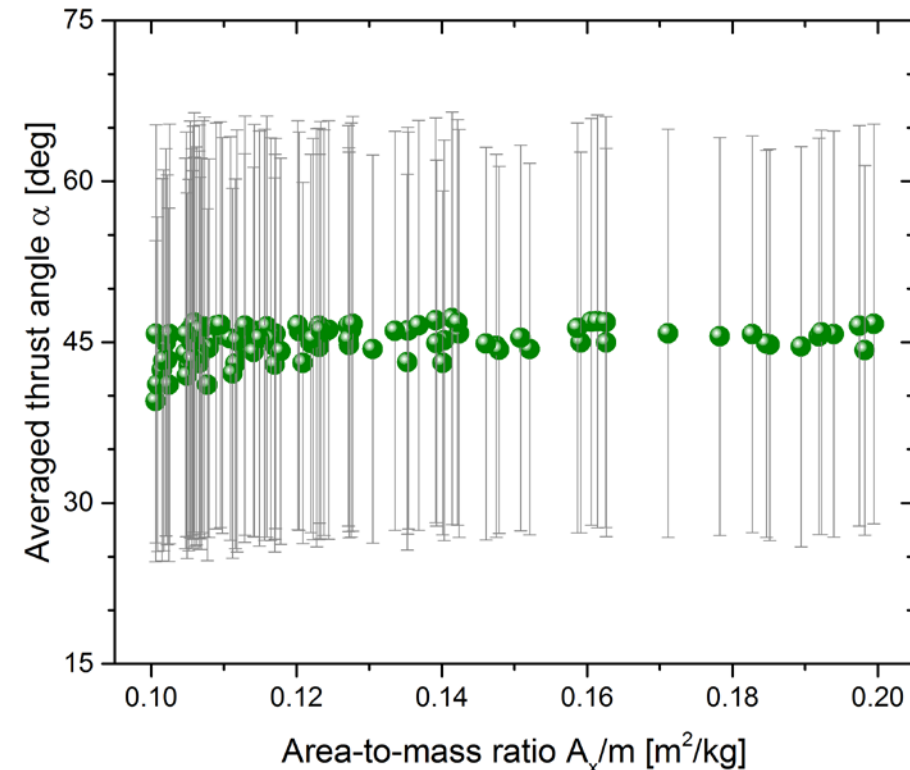
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Monte Carlo Study: Random Target Orientation

Velocity Increment Δv



Mean thrust angle



→ Consideration of large momentum scatter necessary

→ Collision analysis for conceivable trajectories required

→ Large thrust angle yields significant losses in Δv_x .

→ Lateral momentum might cancel out in multi-pulse irradiation.

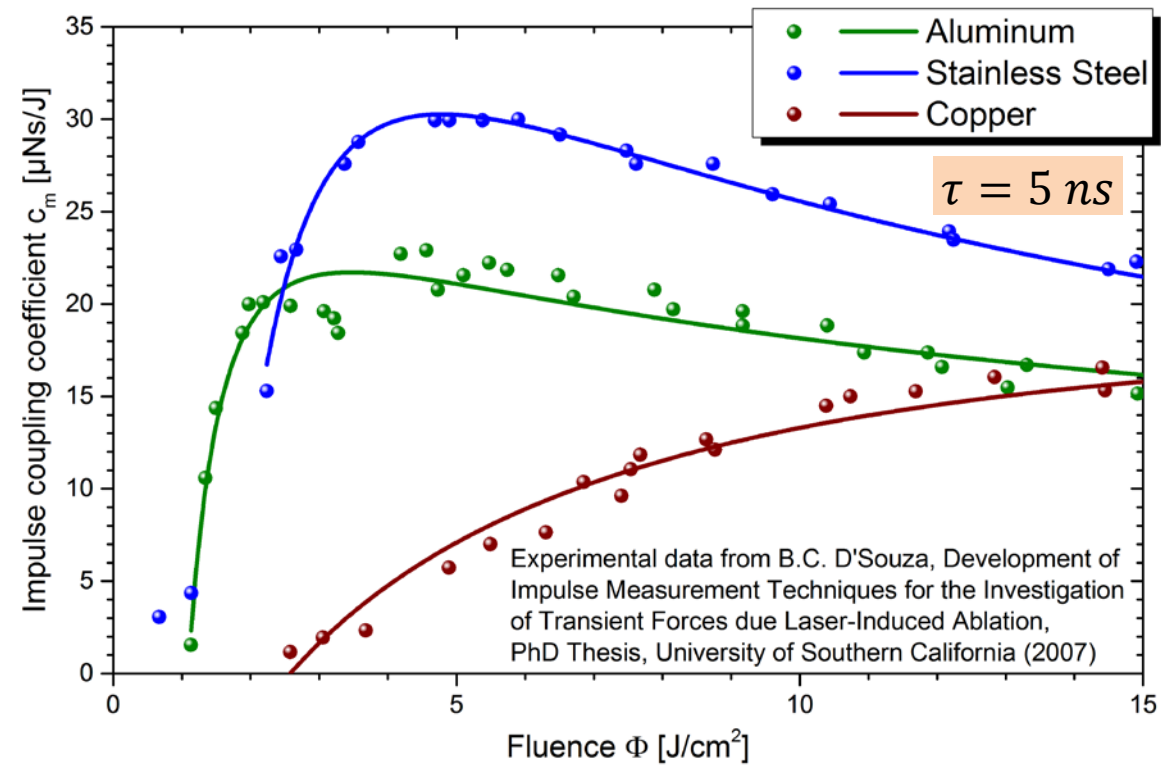


Simulation setup (3 DOF)

- Target CMS = beam center
- Random target orientation
- **Target material: Al, Steel, Cu**

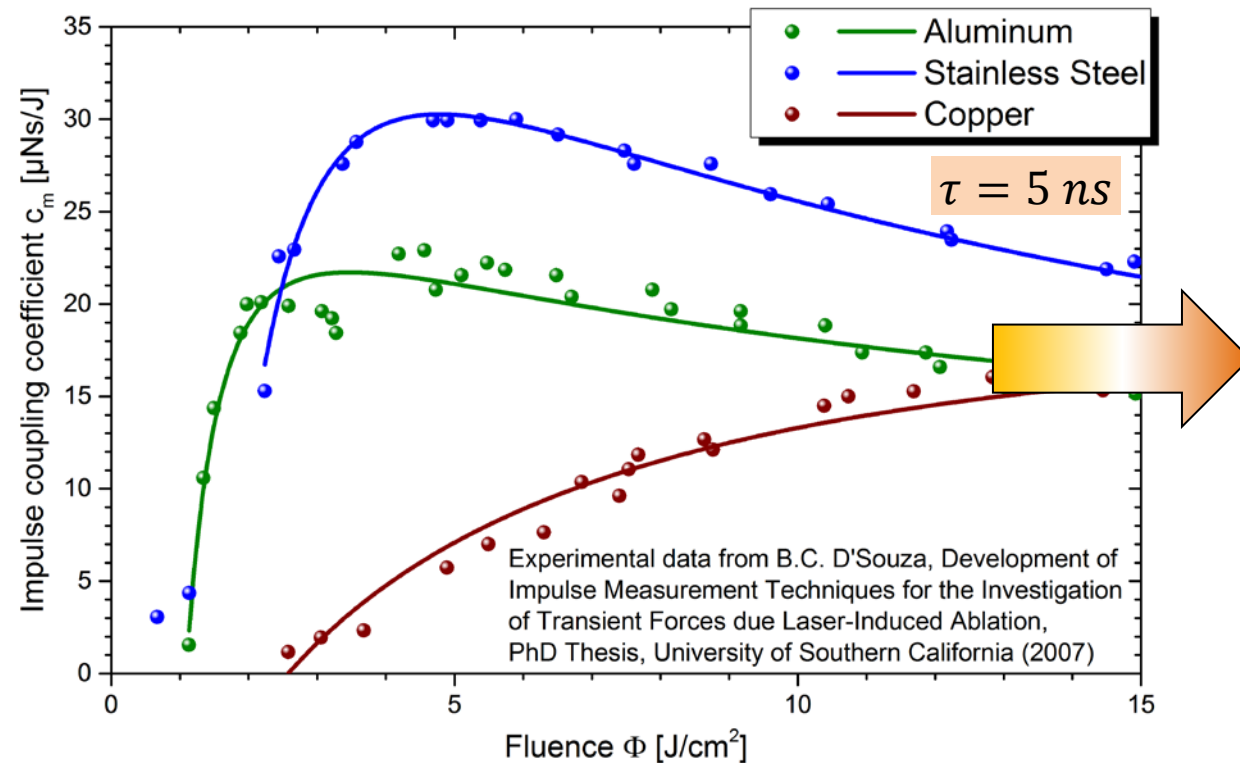
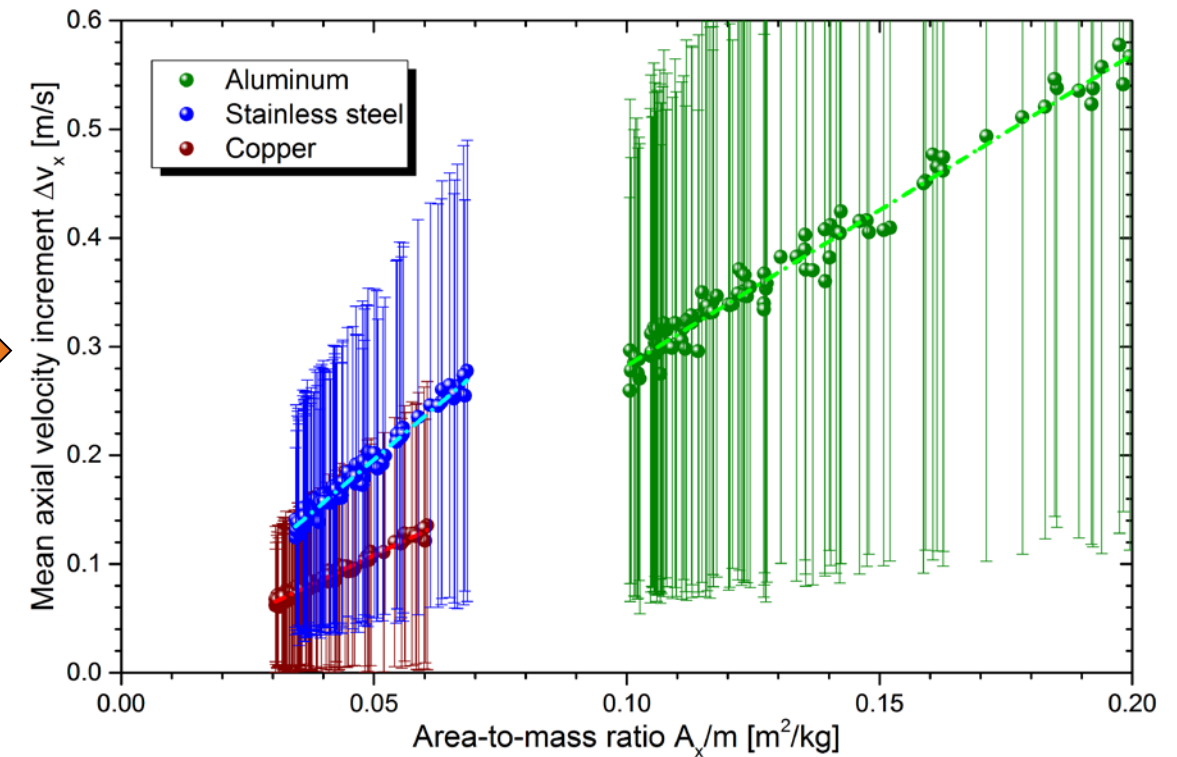
Various Target Materials

Impulse Coupling Characteristics $c_m(\Phi)$



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Various Target Materials**Impulse Coupling Characteristics $c_m(\Phi)$** **Velocity Increment Δv** 

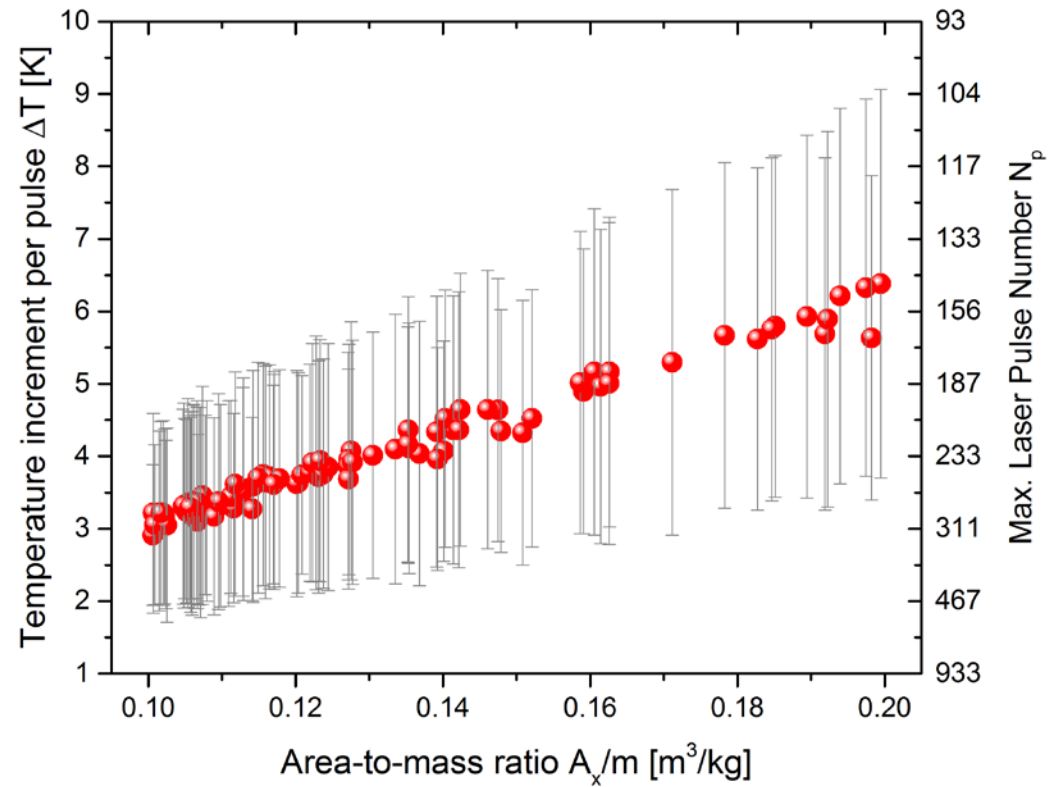
→ Remote material reconnaissance advisable for precise orbit modification



- Target CMS = beam center
- Random target orientation
- Target: Aluminum

Thermo-Mechanical Coupling

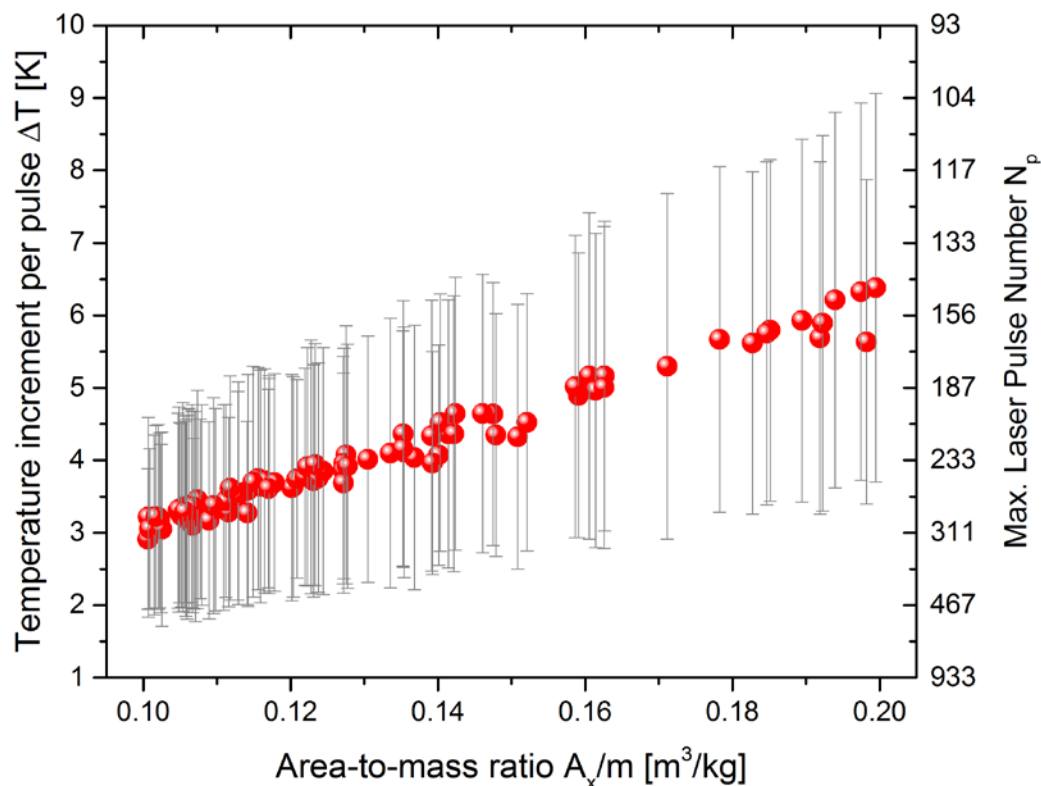
Heating



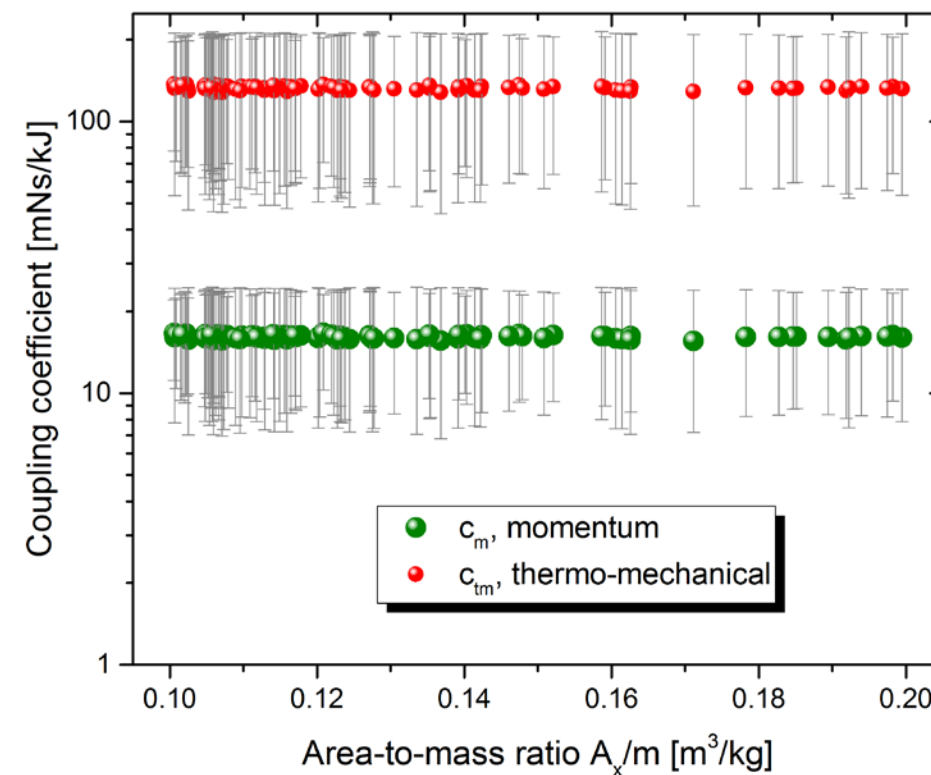
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Thermo-Mechanical Coupling

Heating



(Thermo-)mechanical Coupling



→ Safe Debris Removal requires strong limitation laser pulse number.

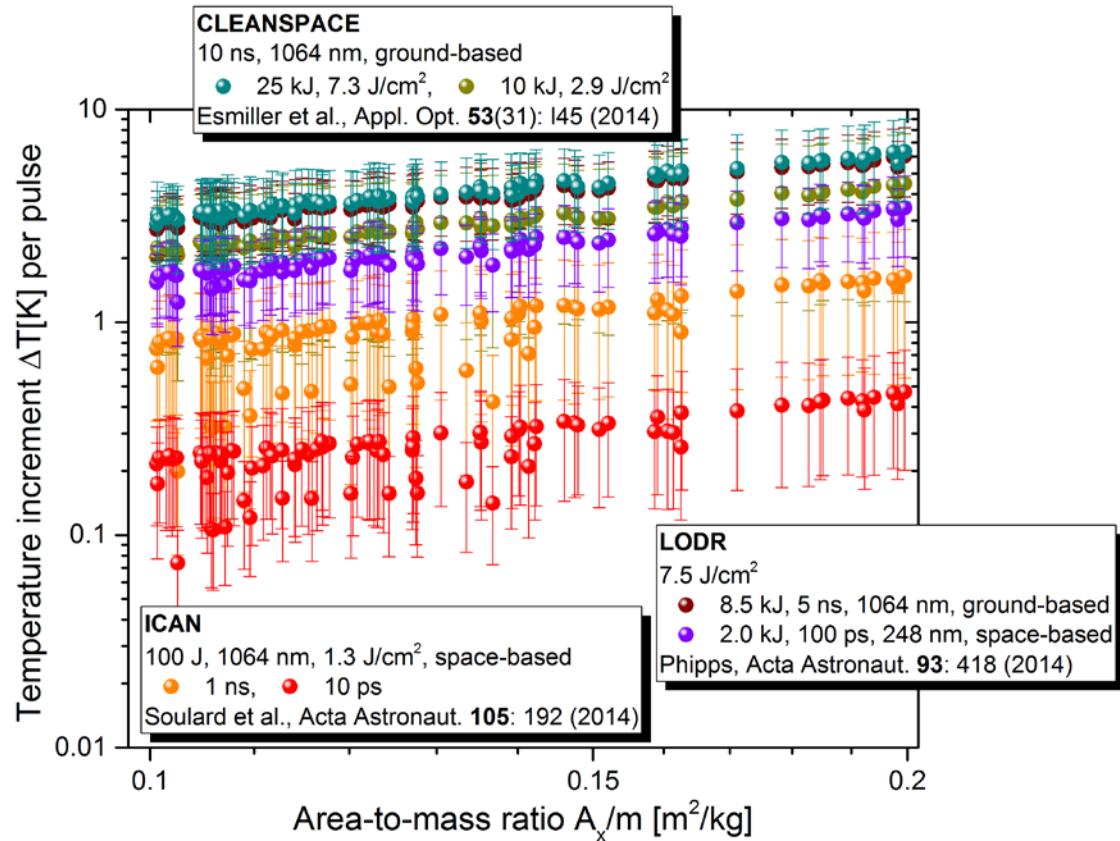
→ *CLEANSACE, AI: max. 100 laser pulses during one transit*



- Various laser configurations
- $c_m(\Phi), \eta_{res}(\Phi)$ *from simulations*
- Target: **Aluminum**

Various Laser Configurations

Single Pulse Characteristics

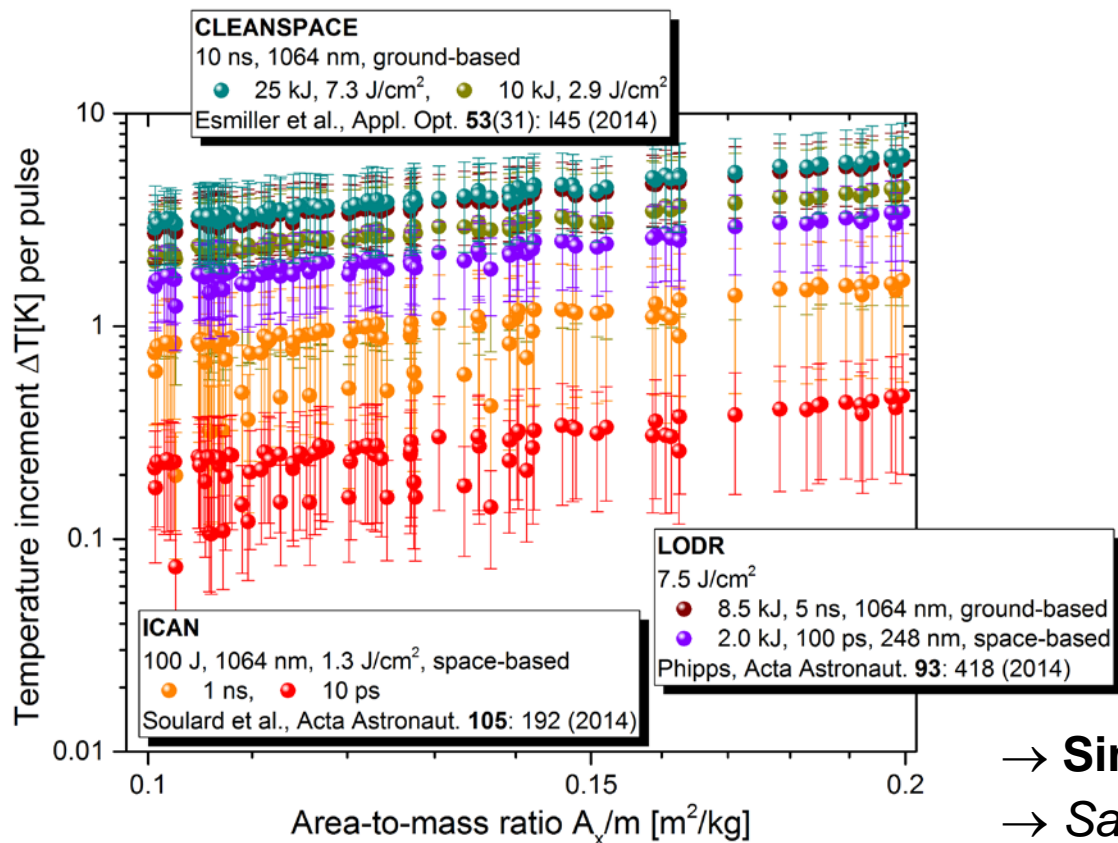


Various Laser Configurations

Simulation setup

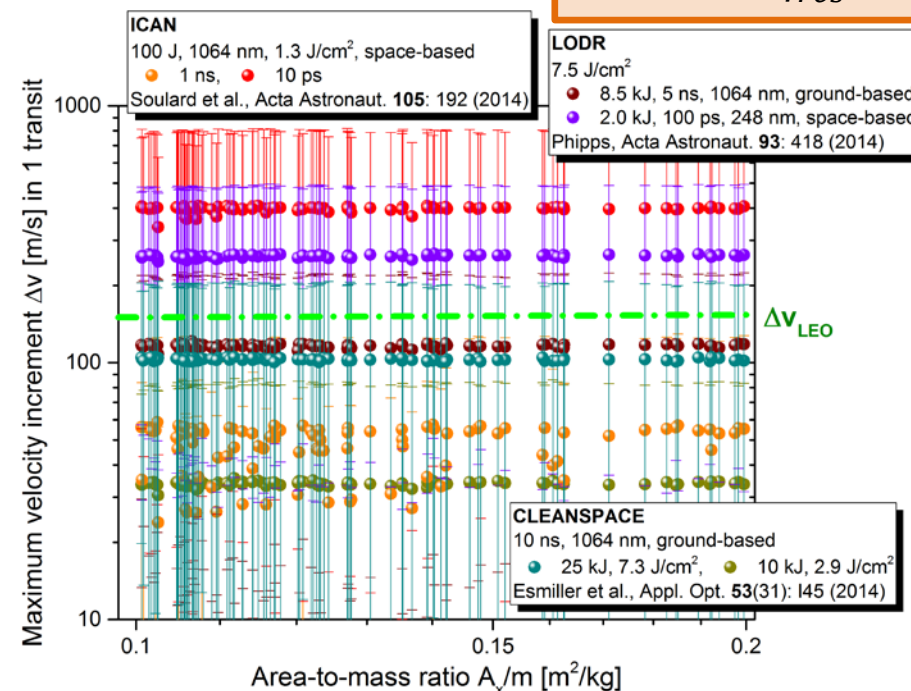
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Single Pulse Characteristics



Multi-pulse Limitations

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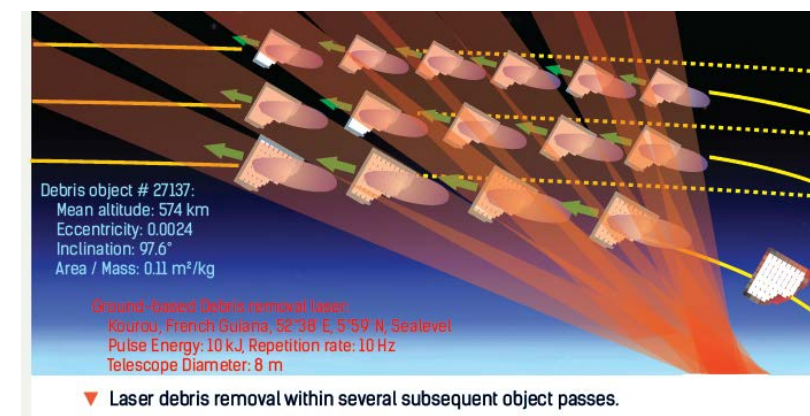
- **Single transit removal might work for rather short pulses.**
- *Safety margins for initial temperature and melting needed*
- *Accumulation of mechanical stress in ultrashort pulse trains?*



Conclusions

Momentum Predictability

- Discretization of Area Matrix approach with CUDA-parallelized C++ code *Expedit* on GPU
- Large scatter in Δv
- Material reconnaissance for Δv prediction
- Pulse number limitation within one transit:
 - Moderate absolute prediction error in Δv
 - lower Rep-rates / average power needed



B. Esmiller et al., HPLA-BEP 2014



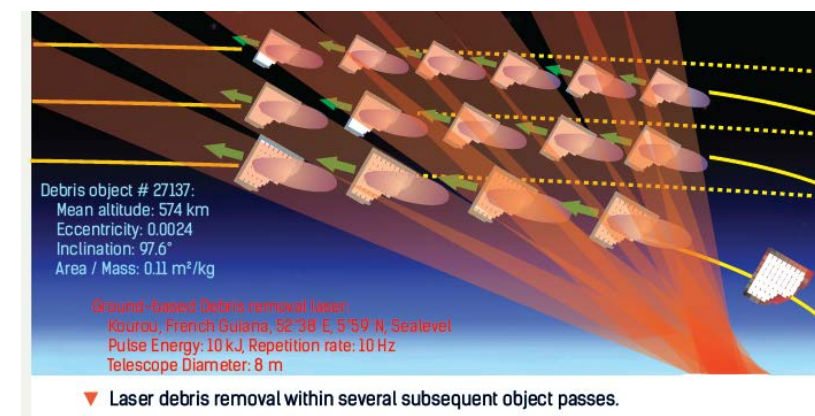
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Outlook

→ Poster Session: R.-A. Lorbeer et al., Laser-Based Space Debris Removal – Laser-Induced Momentum Generation on True Scale Debris-Like Targets



B. Esmiller et al., HPLA-BEP 2014



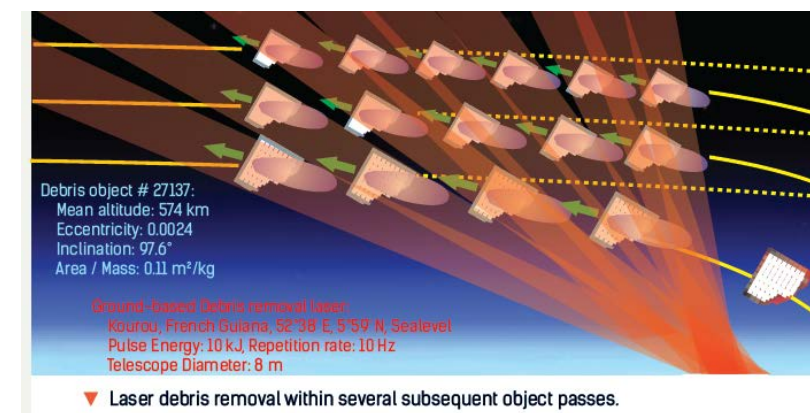
Conclusions

Momentum Predictability

- Discretization of Area Matrix approach with CUDA-parallelized C++ code *Expedit* on GPU
- Large scatter in Δv
- Material reconnaissance for Δv prediction
- Pulse number limitation within one transit:
 - Moderate absolute prediction error in Δv
 - lower Rep-rates / average power needed

Outlook

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B. Esmiller et al., HPLA-BEP 2014

Heat Accumulation

- Discretized Add-on to *Expedit* based on HD simulation data
- Temperature increment per pulse: up to $\Delta T \approx 5K$
- Material reconnaissance for ΔT prediction
- Pulse number limitation within one transit:
 - Avoidance of target melting
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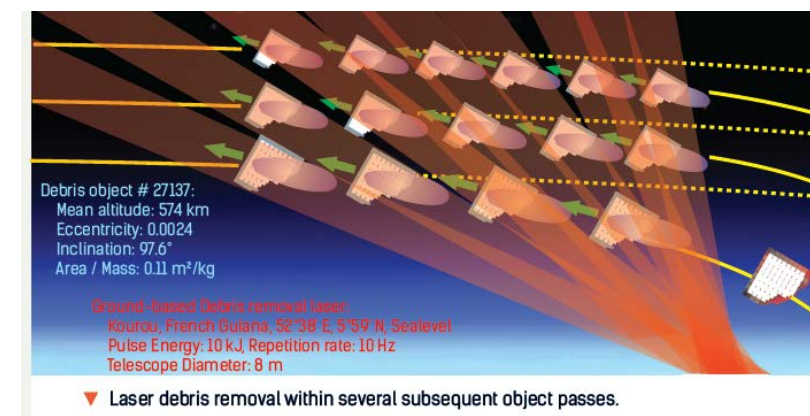
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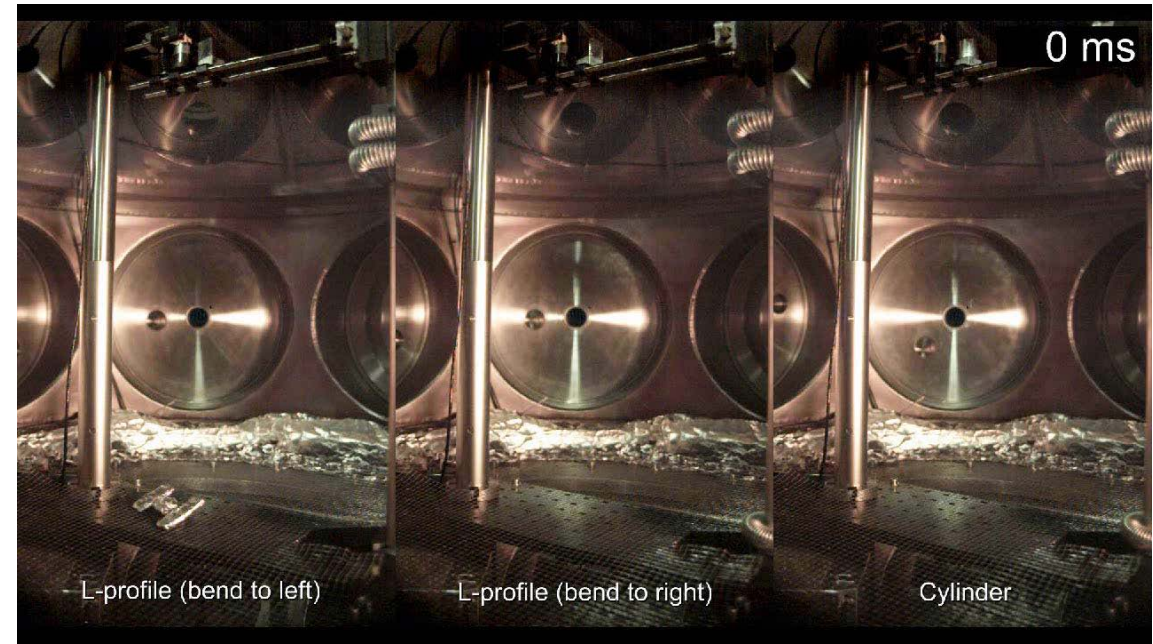
- **Experimental data** needed on:
 - $c_m(\Phi, T)$: temperature-dependent momentum coupling
 - $\eta_{res}(\Phi, T)$: heat (and stress) accumulation



Thank you for your kind attention



„Space debris,“ Finnegan, 7 years



Drop experiments with irregularly shaped targets → Poster Session



Knowledge for Tomorrow

Q&A Backup Slides



Knowledge for Tomorrow



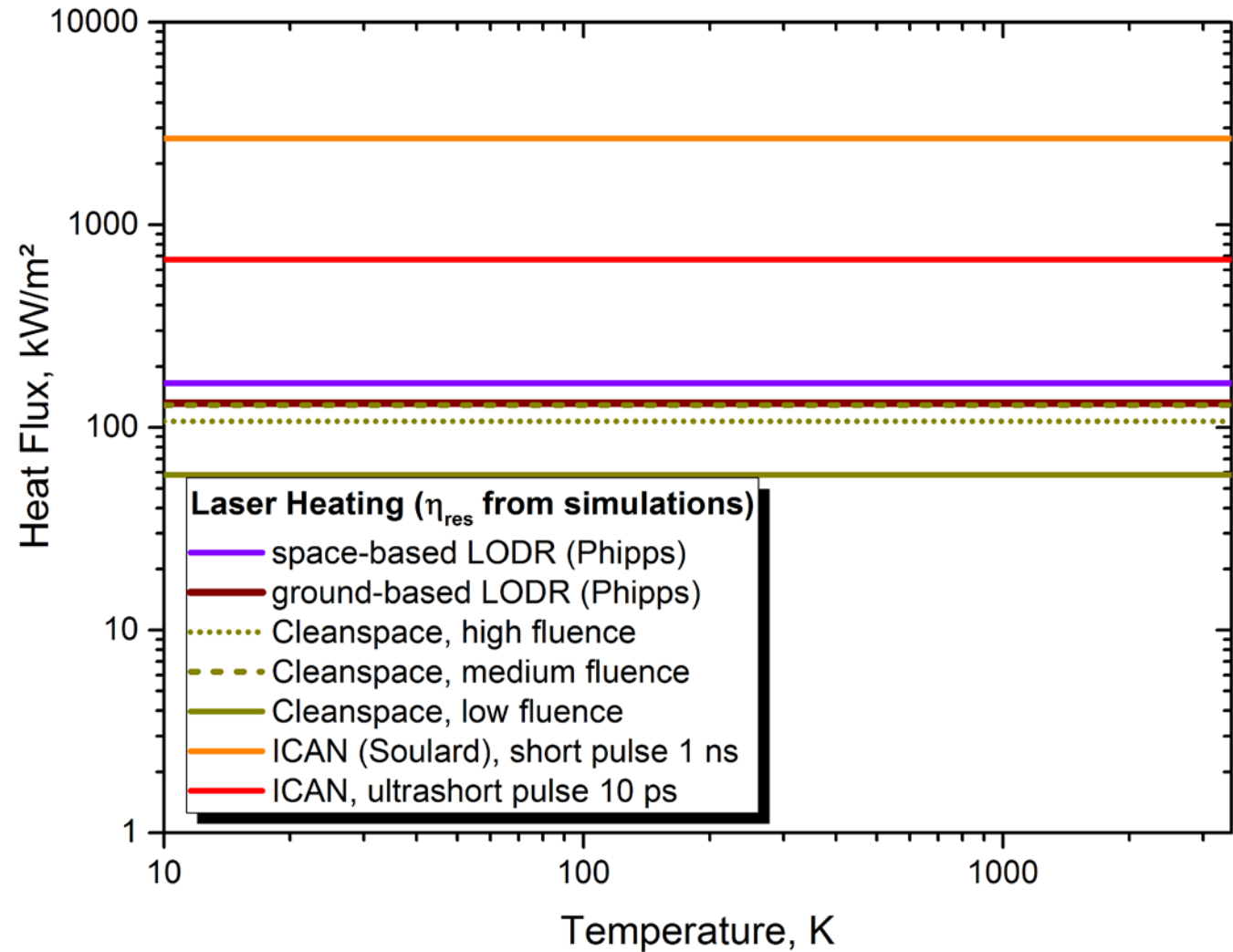
Literature Data on Residual Heat in Laser Ablation

τ	λ [μm]	f_{rep}	Mat.	η_{res} [%]	Ref.
1-6 μs	10.6	(1 pulse)	Al	10 – 40	Autric, Proc. SPIE 3343 : 354 (HPLA I, 1998)
120 ns	1.064	(1 pulse)	Al	35	Lenk et al., Appl. Surf. Sce. 109/110 : 419 (1997)
45 ns	0.69	(1 pulse)	Al	10 – 25	Vorobyev et al., Appl. Phys. A 82 : 357 (2006)
6 ps	1.03	300 kHz	Steel	12.6	Weber et al., Opt. Express 25 (4): 3966 (2017)
65 fs	0.8	(1 pulse)	Ti	20 – 60	Vorobyev et al., J. Phys.: Conf. Ser. 59 : 418 (2007)
65 fs	0.8	(1 pulse)	Zn	10 – 40	Vorobyev et al., Opt. Express 14 (26): 13113 (2006)
60 fs	0.8	1 kHz	Cu, Al	10 – 40	Vorobyev et al., Appl. Phys. Lett. 86 : 011916 (2005)
60 fs	0.8	(1 pulse)	Al	15 – 35	Vorobyev et al., Appl. Phys. A 82 : 357 (2006)



Removal Laser Configurations: Heat Accumulation

Laser heating is:



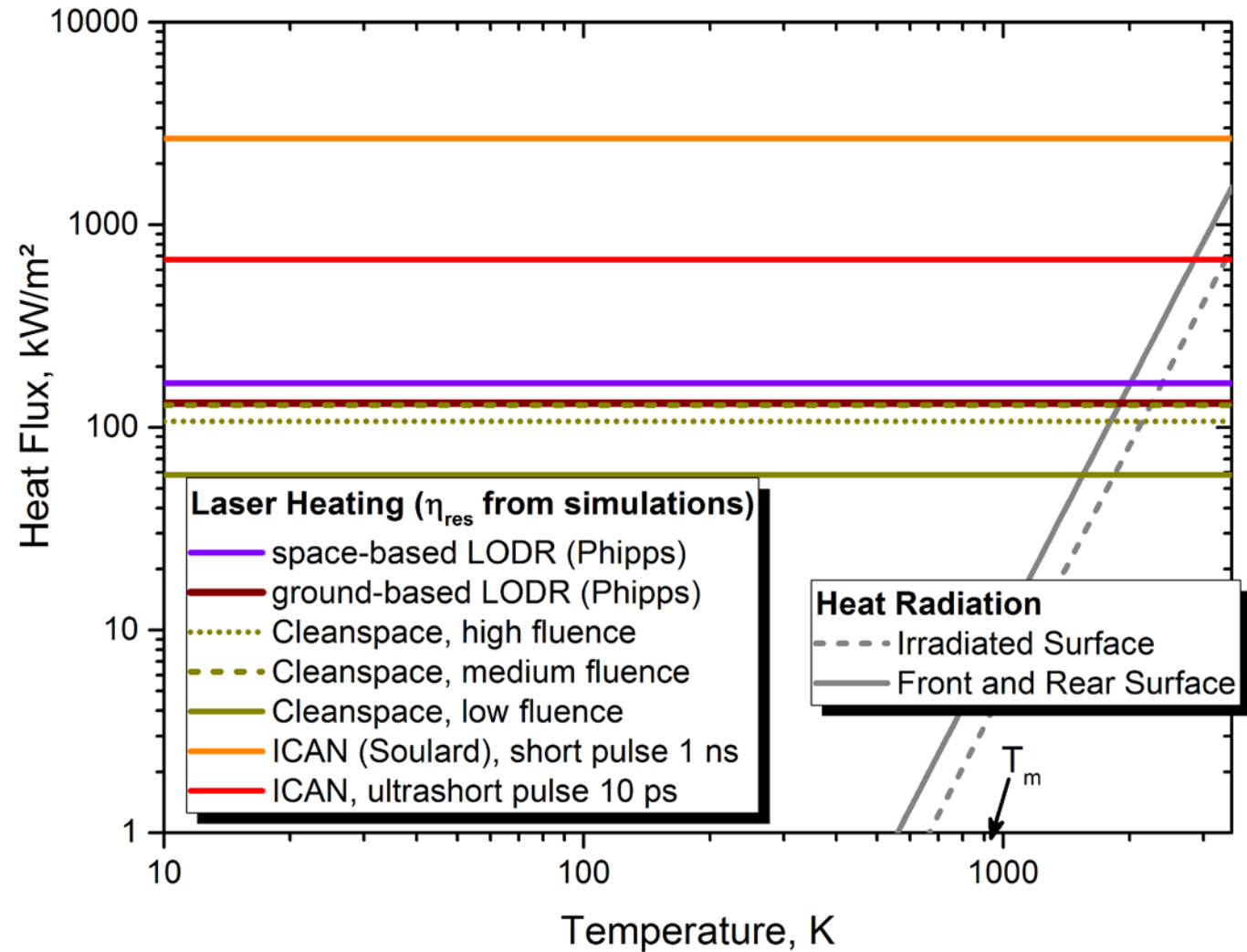
Scharring et al.,
AIAA Journal
(accepted
manuscript)



Removal Laser Configurations: Heat Accumulation

Laser heating is:

- at least 3 orders of magnitude faster than heat re-radiation



Scharring et al.,
AIAA Journal
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manuscript)

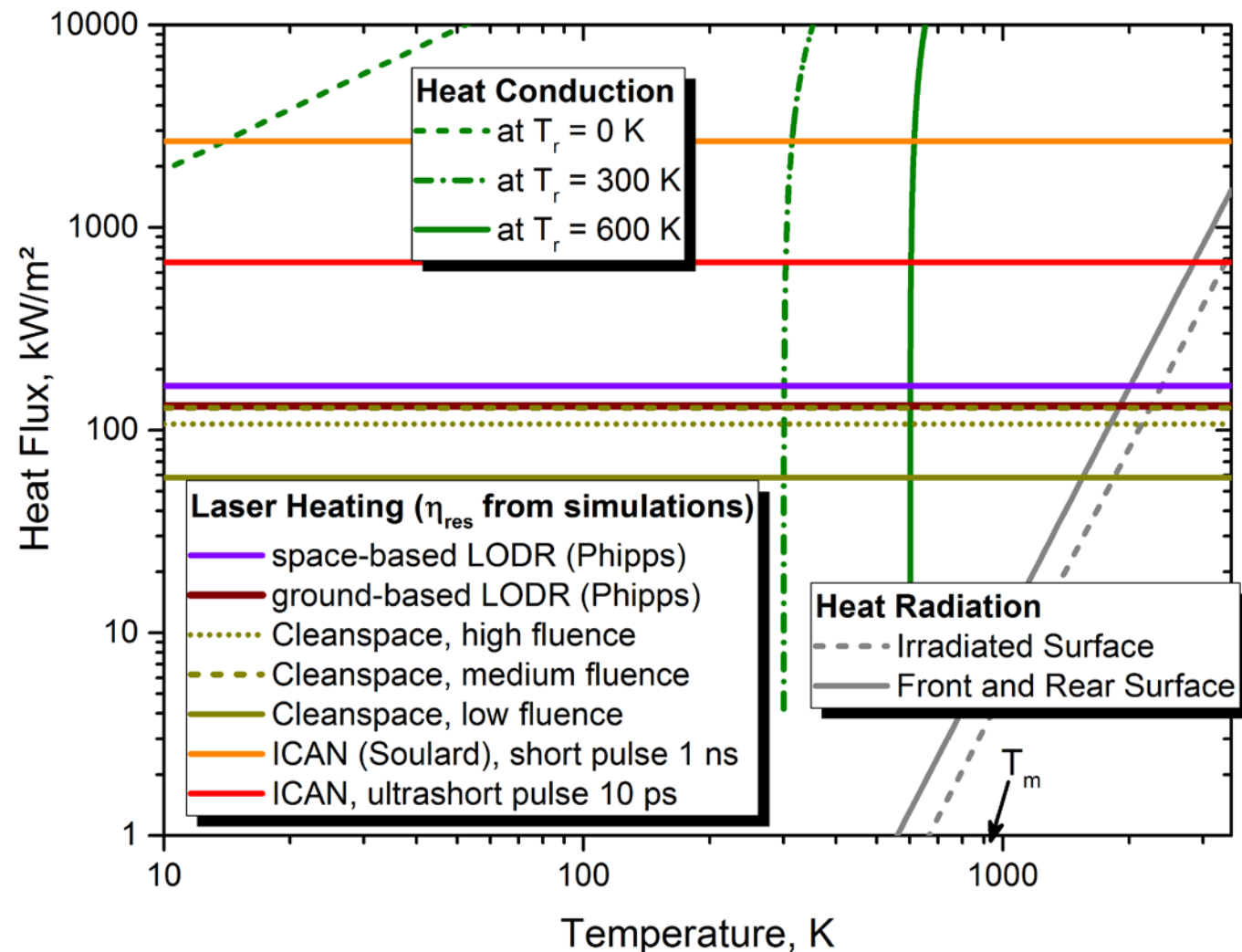


Removal Laser Configurations: Heat Accumulation

Laser heating is:

- at least 3 orders of magnitude faster than heat re-radiation
- much slower than heat conduction (for significant T-gradients)

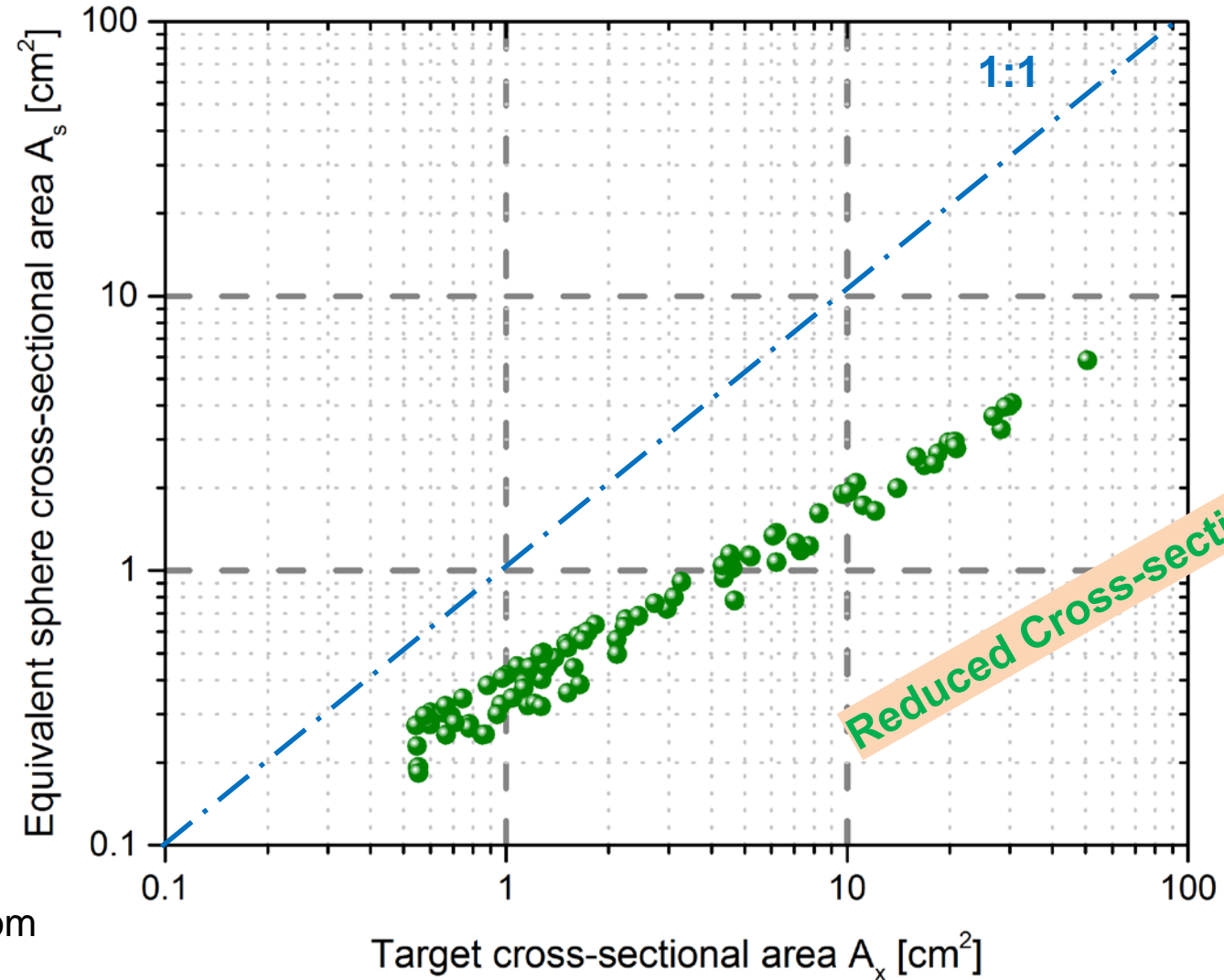
Simulations for Al sample targets



Scharring et al.,
AIAA Journal
(accepted
manuscript)



Target Melting: Space Debris Compactor



Ellipsoid Sample Targets from Monte Carlo Simulations

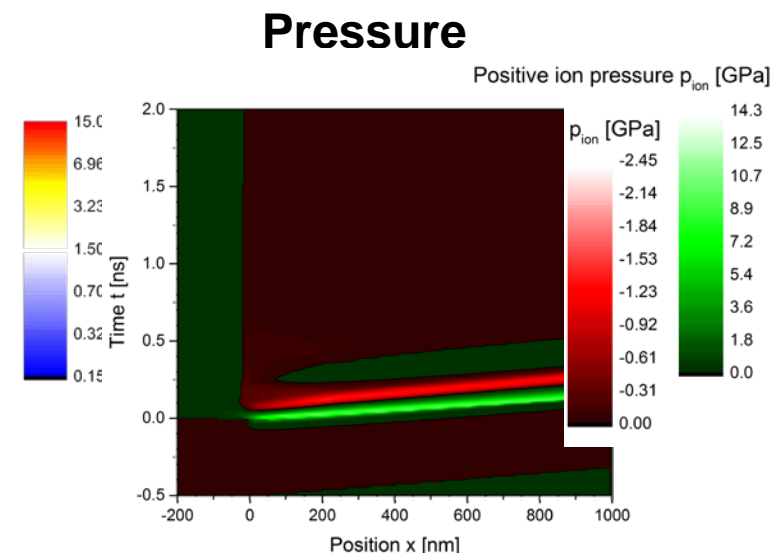
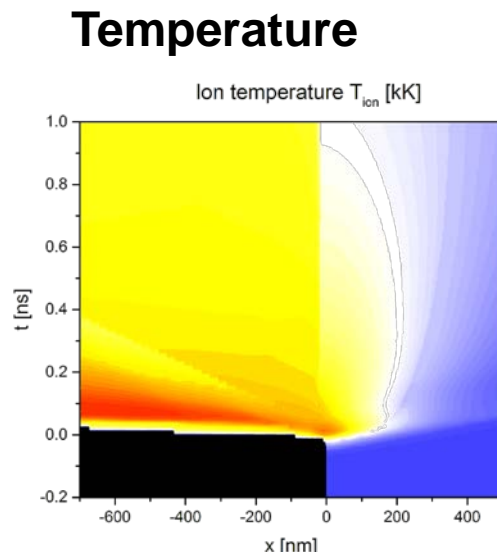
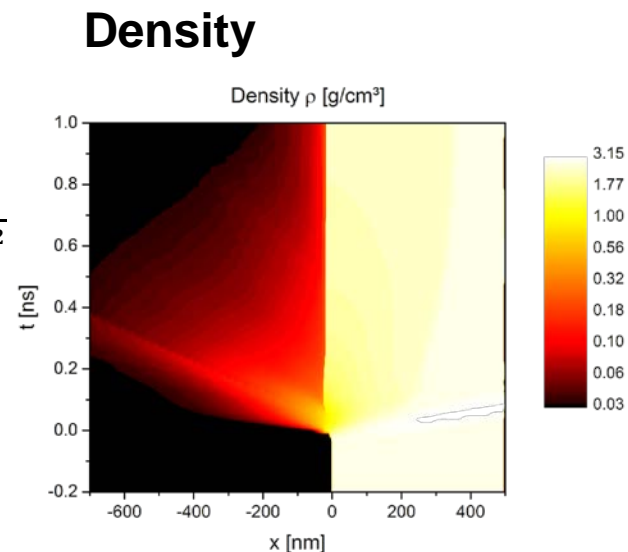


Residual Heat and Mechanical Stress in Short and Ultrashort-Pulse Ablation

Short pulses:

Example $\tau = 50 \text{ ps}, \Phi = 1.49 \frac{\text{J}}{\text{cm}^2}$

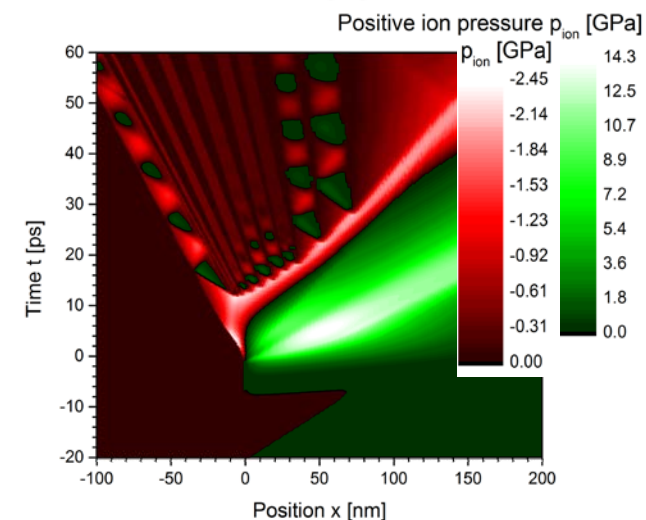
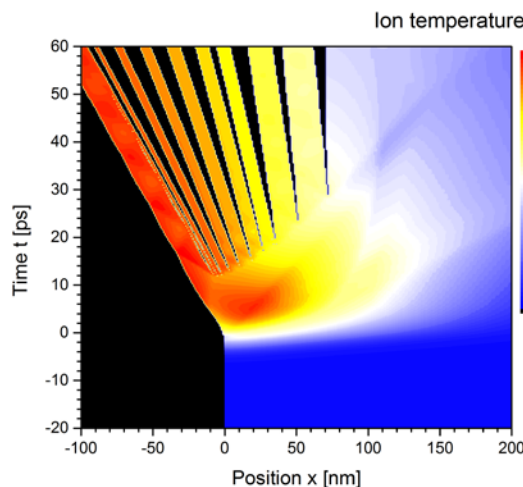
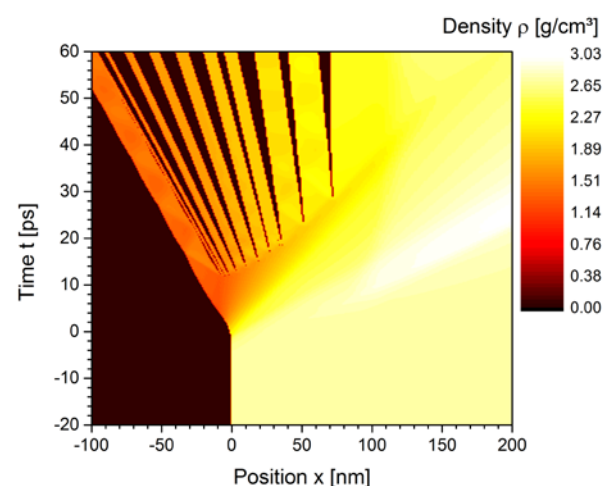
- Large residual heat
- Moderate pressure waves



Ultrashort pulses

Example: $\tau = 5 \text{ ps}, \Phi = 0.74 \frac{\text{J}}{\text{cm}^2}$

- Low residual heat
- Strong pressure waves



Hydrodynamic simulations with Polly-2T, code kindly provided by Mikhail Povarnitsyn, JIHT RAS Moscow



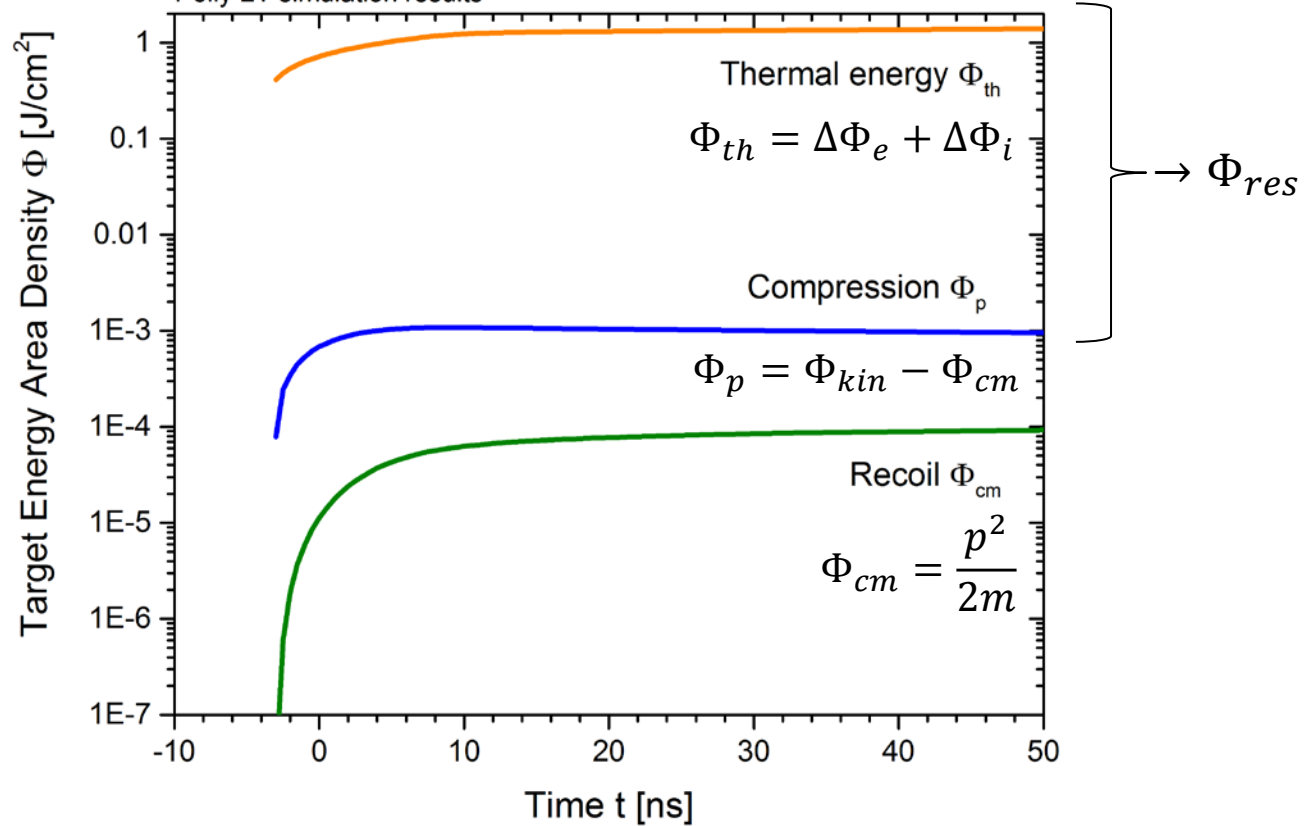
Shockwave thermalization

Short Pulses, Example: 10 ns

Al Target, $\Phi = 10 \text{ J/cm}^2$

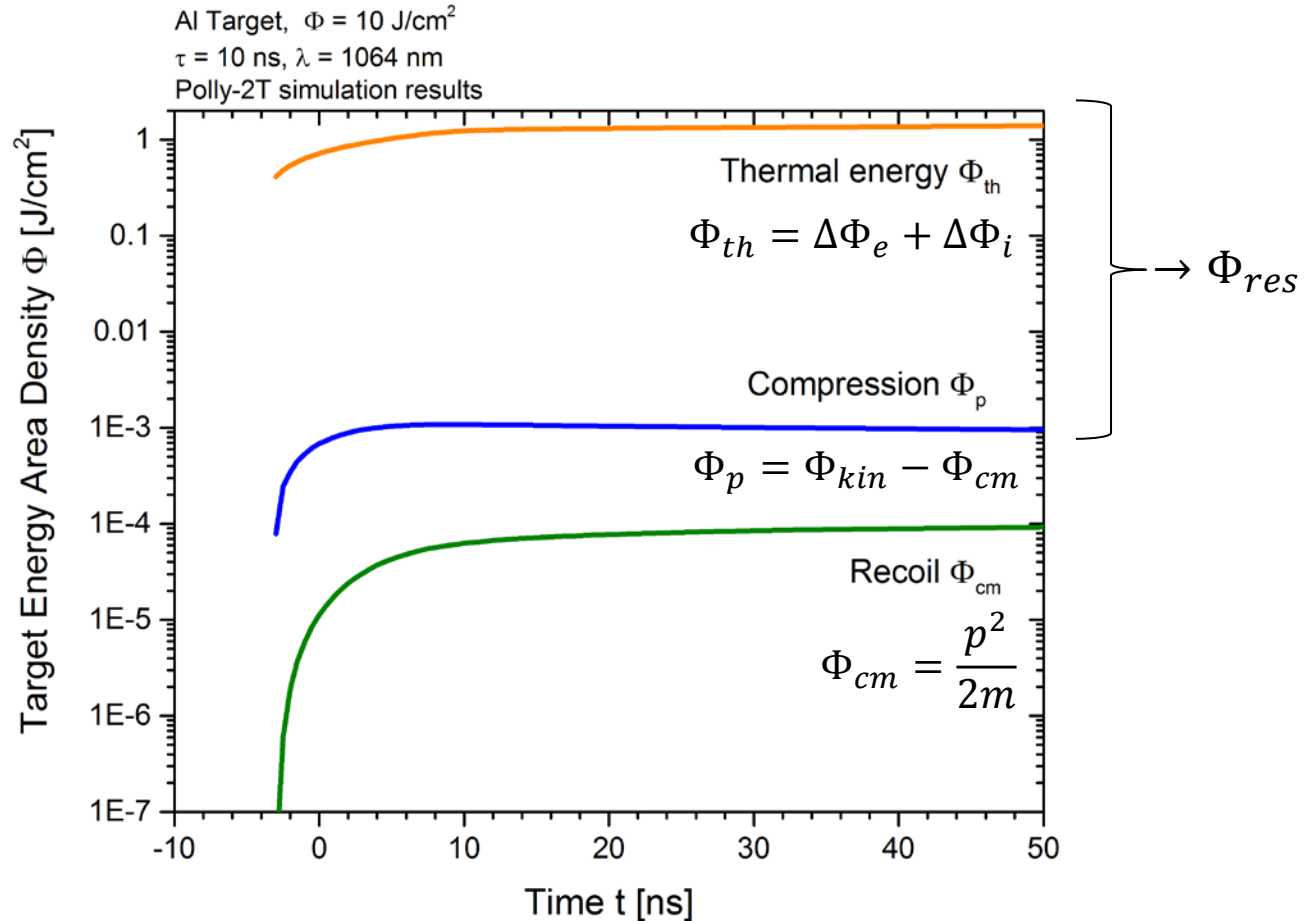
$\tau = 10 \text{ ns}$, $\lambda = 1064 \text{ nm}$

Polly-2T simulation results

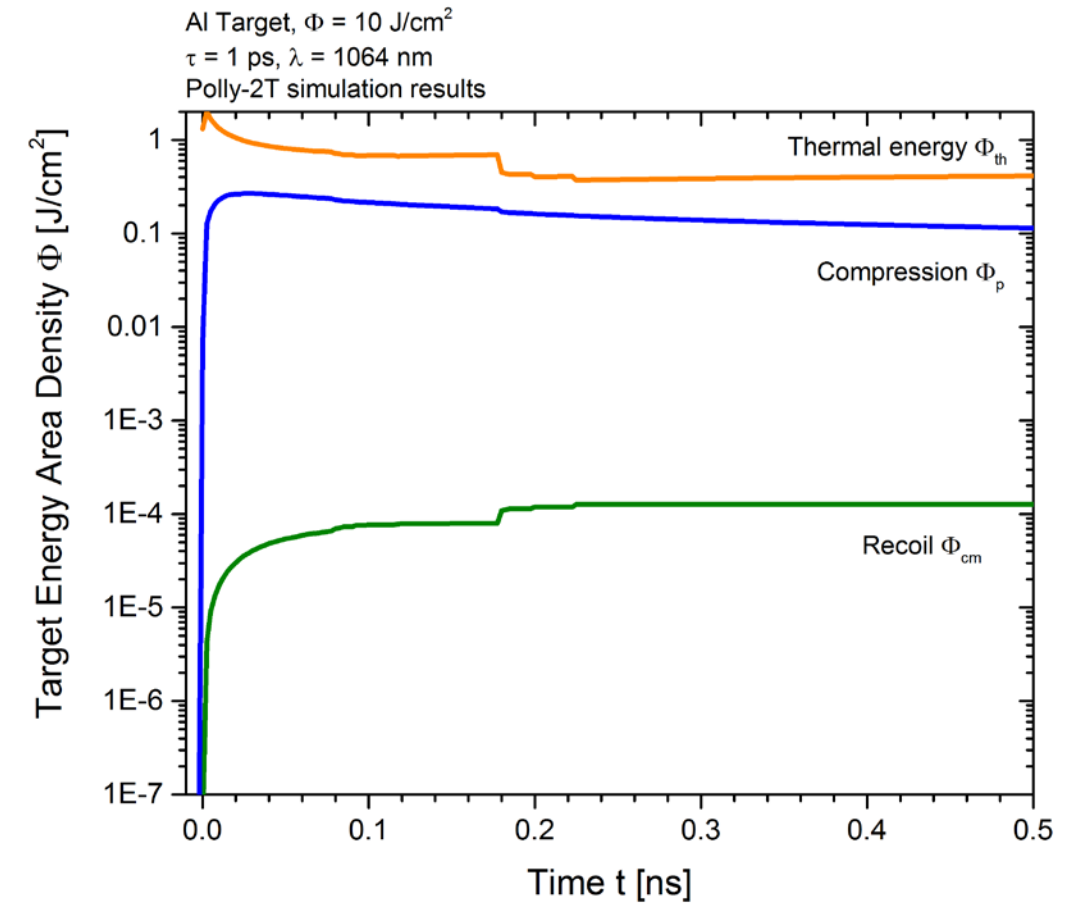


Shockwave thermalization

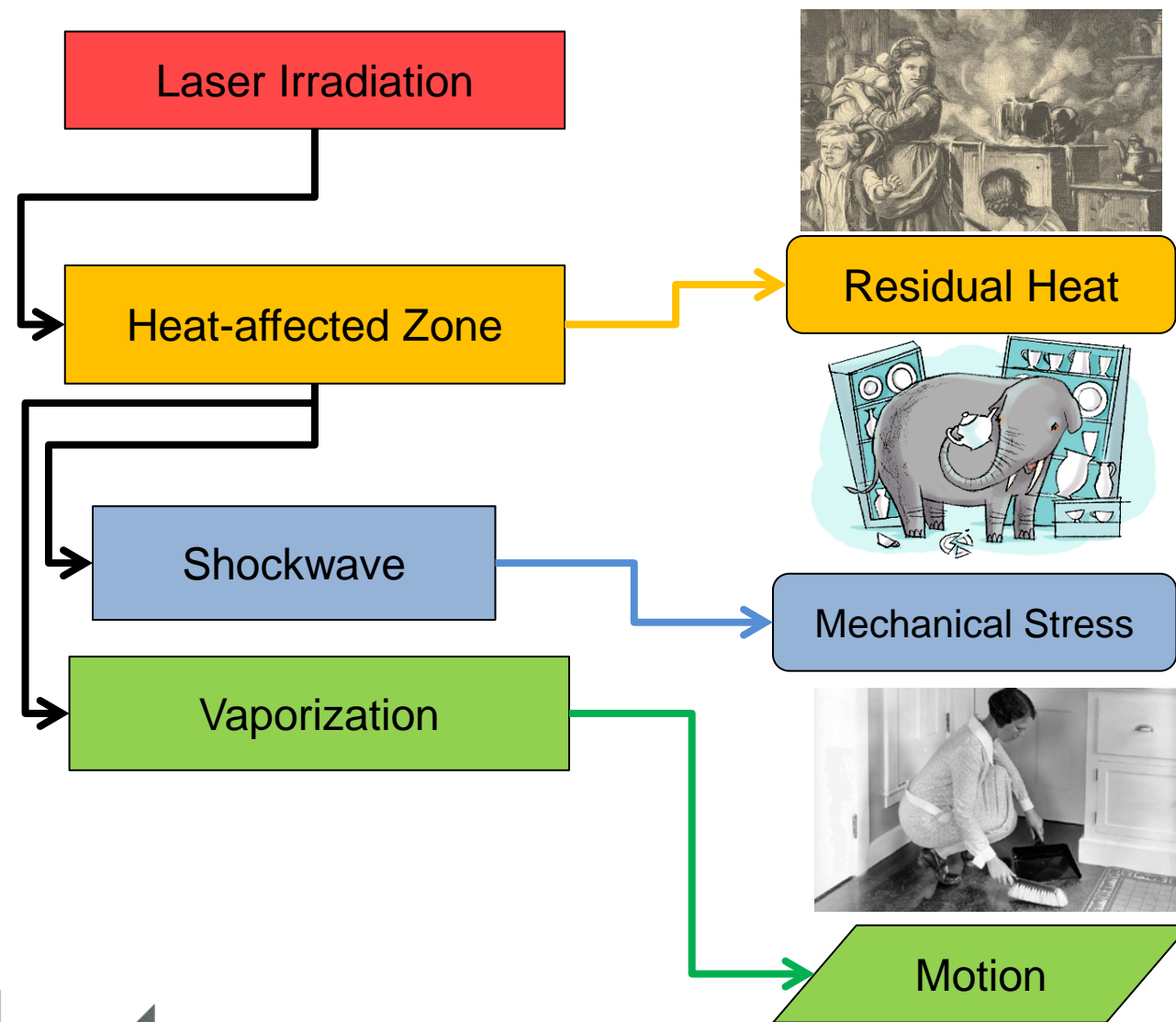
Short Pulses, Example: 10 ns



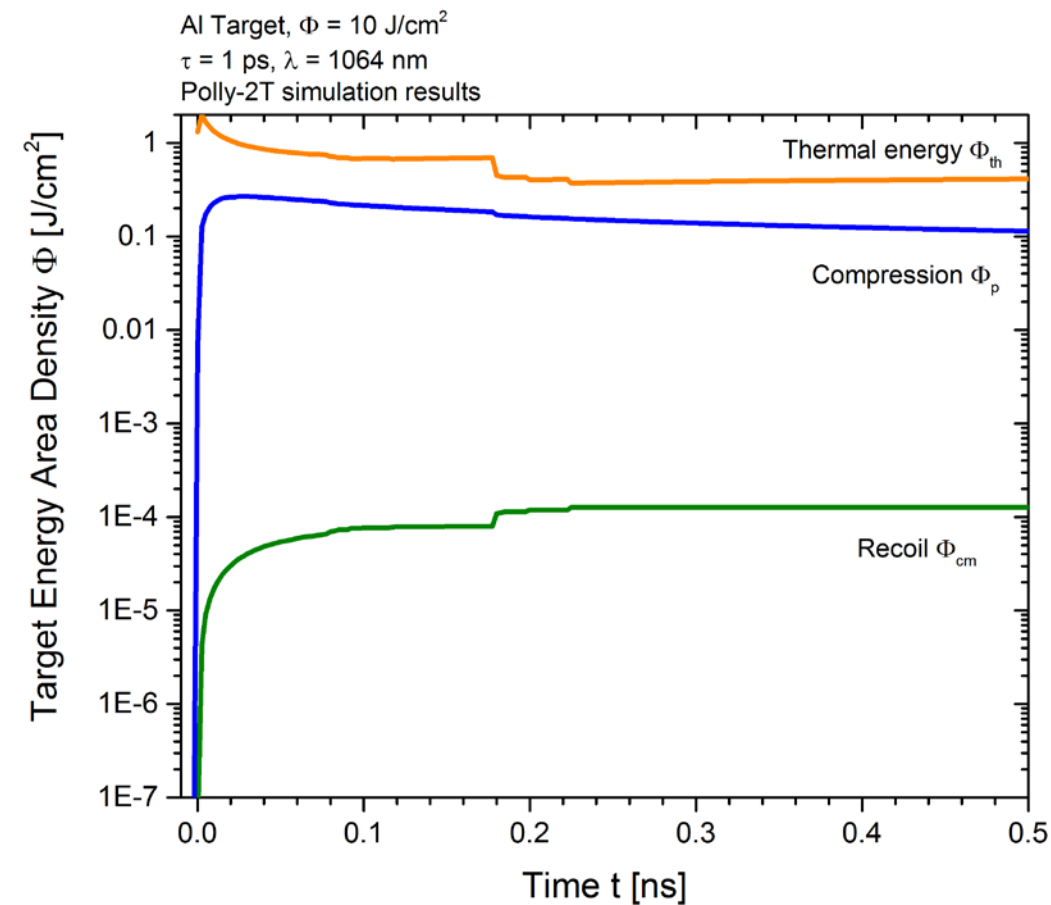
Ultrashort Pulses, Example: 1 ps



Side Effect: Ablative Recoil

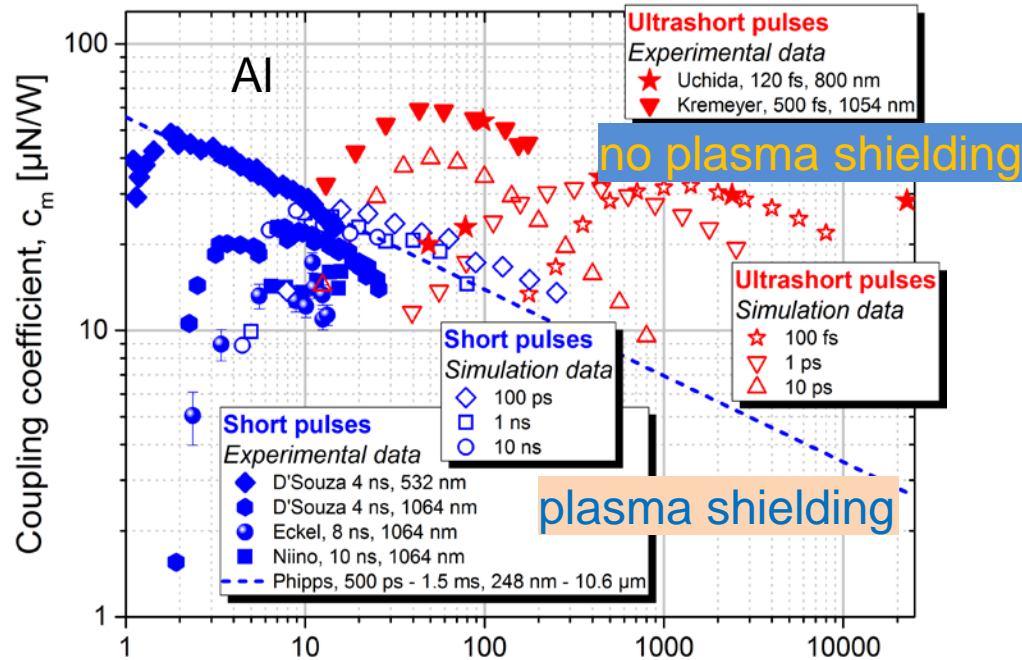


Ultrashort Pulses, Example: 1 ps



HD Simulations on Momentum Coupling Experimental Validation

Wide Range



Laser-matter-interaction parameter $I\lambda\sqrt{\tau}$ [W√s/cm]

D'Souza, B. C., PhD Thesis, University of Southern California, 2007

Niino, M. et al., Proc. SPIE, 3885: 370 – 377 (2000)

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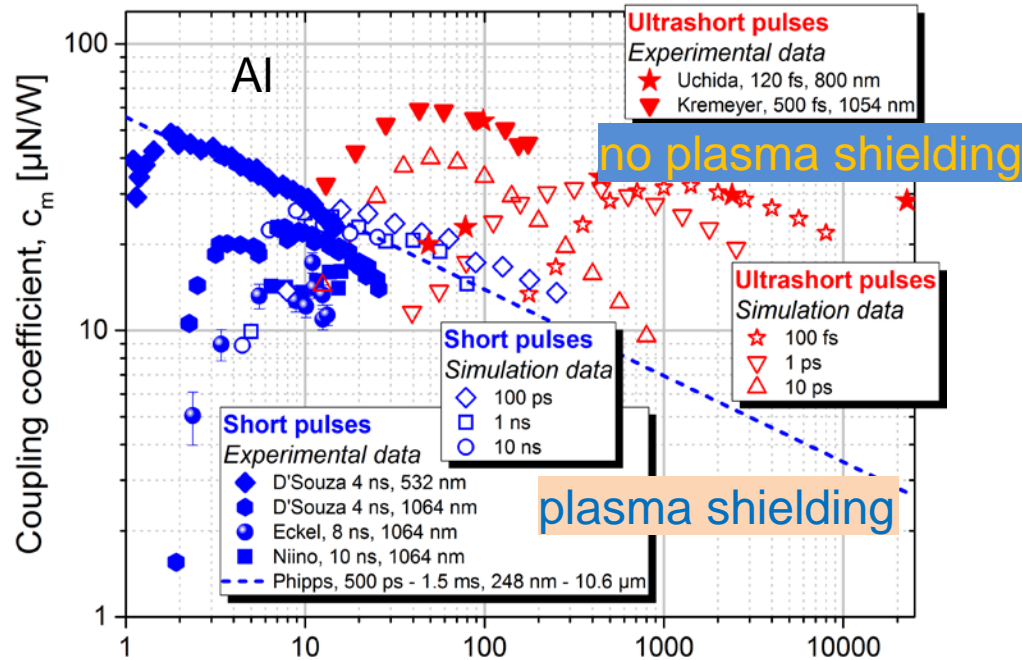
K. Kremeyer, et al., AIP Conf. Proc., 997: 147 – 158 (2008)

C.R. Phipps et al., J. Appl. Phys. 64(3): 1083 – 1096 (1988)



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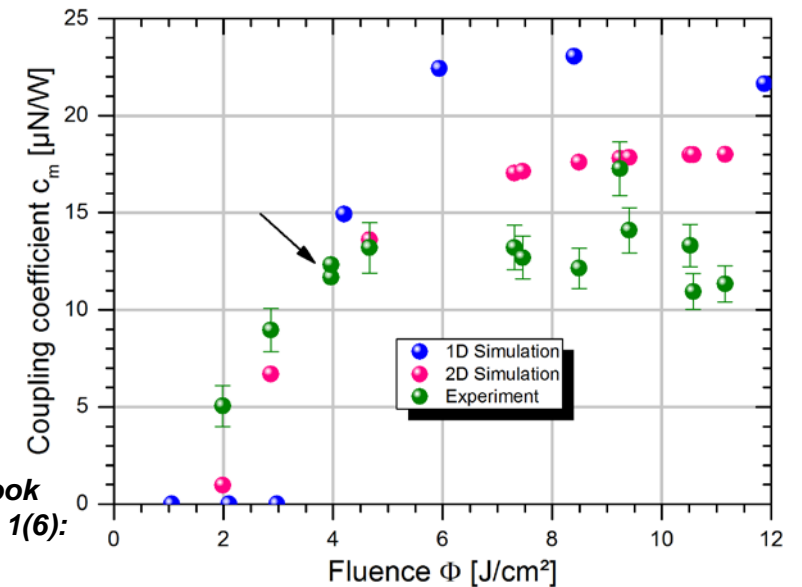
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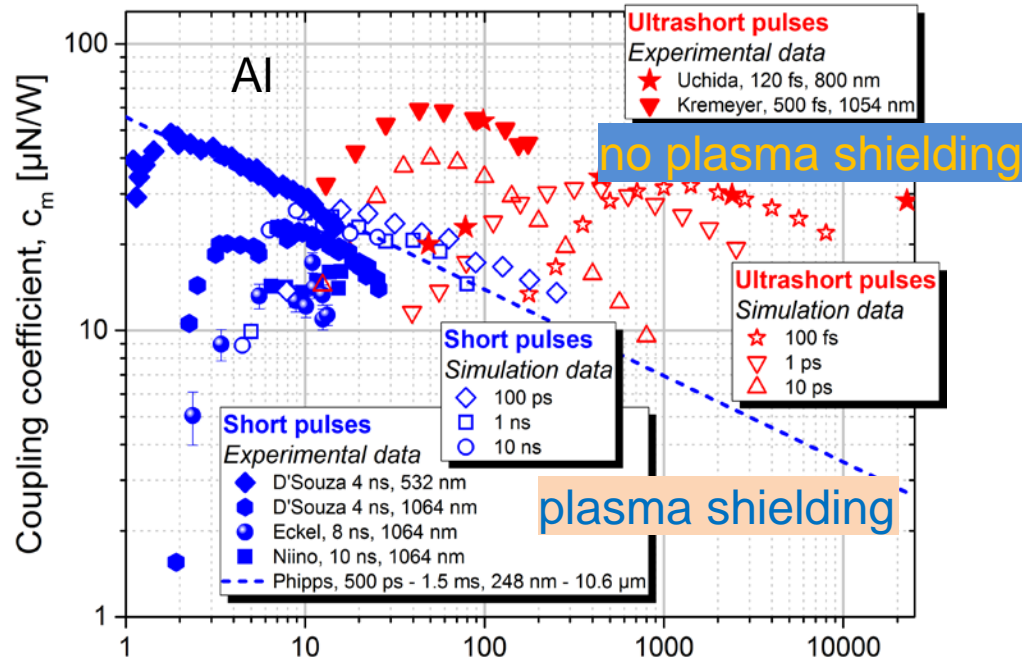
Short Pulses



S. Scharring et al., *IAA Book Series on Small Satellites 1(6): 27 – 34 (2016)*

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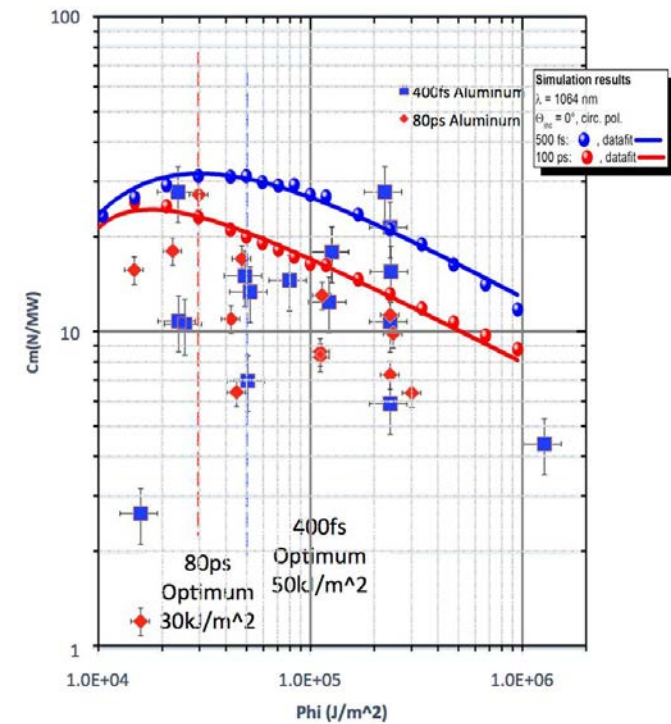
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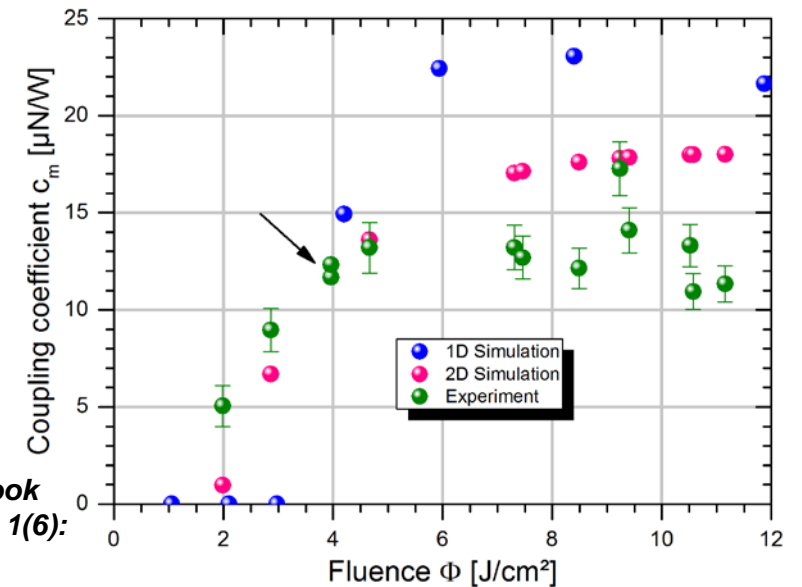
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Ultrashort Pulses



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$$c_{tm} = \frac{\Delta p}{Q_{Heat}} = \frac{\text{Thrust}}{\text{Heating Power}}$$

Thermo-mechanical Coupling

$$\Delta v_{max} = \frac{c_m}{\eta_{res}} \cdot c_p \cdot (T_m - T_0) = c_{tm} \cdot c_p \cdot (T_m - T_0)$$



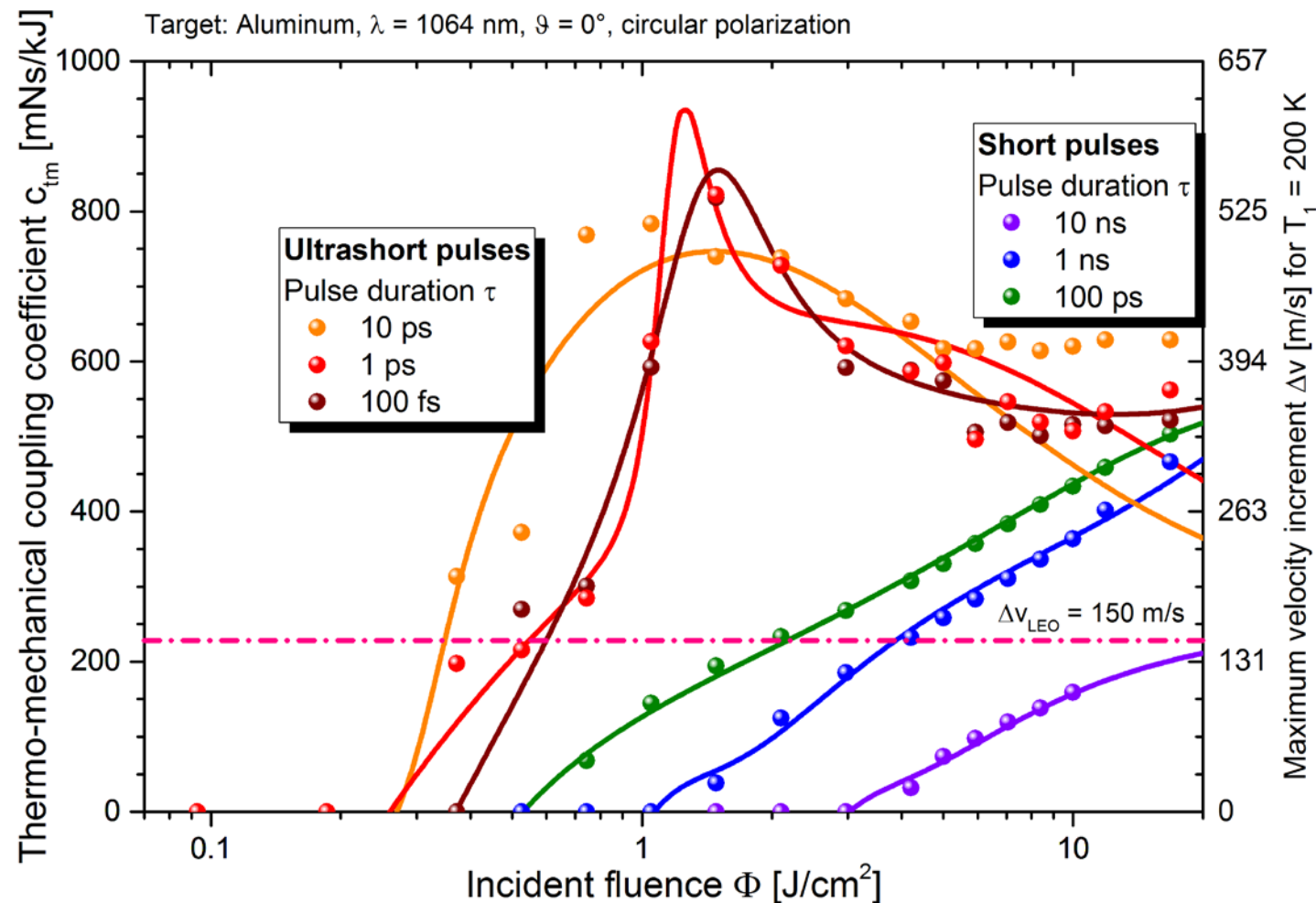
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Pulse Length Dependency

- Short Pulses:
 - Unfavourable thermo-mech. coupling
 - Acceptable at larger fluences
- Ultrashort Pulses:
 - Advantageous thermo-mech. coupling
 - Even at moderate fluences



Space Debris – Properties

- Characteristic length L_C

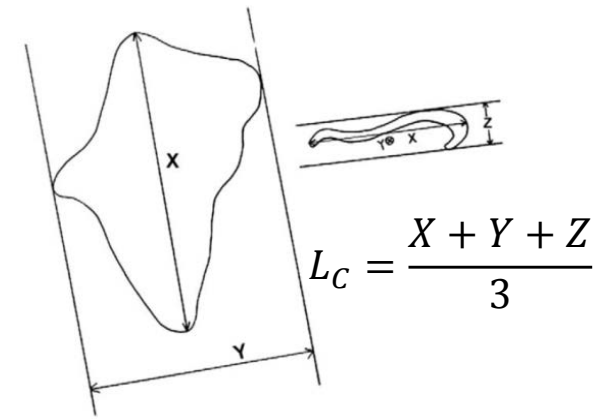
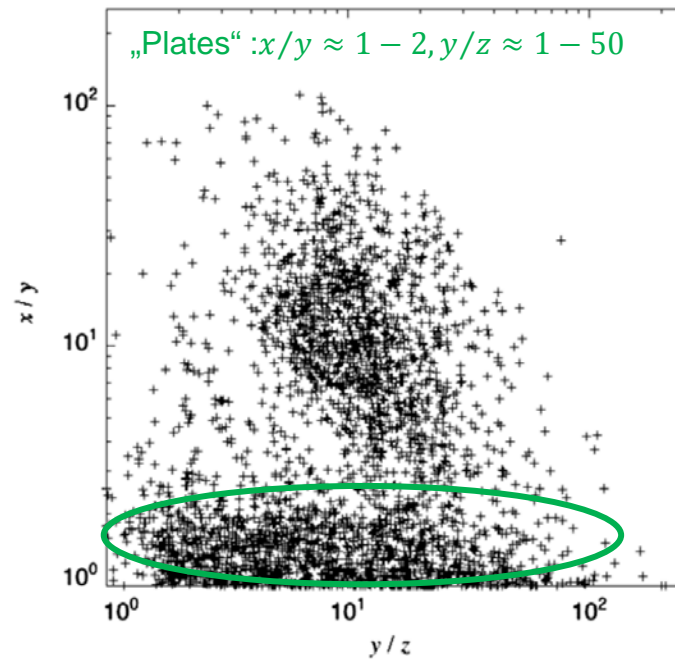
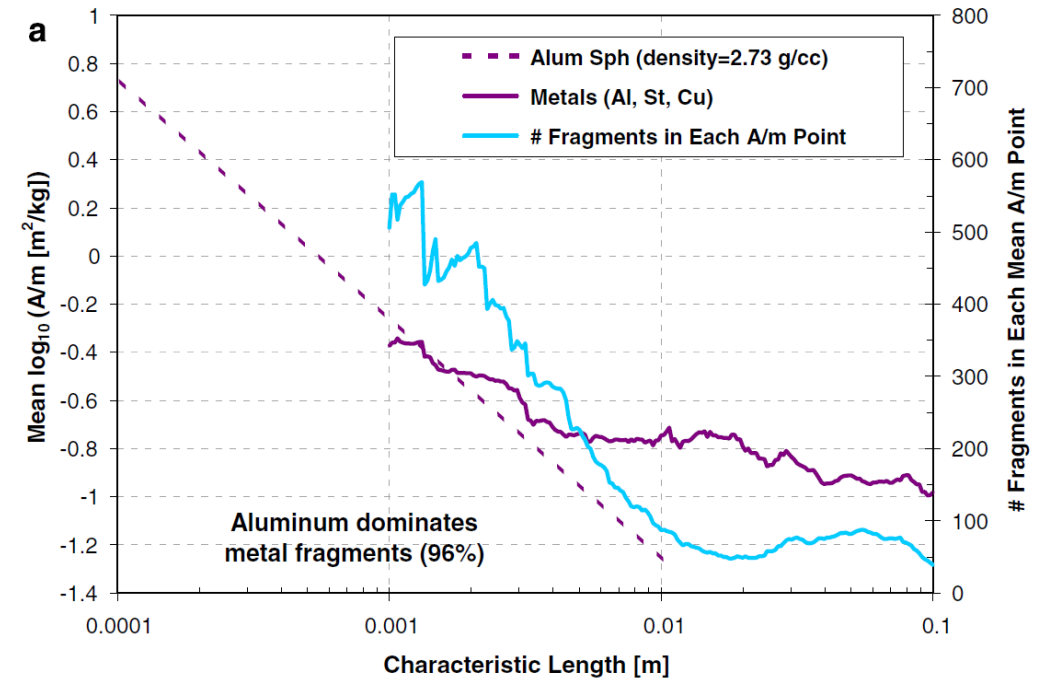


Fig. 6. Sketch of NASA orthogonal 'Projection Dimensions' in Krisko et al. (2008).

Hanada et al., Adv. Space Res. 44(5): 558 – 567 (2009)



T. Hanada et al., ibid



P.H. Krisko et al., Adv. Space Res. 41: 1138 – 1146 (2008)



Space Debris – Properties

- Characteristic length L_C
- Cross-sectional area A_x

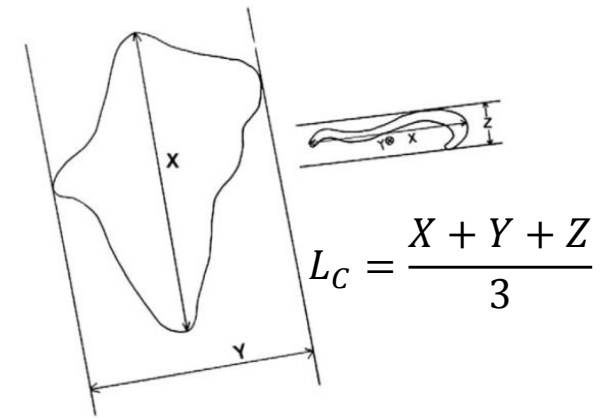
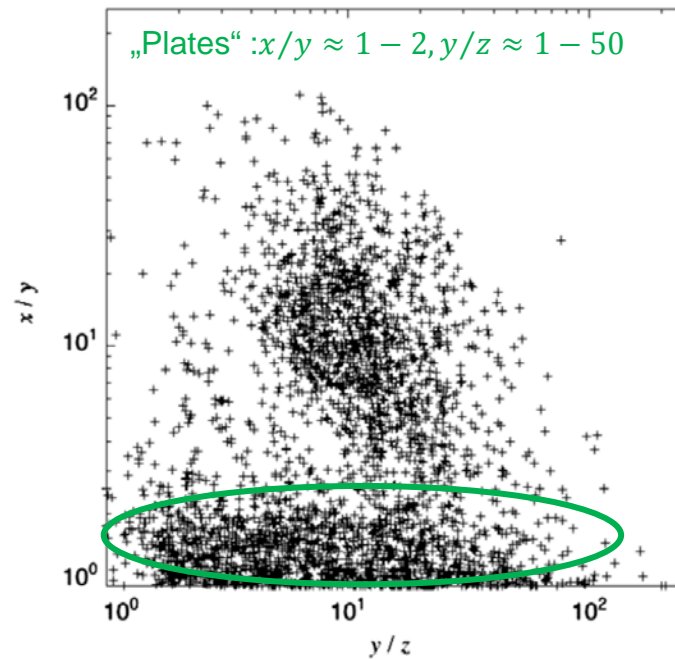
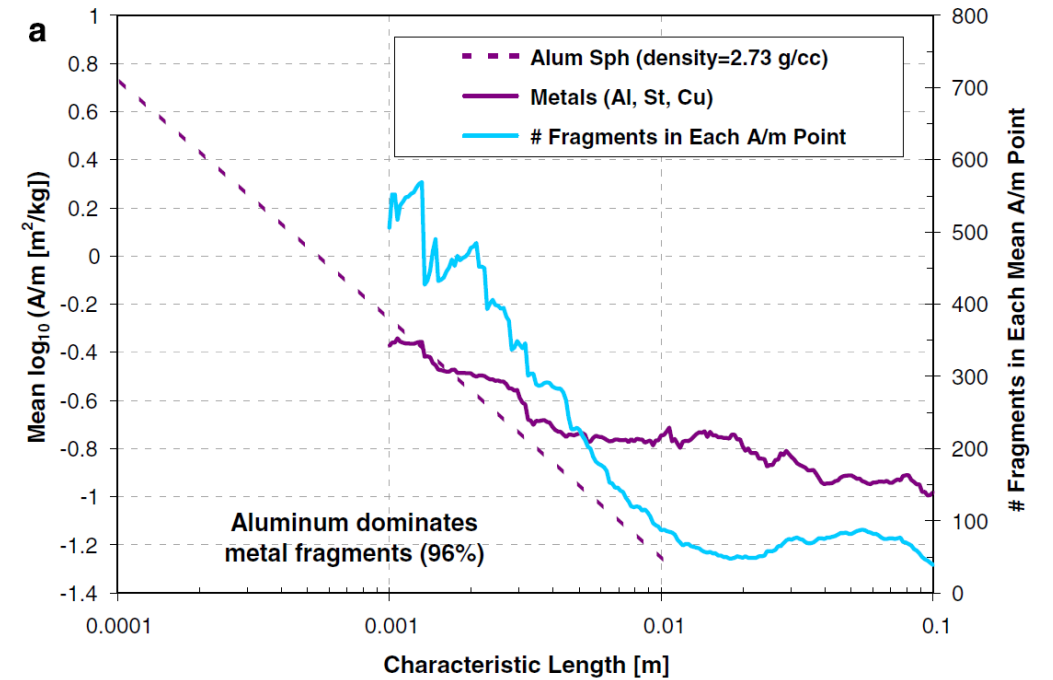


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Space Debris – Properties

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- Cross-sectional area A_x
- Area-to-mass ratio: A_x/m
- Material: mainly aluminum

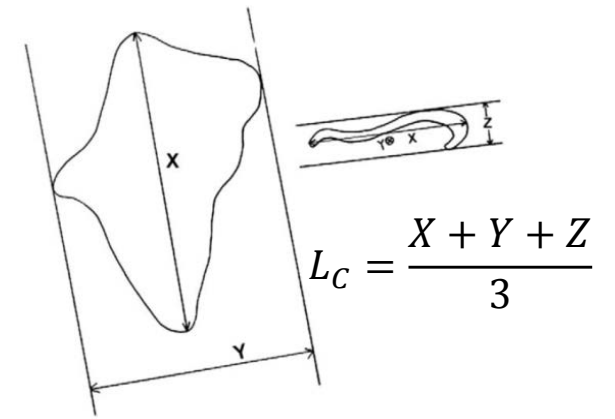
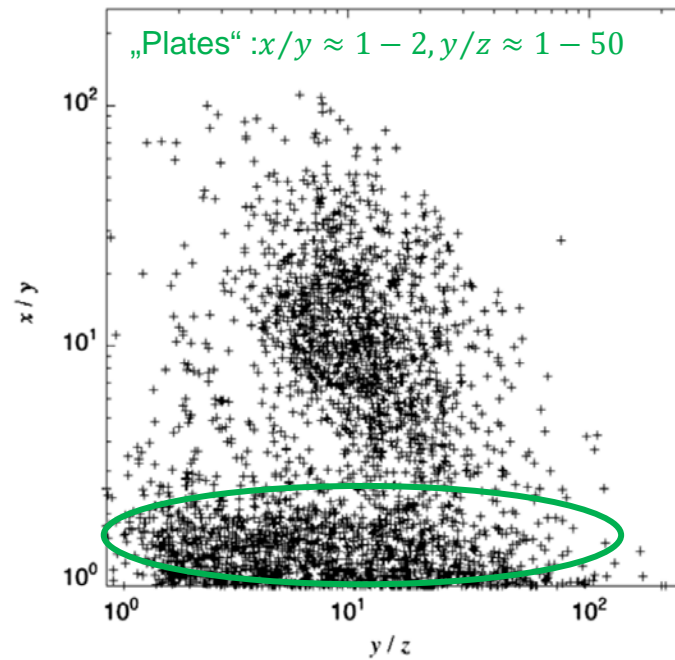
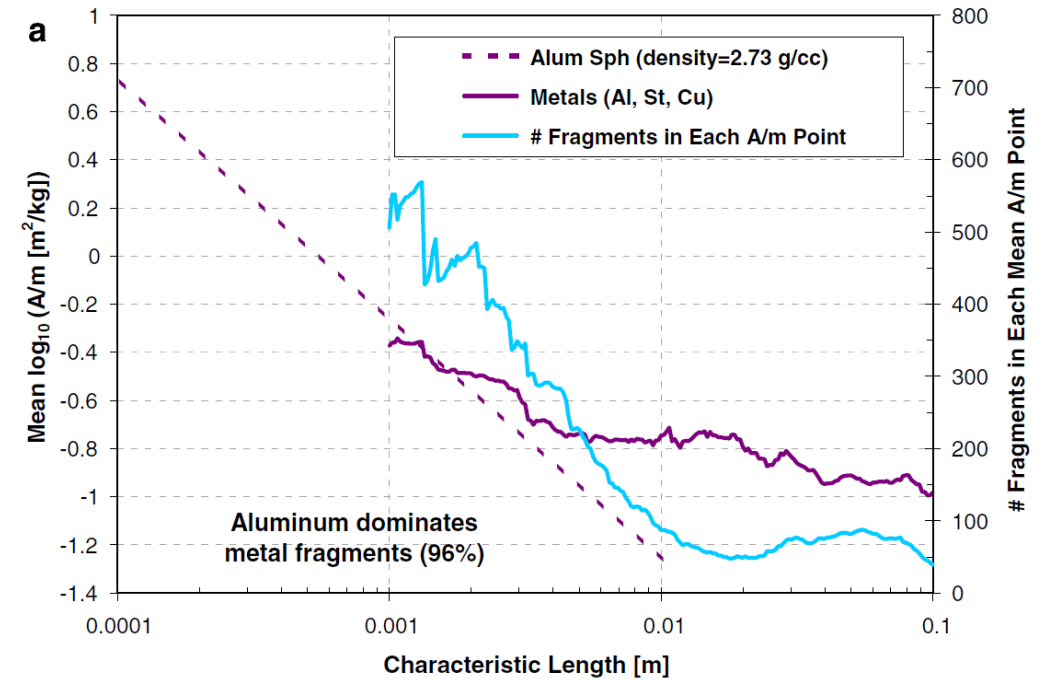


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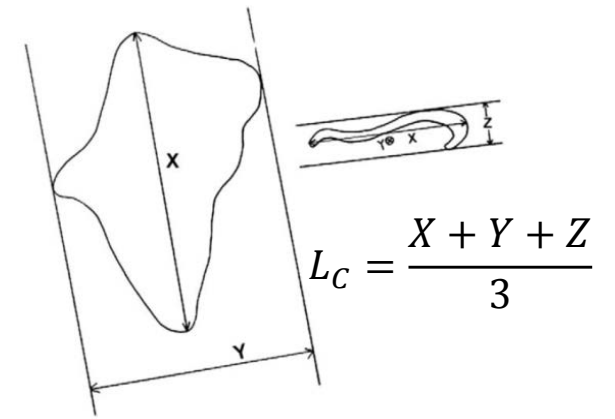
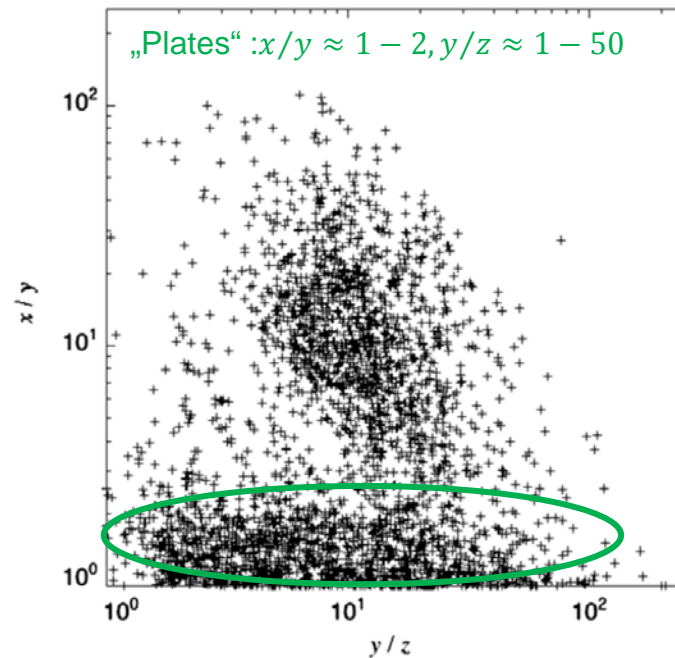
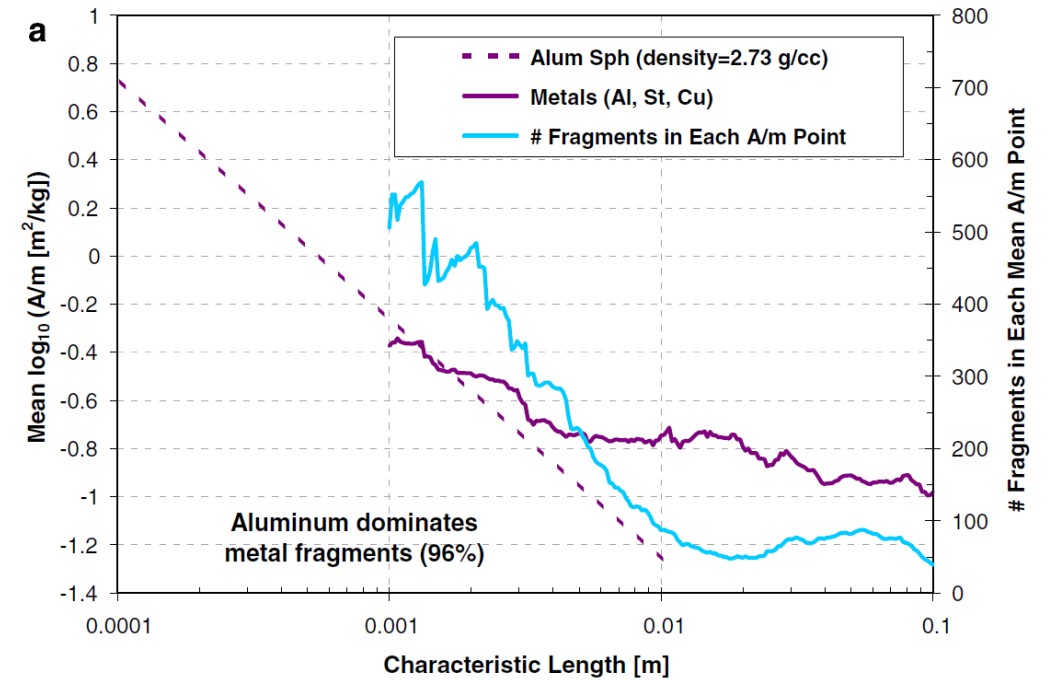


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$$A_x = 0.5556945 \cdot L_c [m]^{2.0047077} | L_c \geq 1.67 \text{ mm}$$

NASA standard breakup model, in Hanada, *ibid*.

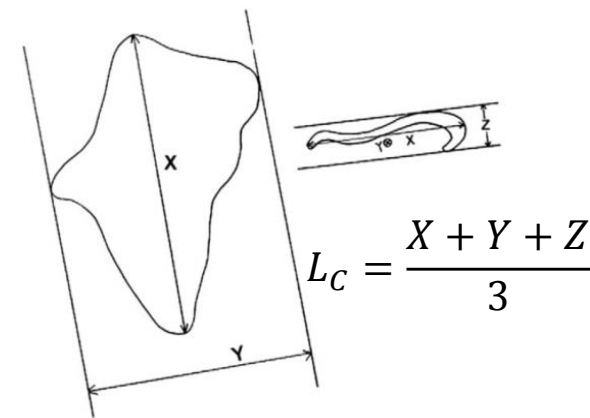
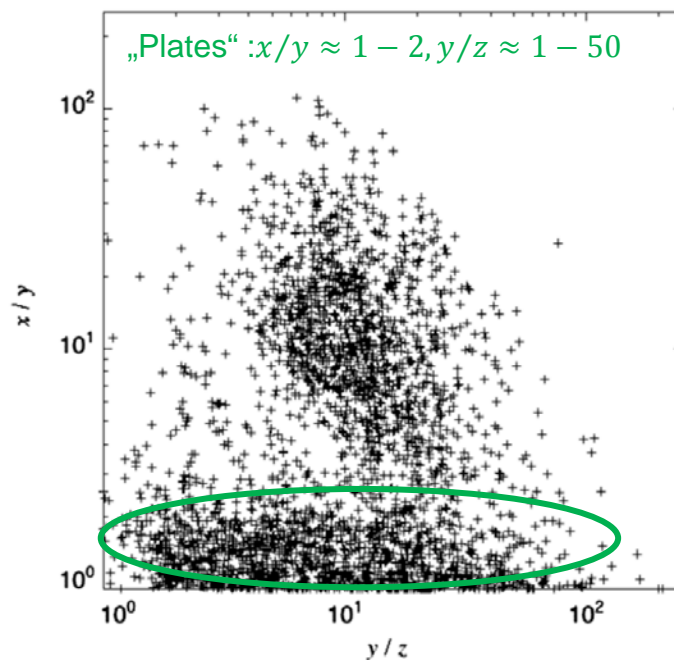
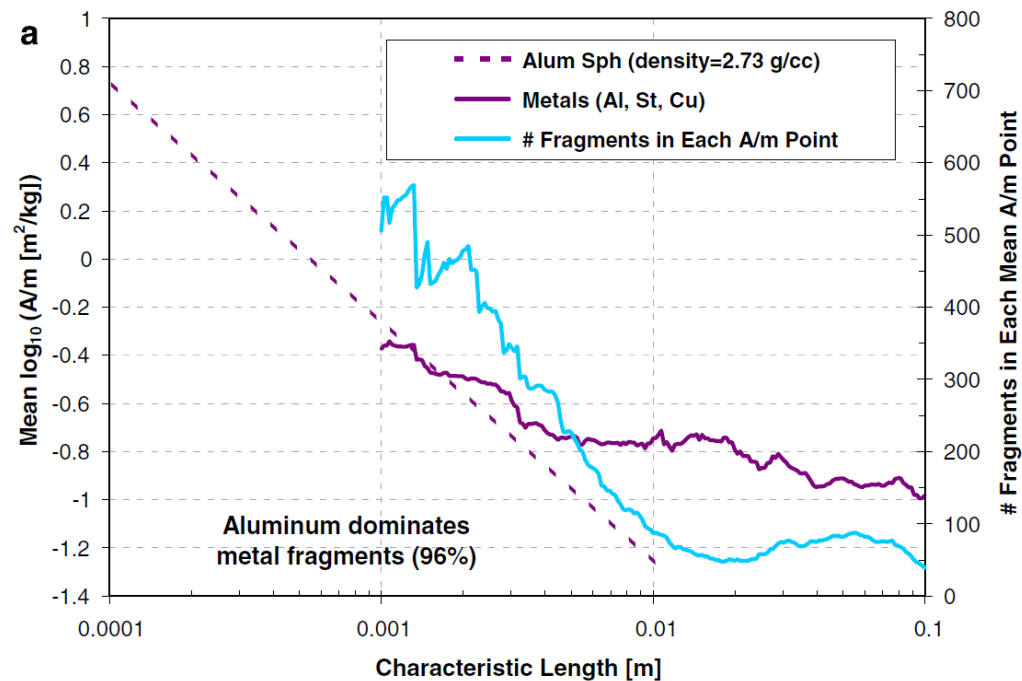


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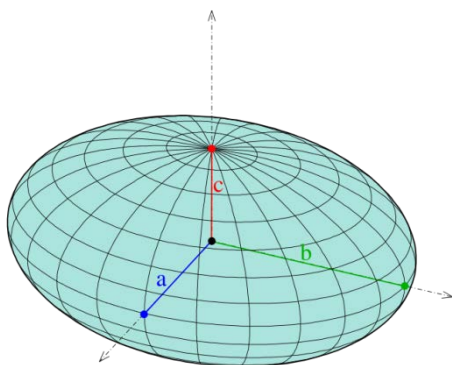
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Laser cross-section area vs. area-to-mass ratio

Laser cross-sectional area (projections)

- Maximum: $A_{max} = \pi ab$
- Minimum: $A_{min} = \pi bc$



from:
<https://commons.wikimedia.org/wiki/File:Ellipsoide.svg>
 CC-BY-SA-4.0, author: Ag2gaeh



Space debris cross-sectional area

$$A_x = 0.5556945 \cdot L_c [m]^{2.0047077} \quad | L_c \geq 1.67 \text{ mm}$$

with characteristic length $L_c = \frac{X+Y+Z}{3}$

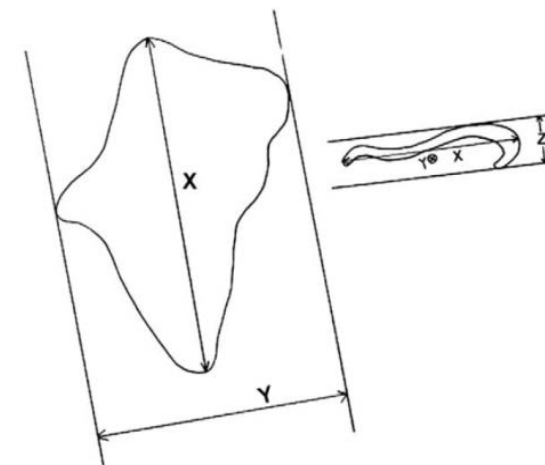
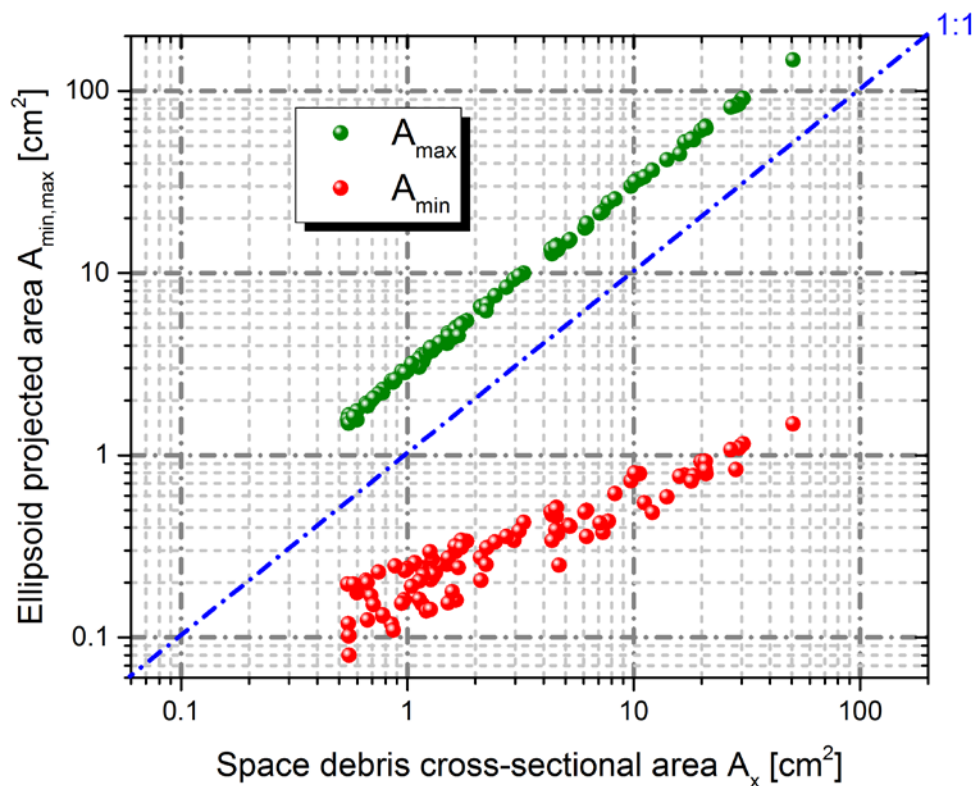


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Analytical treatment of momentum scatter for a 1D plate

Target position in a Gaussian beam

- Optimum position:

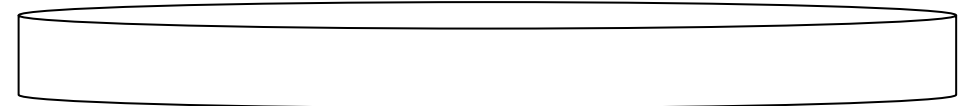
$$r = 0 \rightarrow \Phi(r) = 2\langle\Phi\rangle, \Delta v \approx 2 \frac{c_m \cdot A \cdot \Phi}{m}$$

- Worst position:

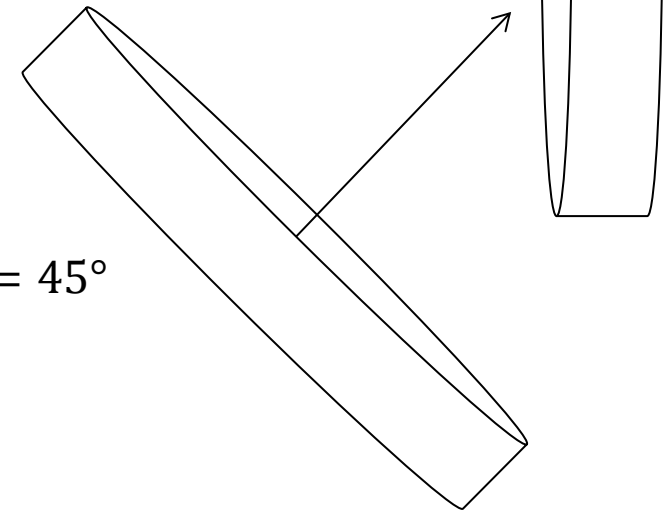
$$r \gg \sigma: \Phi(r) < \Phi_0, \Delta v \approx 0$$

Mean target orientation

- Optimum orientation: $\Delta v \rightarrow \frac{c_m \cdot A \cdot \Phi}{m}$



- Worst orientation: $\Delta v \rightarrow 0$



- Average orientation: $\alpha = 45^\circ$



Expedit Upgrade: Temperature-Sensitive Modeling of Repetitive Debris Irradiation

→ Interaction of thermo-mechanical coupling and debris temperature

→ $c_m(\Phi, T), \eta_{res}(\Phi, T)$ experimental data needed!

→ Approximation $c_m(\Phi, T_{init}) = c_m(\Phi + c_p \rho d (T_{init} - T_0), T_0)$

→ Intra-pulse radiative cooldown

→ Temperature-dependent material parameters: $c_p(T), \rho(T), \varepsilon(T)$

