Uncertainty Analysis in Railway Asset Management using the Point Estimate Method

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Motivation



- Detection
- Diagnosis
- Prognosis



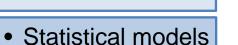
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- Failures
- Reliability



Modelling



- Physical models
 - Hybrid models



Preventive and condition-based maintenance

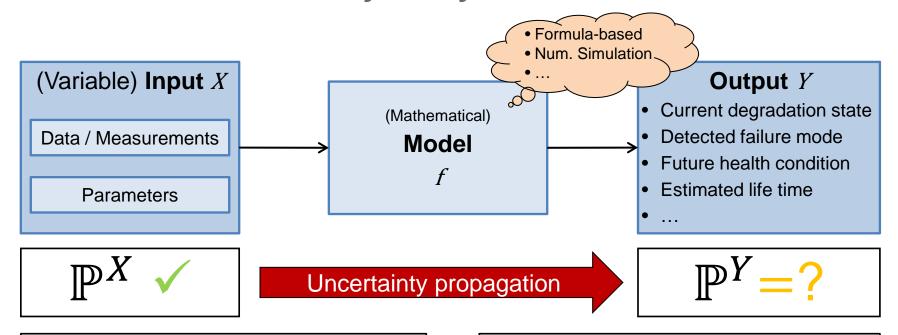


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UNCERTAINTY



Models and Uncertainty Analysis



Sources of uncertainty in modelling

- Data / Measurements
- Model parameters
- Model structure

Mathematical notation

$$f: \mathbb{R}^n \to \mathbb{R}$$
 $Y = f(X)$ where

$$X = (X_1, \dots, X_n)^T$$

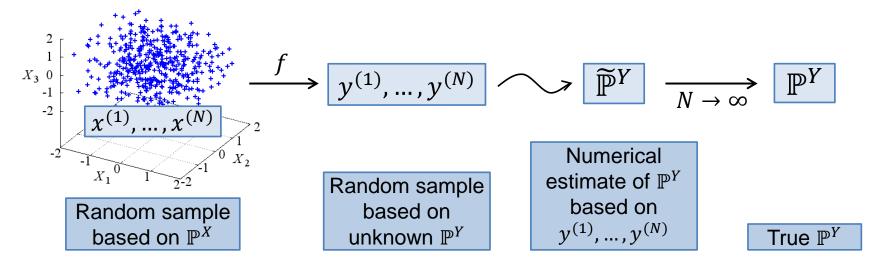
 $(X_i \text{ stochastically independent})$



How to derive the output distribution?



Standard approach: Monte Carlo simulation (MC)



- In general, large samples necessary!
- Approximate results only!



Alternative approach: Point Estimate Method (PEM)

• Often it is **sufficient to know** some **basic statistics** of the output distribution

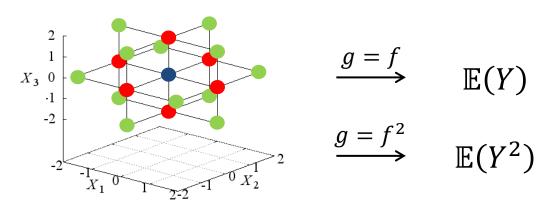
Mean: $\mathbb{E}(Y)$ Variance: Var(Y) k-th moment: $\mathbb{E}(Y^k)$...

• Approximation scheme (= core element of PEM):

$$\int_{\Omega} g(x) \operatorname{pdf}_{X}(x) dx \approx w_{0} g(\operatorname{GF}[0]) + w_{1} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}} g(\operatorname{GF}[\pm \vartheta]) + \dots + w_{m} \sum_{m \text{ times}$$

with suitable weights w_j and deterministic sample points

- **GF**[0]
- $GF[\pm \vartheta]$
- $GF[\pm\vartheta,\pm\vartheta]$
- ...



$$Var(Y) = \mathbb{E}(Y^2) - (\mathbb{E}(Y))^2$$



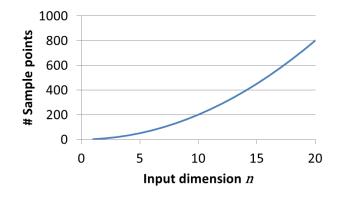
Standard scheme (m = 2)

$$\int_{\Omega} g(x) \operatorname{pdf}_{X}(x) dx \approx w_{0} g(\operatorname{GF[0]}) + w_{1} \sum g(\operatorname{GF[\pm\vartheta]}) + w_{2} \sum g(\operatorname{GF[\pm\vartheta,\pm\vartheta]})$$
 where
$$w_{0} = 1 + \frac{n^{2} - 7n}{18} \qquad w_{1} = \frac{4 - n}{18} \qquad w_{2} = \frac{1}{36} \qquad \vartheta = \sqrt{3}$$

- Weights determined such that scheme is **exact for polynomials** $g: \mathbb{R}^n \to \mathbb{R}$ (degree ≤ 5) in case of standard Gaussian inputs X_i for i = 1, ..., n
- Transformation of the sample points in case of other input distributions

Number of sample points

$$N = 2n^2 + 1$$

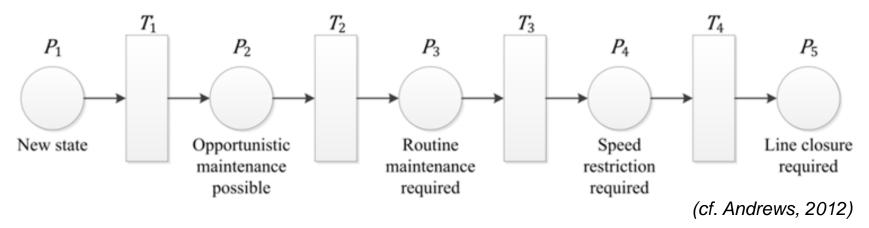


n	N	
1	(3)	
2	9	
3	19	
4	33 (25)	
5	51	



Example of use: Track degradation

• Simple **Petri net model** for track degradation (without maintenance):

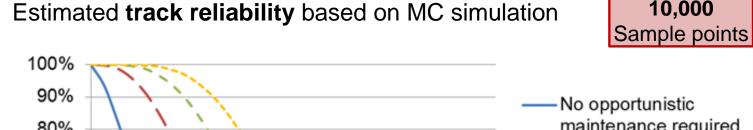


• Stochastic **transitions**: $T_r \sim \mathcal{W}(\beta_r, \eta_r)$ (i.e., Weibull distributed duration [in days] before jumping to the next "health state")

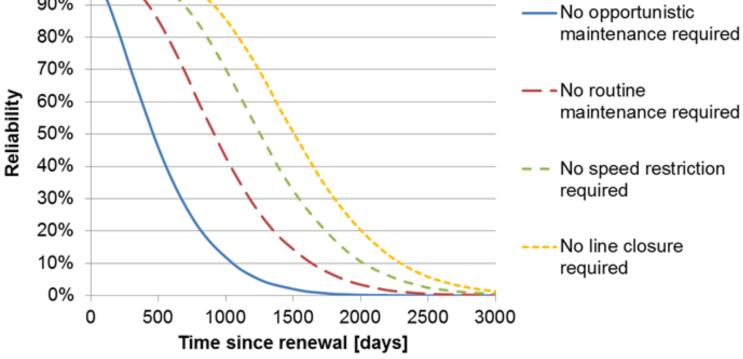
	T_1	T_2	T_3	T_4
eta_r (shape)	1.5	1.5	1.6	1.7
η_r (scale)	600	500	370	280



Example of use: Track degradation



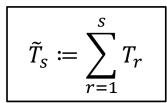
10,000

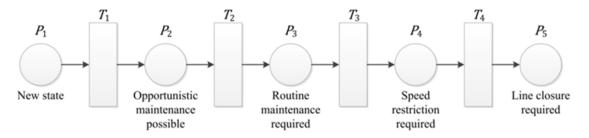




Example of use: Track degradation

• Duration [in days] before reaching state P_{s+1} after renewal or new construction:





Analytical solution	$\mathbb{E}(\cdot)$	$\sigma(\cdot)$
$ ilde{T}_1$	541.6	367.8
$ ilde{T}_2$	993.0	478.7
$ ilde{T}_3$	1324.8	523.7
$ ilde{T}_4$	1574.6	545.1

Δ _{rel} (MC)	$\mathbb{E}(\cdot)$	$\sigma(\cdot)$
$ ilde{T}_1$	-0.68%	+0.50%
$ ilde{T}_2$	-1.00%	-0.03%
$ ilde{T}_3$	-0.56%	+0.50%
$ ilde{T}_4$	-0.49%	+0.67%

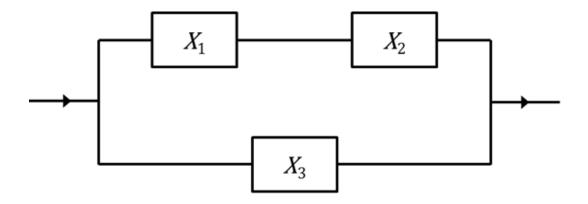
Δ _{rel} (PEM)	$\mathbb{E}(\cdot)$	$\sigma(\cdot)$
$ ilde{T}_1$	+0.00%	-0.03%
$ ilde{T}_2$	+0.00%	-0.03%
$ ilde{T}_3$	+0.01%	-0.05%
$ ilde{T}_4$	+0.01%	-0.07%

10,000Sample points

25 (!)
Sample points



Composite system with three (stochastically) independent components:



- Exponential life distributions: $X_i \sim \text{Exp}(\beta_i) \rightarrow \text{Reliability}$: $R_{X_i}(t) = \exp(-\frac{t}{\beta_i})$
- **System reliability** (= probability that the system "survives" until time t):

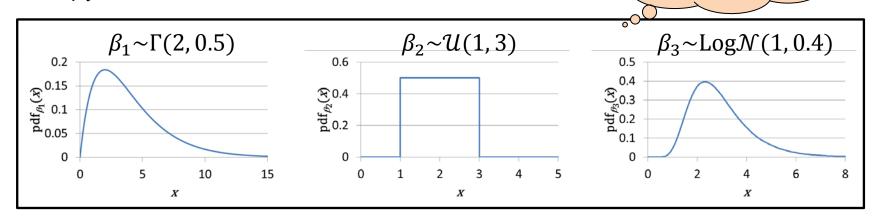
$$R_{\text{sys}}(t) = R_{X_1}(t)R_{X_2}(t) + R_{X_3}(t) - R_{X_1}(t)R_{X_2}(t)R_{X_3}(t)$$



$$R_{\text{sys}}(t) = \exp\left(-\frac{t}{\beta_1} - \frac{t}{\beta_2}\right) + \exp\left(-\frac{t}{\beta_3}\right) - \exp\left(-\frac{t}{\beta_1} - \frac{t}{\beta_2} - \frac{t}{\beta_3}\right)$$

Exemplary assumptions!

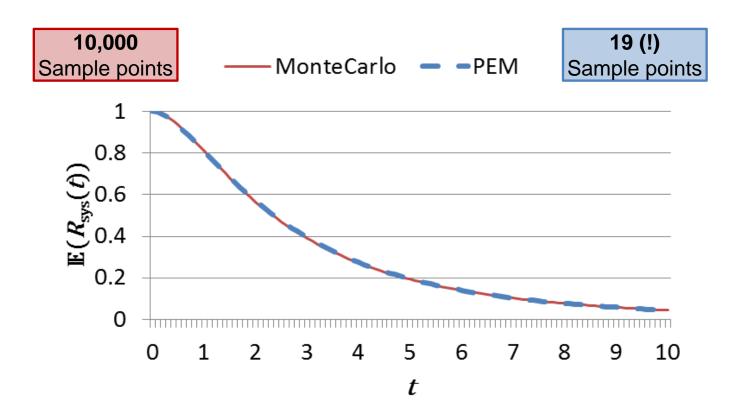
- Parameters β_i fixed \rightarrow Deterministic function!
- But, β_i uncertain \rightarrow Random variable for each t!



• Apply **PEM** (in comparison to MC) for estimating $\mathbb{E}(R_{\rm sys}(t))$ and ${\rm Var}(R_{\rm sys}(t))$ depending on t

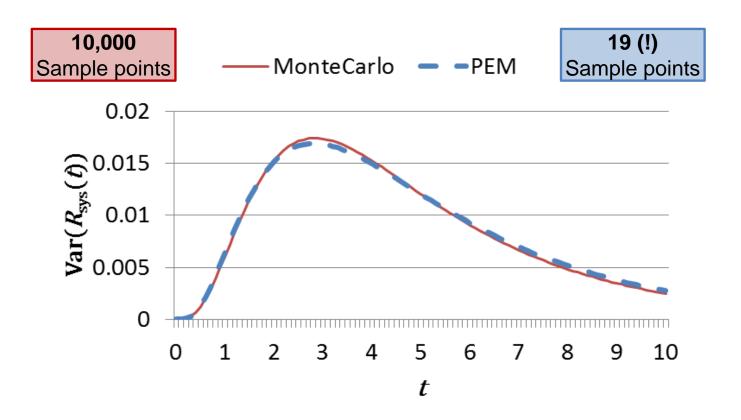


Expected system reliability based on PEM and MC simulation





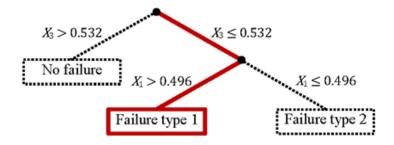
Variance of the system reliability based on PEM and MC simulation



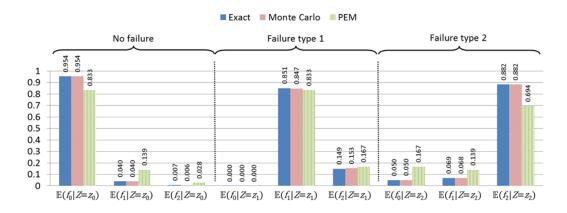


Example of use: Failure diagnosis using decision trees

Decision tree:



Results:



Further information: see supplementary material!

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Draft manuscript (submitted to Proc IMechE Part O: J Risk and Reliability)

Analyzing uncertainties in model response using the point estimate method: applications from railway asset management

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Abstract

Predicting current and future states of rail infrastructure based on existing data and measurements is essential for optimal maintenance and operation of railway systems. Statistical and/or other complex models provide helpful tools for detecting failures and extrapolating current states into the future. This, however, inherently gives rise to uncertainties in the model response that must be analyzed carefully to avoid misleading results and conclusions. Commonly, Monte Carlo (MC) simulations are used for such analyses which often require a large number of sample points to be evaluated for convergence. Moreover, even if quite close to the exact distributions, the MC approach necessarily provides approximate results only. In contrast to that, the present contribution reviews an alternative way of computing important statistical quantities of the model response. That is the so-called point estimate method (PEM) which can be shown to be exact under certain constraints and which usually (i.e., depending on the number of input variables) works with only a few specific sample points. Thus, this method helps to reduce the computational load for model evaluation considerably in the case of complex models or in large-scale applications. Based on three more or less academic examples from the wide field of railway asset management, the performance of the PEM is demonstrated: i) track degradation, ii) reliability analysis of composite systems and iii) failure detection/identification using decision trees. Advantages as well as limitations of the PEM in comparison to common MC simulations are discussed.

Keywords

Uncertainty propagation analysis, reliability, asset management, prognosties, health management, point estimate method



Summary: Assets and drawbacks of PEM

- Flexible approach (Easy to apply)
- Reduction of computing time because of small samples (compared to MC)
- Exact results (for "polynomial models" with given maximum degree)
- Applicable to various types of distributions (by transforming sample points)
- Reproducible results (deterministic approach)
- Approximate calculation of the full output distribution possible by combining PEM with further approaches (e.g., polynomial chaos expansion)
- Basic statistics of the output distribution only (when using the original PEM)
- Stochastically independent inputs required
- No general guarantee concerning the accuracy of the results (i.e., no convergence as $N \to \infty$)









Thanks for your attention!

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